

Design of the Booster transverse damper.

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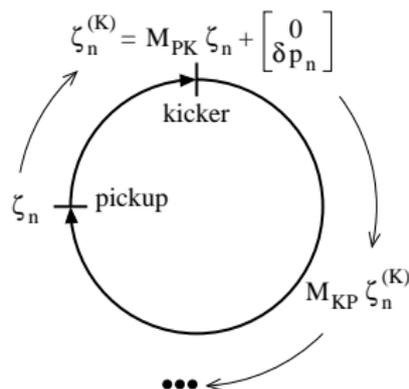
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1. Damper System

Transverse beam motion can be described in terms of betatron state-vector

$$\zeta(s) \stackrel{\text{def}}{=} [q(s), p_q(s)]^T$$

(where $q = x, z$ is one of the canonical transverse coordinates and p_q is the corresponding conjugate momentum dq/ds)

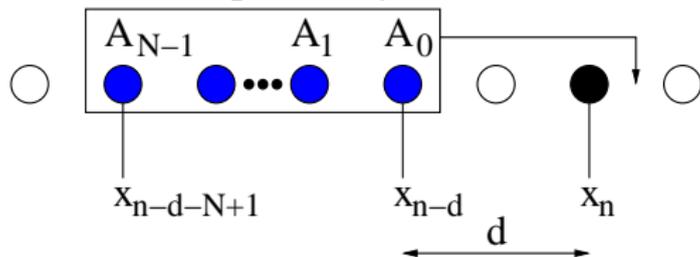


2. Digital Filter

In most general form the filter which is based on a prehistory of **N** turns and applied **d** turns later can be written as:

$$\delta p_n \propto \sum_{k=0}^{N-1} A_k x_{n-d-k}.$$

Correction uses **N**
turns of prehistory



3. Choice of coefficients

1. Notch Filter

In general the digital filter should not be sensitive to the equilibrium orbit offset relative to the geometrical center of pickup

$$x_n = \alpha = \text{const}$$

in order to provide the best work of the damping algorithm. This condition is usually called a notch filter and simply gives an additional constraint

$$\sum_{k=0}^{N-1} A_k = 0.$$

Sum rearrangement

The notch condition allows one to rearrange the sum and reduce number of independent coefficients:

$$\sum_{k=0}^{N-1} A_k x_{n-d-k} = \sum_{k=0}^{N-2} B_k (x_{n-d-k} - x_{n-d-k-1}).$$

where

$$B_i = \sum_{k=0}^i A_k$$

2. Filter sensitivity to the linear change of the orbit in time

In addition to the notch filtering one can make the filter to be non-sensitive to the linear orbit change

$$x_n \propto \beta n$$

which gives

$$\sum_{k=0}^{N-2} B_k = 0.$$

3. Generalization

This result can be generalized for K -th order polynomial

$$x_n^{\text{eq}} = \alpha + \beta n + \dots + \gamma n^K,$$

where at least $(K + 2)$ coefficients are needed and they are given by the solution of matrix equation

$$\begin{bmatrix} 1 & 1 & 1 & \cdots & (K+1)^0 \\ 0 & 1 & 2 & \cdots & (K+1)^1 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ 0 & 1 & 2^K & \cdots & (K+1)^K \end{bmatrix} \begin{bmatrix} A_0 \\ A_1 \\ \vdots \\ A_{K+1} \end{bmatrix} = 0,$$

which solution is related to the binomial coefficients

$$A_k = (-1)^k C_k^{K+1}, \quad k = 0, \dots, K+1.$$

4. Is it enough?

- **Whether the choice of coefficients is optimal?**
- **Why do not we use let say 100 turns of prehistory for the corrections?**

4. Beam dynamics

The canonical transformation to the so-called normalized coordinates $(p, q) \rightarrow (\mathcal{P}_q, \eta_q) \rightarrow z = \eta - iP$:

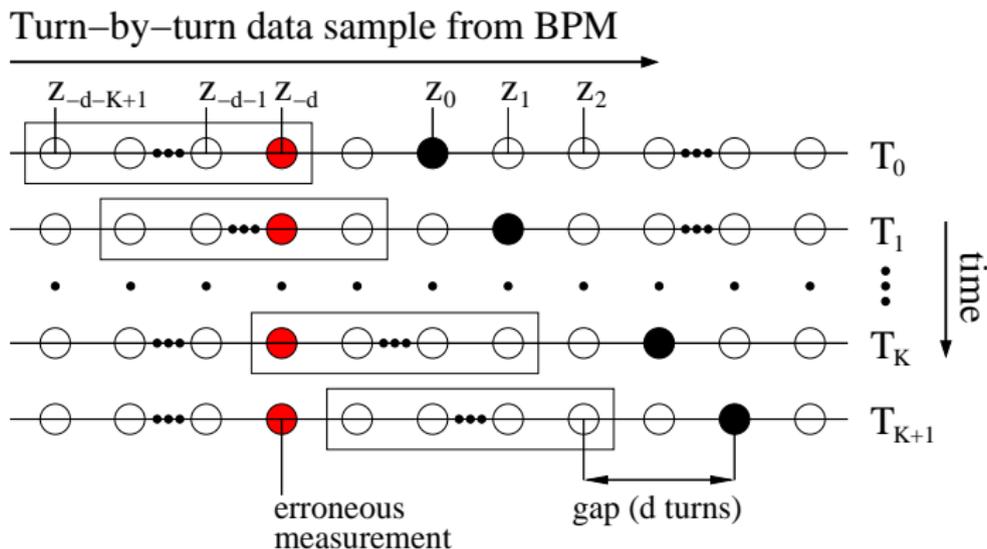
$$\begin{aligned}\eta_q(s) &= q(s)/\sqrt{\beta(s)}, \\ \mathcal{P}_q(s) &= p_q(s)\sqrt{\beta(s)} + q(s)\frac{\alpha(s)}{\sqrt{\beta(s)}},\end{aligned}$$

simplify the motion to the simple rotation, and allow to write recurrent relation which describes the beam dynamics

$$z_{n+1} = e^{i\mu_2} \left[e^{i\mu_1} z_n - ig \sum_{k=0}^{\mathcal{K}-1} A_k (\Re z_{n-d-k} + \delta\eta_{n-d-k}) \right].$$

5. Emittance growth

Each erroneous measurement will contribute K turns \rightarrow the number of coefficients should be minimized.



6. Damping

Damping rate can be easily calculated for the case of the small gain g :

$$g_d = i \frac{g}{2} e^{-i(\mu_1 + \mu_0 d)} \sum_{k=0}^{\mathcal{K}-1} A_k e^{-i\mu_0 k},$$

which gives an additional constraint

$$\Im(g_d) = 0$$

in order to maximize $\Re(g_d)$.

7. Conclusion

Joint solution of matrix equation for A_k along with damping constraint $\mathfrak{S}(g_d)$ gives:

$N = 0$	$A_0 :$	$\sin(1.5\mu_0 + \delta\mu)$
	$A_1 :$	$-\sin(1.5\mu_0 + \delta\mu) - \sin(0.5\mu_0 + \delta\mu)$
	$A_2 :$	$\sin(0.5\mu_0 + \delta\mu)$
$N = 1$	$A_0 :$	$\cos(2\mu_0 + \delta\mu)$
	$A_1 :$	$-2\cos(2\mu_0 + \delta\mu) - \cos(\mu_0 + \delta\mu)$
	$A_2 :$	$\cos(2\mu_0 + \delta\mu) + 2\cos(\mu_0 + \delta\mu)$
	$A_3 :$	$-\cos(\mu_0 + \delta\mu)$
$N = 2$	$A_0 :$	$\sin(2.5\mu_0 + \delta\mu)$
	$A_1 :$	$-3\sin(2.5\mu_0 + \delta\mu) - \sin(1.5\mu_0 + \delta\mu)$
	$A_2 :$	$3\sin(2.5\mu_0 + \delta\mu) + 3\sin(1.5\mu_0 + \delta\mu)$
	$A_3 :$	$-\sin(2.5\mu_0 + \delta\mu) - 3\sin(1.5\mu_0 + \delta\mu)$
	$A_4 :$	$\sin(1.5\mu_0 + \delta\mu)$

Thank you for attention!