

PARASITIC RESONANCES IN HIGH POWER PROTON LINACS

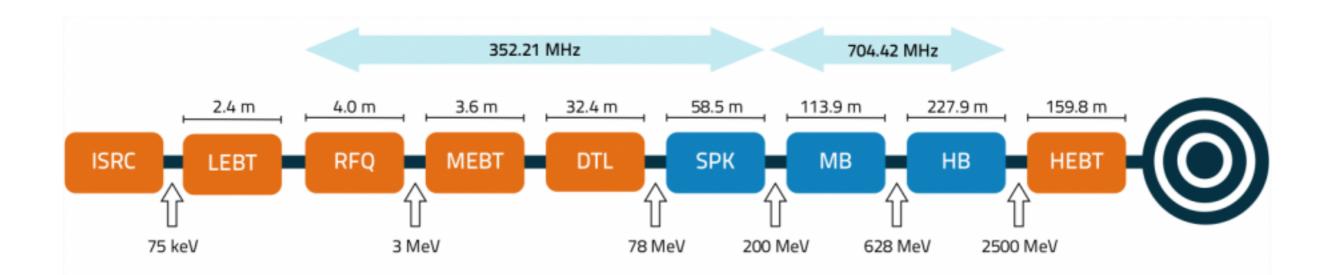
Rob Ainsworth

John Adams Institute for Accelerator Science

OUTLINE

- European Spallation Source
- Cavity Modes
 - Spoke Cavities
 - Elliptical Cavities
- Influence of Parasitic Modes
 - Same Order Modes (SOMs)
 - Higher Order Modes (HOMs)
- HOM coupler designs
 - Multipacting

EUROPEAN SPALLATION SOURCE



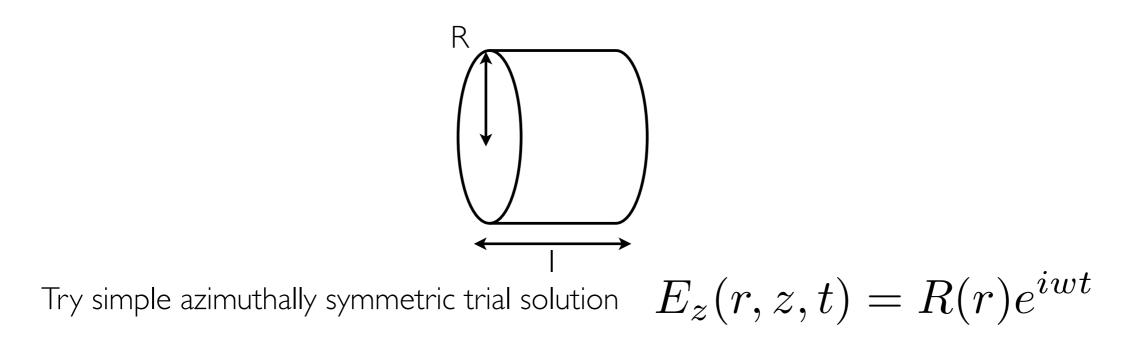
	Value	Unit
Final kinetic energy	2.5	GeV
Current	50	mA
Pulse repetition rate	14	Hz
Bunch frequency	352.21	MHz
Average power	5	MW
Peak power	125	MW



CAVITY MODES



PILLBOX CAVITY



Wave Equation
$$\frac{\partial^2 E_z}{\partial z^2} + \frac{1}{r} \frac{\partial E_z}{\partial r} + \frac{\partial^2 E_z}{\partial r^2} - \frac{1}{c^2} \frac{\partial^2 E_z}{\partial t^2} = 0$$

Boundary Condition: No tangential E field No normal B field



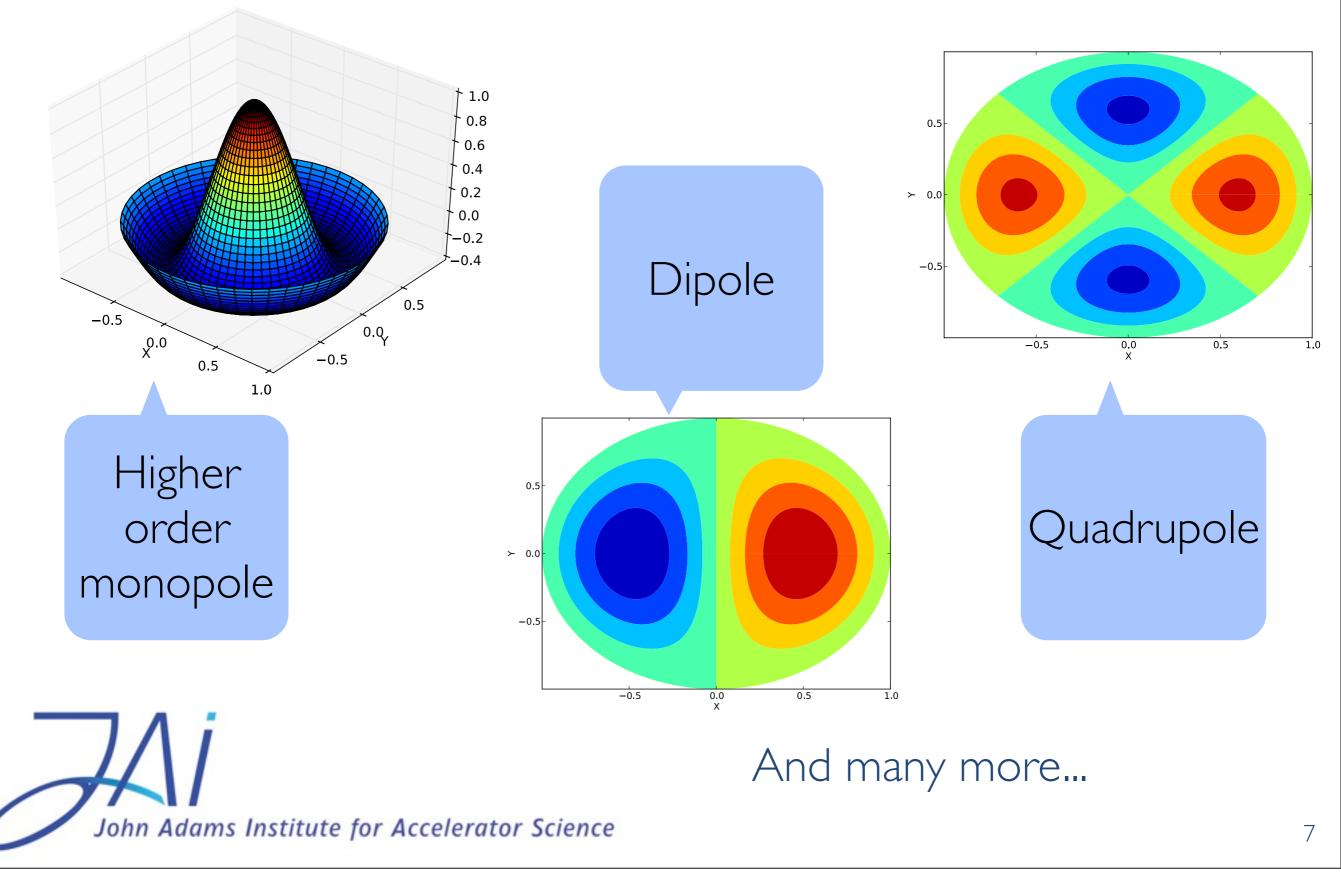
ACCELERATING MODE

Transverse Magnetic Mode (TM) $E_z = E_0 J_0(k_r r) \cos \omega t \qquad B_\theta = -\frac{E_0}{c} J_1(k_r r) \sin \omega t$ 0.8 0.6 0.4 0.2 0.0 0.5 0.0, -0.50.0 X -0.5 0.5 1.0

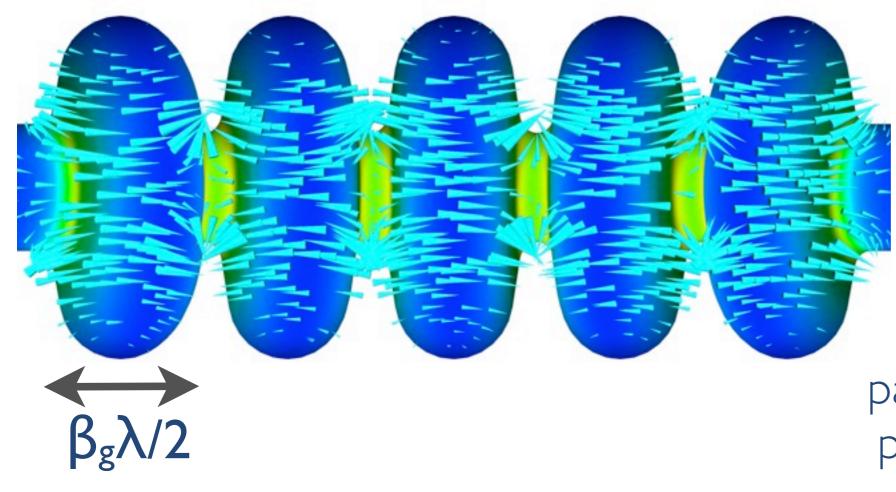
However, not the only mode . ..

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HIGHER ORDER MODES



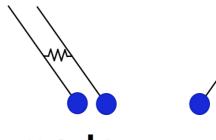
ELLIPTICAL CAVITIES



N coupled pillbox cavities

Modes split into passbands with differing phase advance per cell

Two families of ellipticals operating in π - mode @ 704.42 MHz

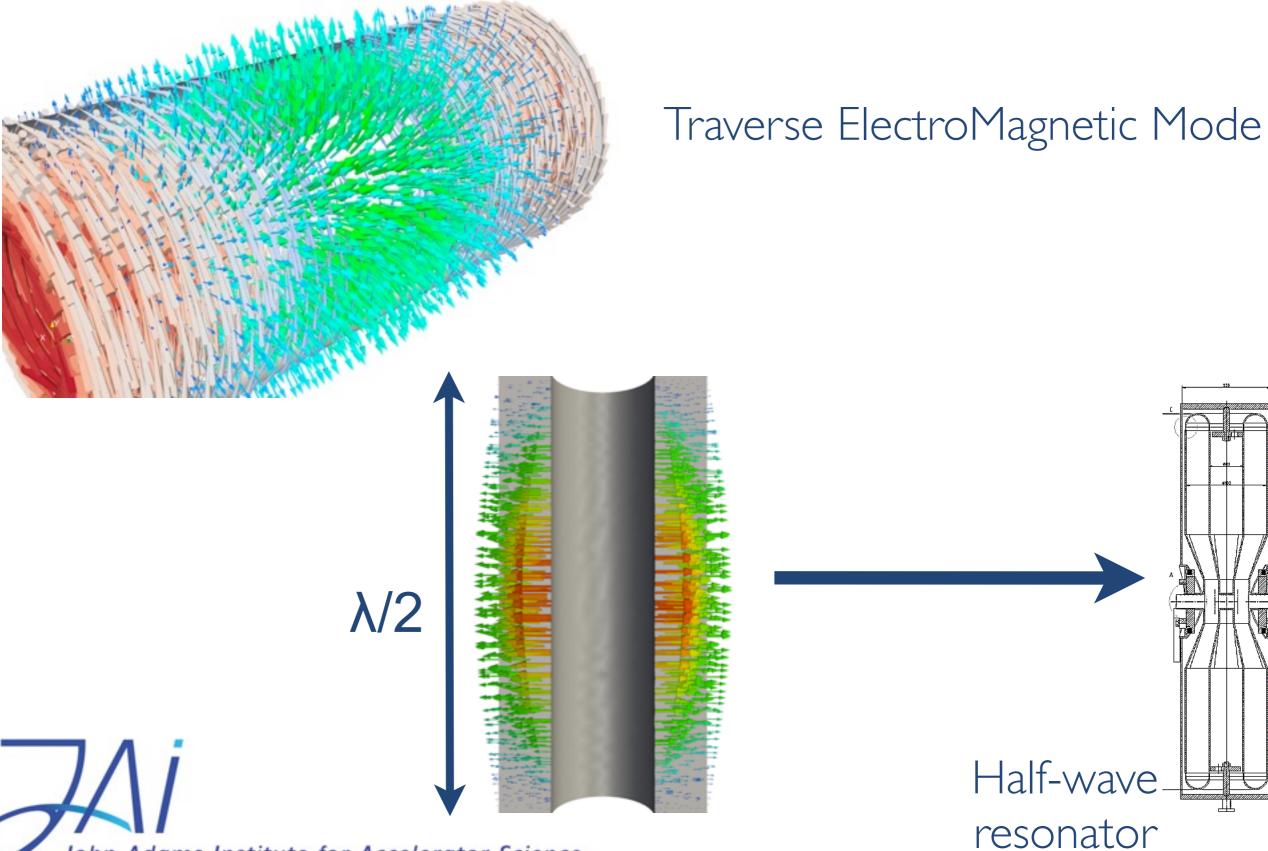




π-mode

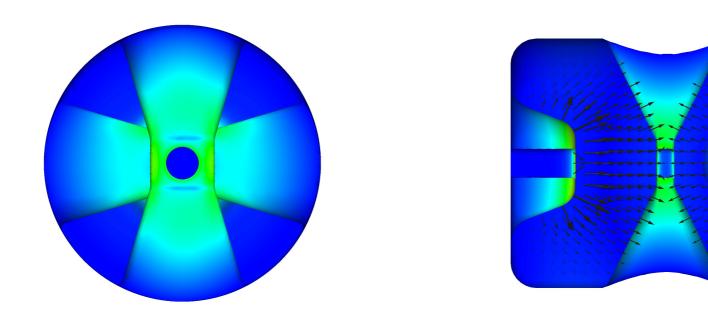


TEM RESONATOR



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SPOKE RESONATORS



Each spoke rotated by 90°

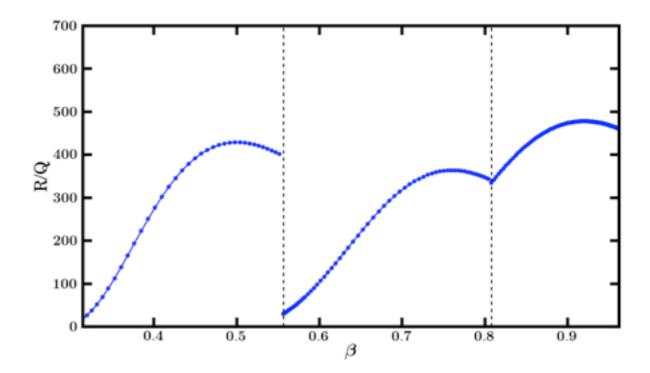
Variant of TEM cavity

n stacked HWRs



THE NEED FOR 3 FAMILIES

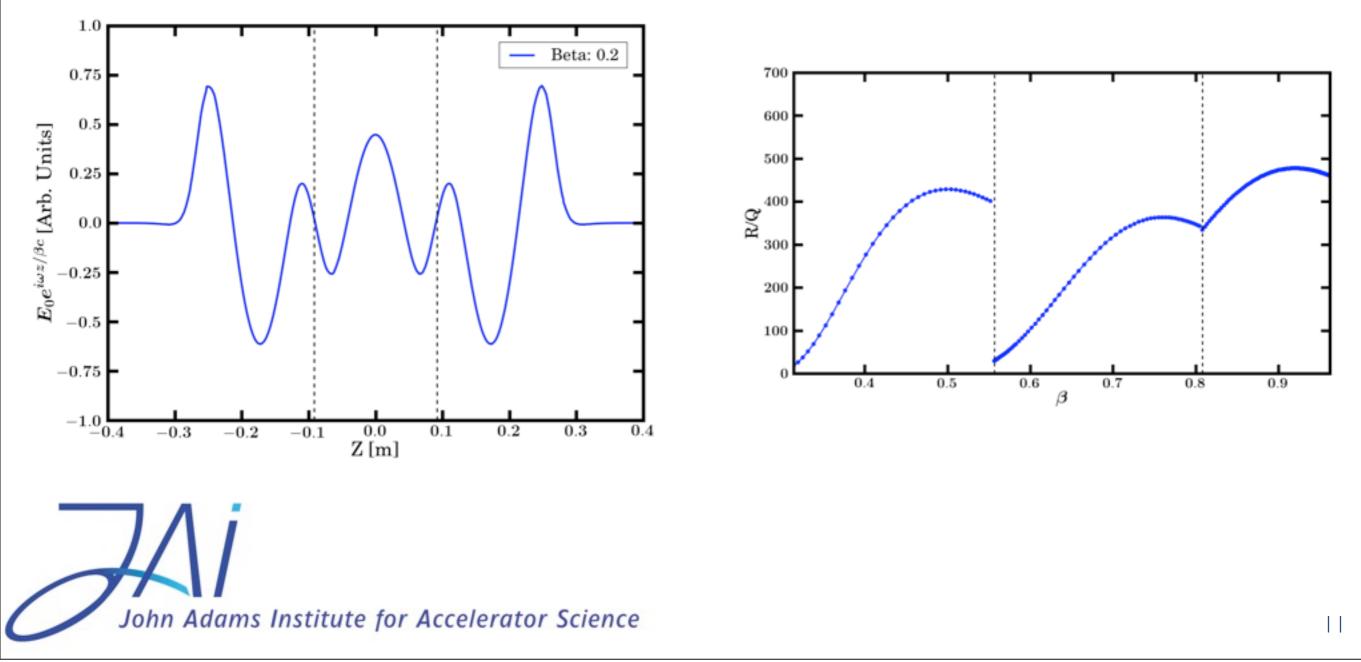
$$(R/Q)_n(\beta) = \frac{\left|\int_{-\infty}^{\infty} E_{z,n}(r=0,z)e^{i\omega_n \frac{z}{\beta c}} dz\right|^2}{\omega_n U_n}$$





THE NEED FOR 3 FAMILIES

$$(R/Q)_n(\beta) = \frac{\left|\int_{-\infty}^{\infty} E_{z,n}(r=0,z)e^{i\omega_n \frac{z}{\beta c}} dz\right|^2}{\omega_n U_n}$$



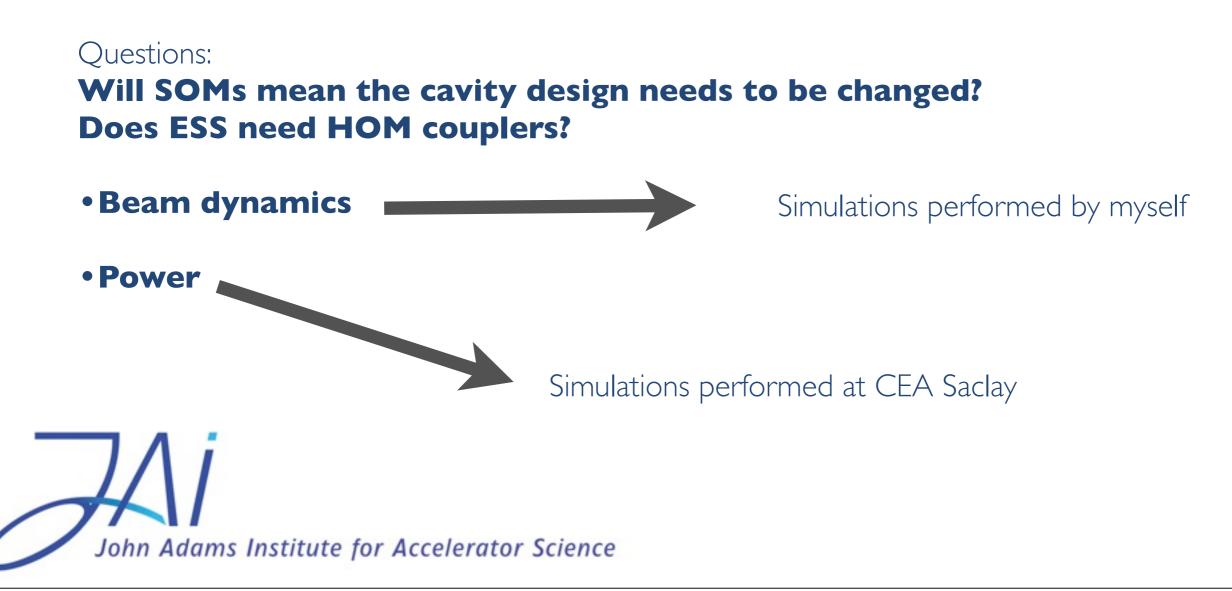
PARASITIC MODES



MOTIVATION

Beam induced modes in SCRF cavities may drive the **beam unstable** and **increase the cryogenic load**, therefore **HOM couplers** are usually installed to provide sufficient damping.

.....However, recent experience at SNS has shown **couplers may be unnecessary** and have **degraded performance** of the machine.



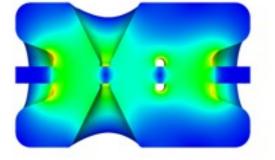
SAME ORDER MODES

Part of

same passband as

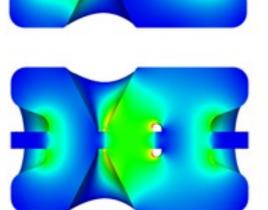
fundamental

π-mode 352.21 MHz

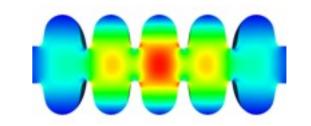


0-mode 362.69 MHz

396.96 MHz



Same order, just different phase advance



π/5 - mode 693.19 MHz

2π/5 - mode 696.30 MHz

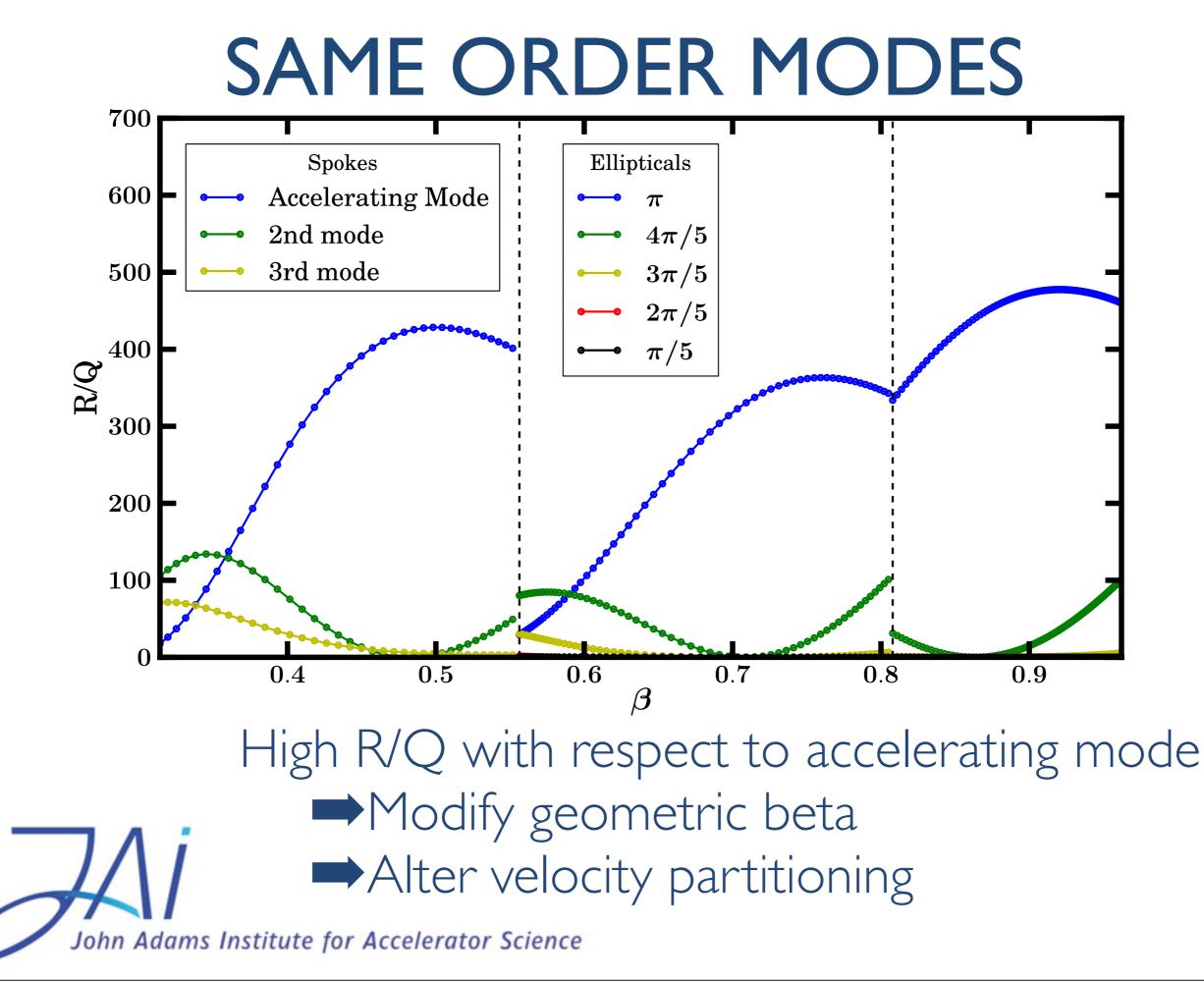
3π/5 - mode 700.14 MHz

4π/5 - mode 703.2 MHz

π - mode 704.42 MHz



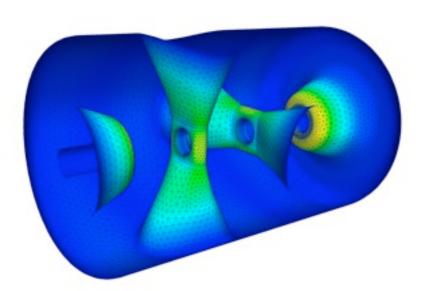
Close in frequency to accelerating mode Cannot damp using couplers

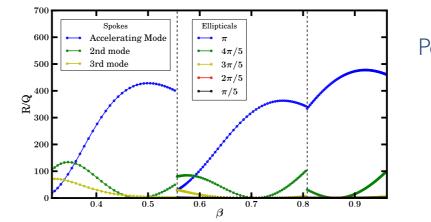


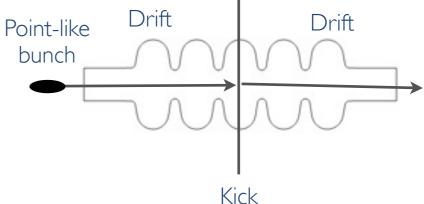
SIMULATION INFO

Simulate cavity geometries to extract field-maps Determine R/Q, frequencies of modes below cutoff

Calculate the influence of modes of beam quality

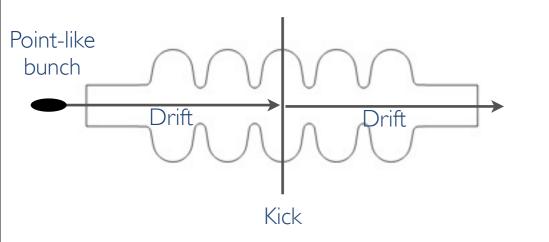






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SIMULATION INFO



Energy and time error calculated at each cavity with respect to synchronous bunch

$$\Delta E^{(m+1)} = \Delta E^{(m)} + \Delta U_{RF}^{(m)} + \Delta U_n^{(m)}$$

- I million point-like bunches tracked per linac
- SOM/HOM frequencies distributed with a gaussian spread

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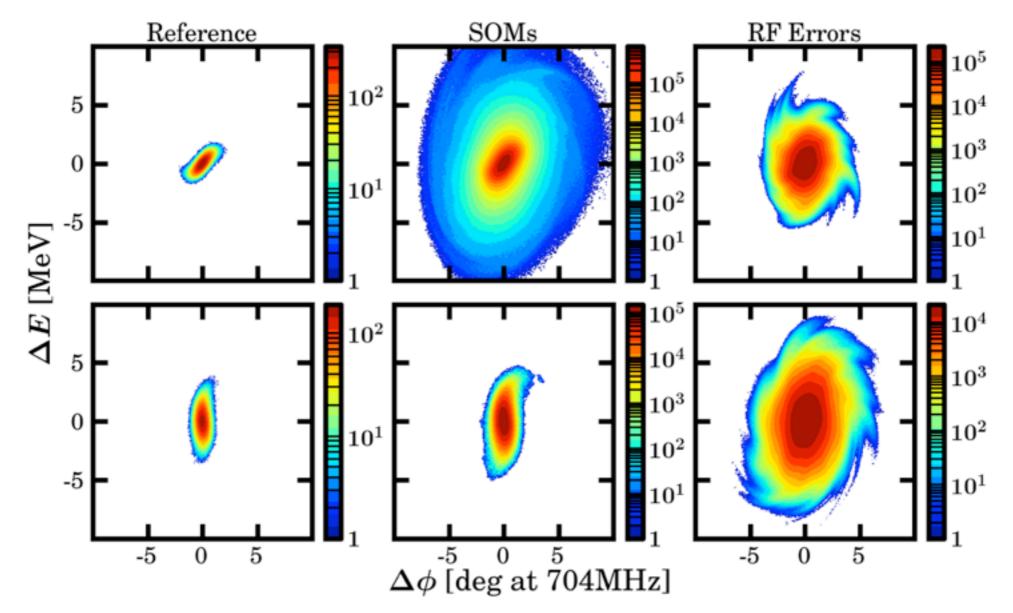
• $\sigma = 1.09 \times 10^{-3}$. |f₀ - f_{hom}|

$$\Delta t^{(m+1)} = \Delta t^{(m)} + (dt/dE)_E^{(m)} \cdot \Delta E^{(m)}$$

$$\Delta U_n = q(\Re(V_n)\cos(\omega_n dt) - \Im(V_n)\sin(\omega_n dt)) - \frac{1}{2}\Delta V_{q,n}$$

$$\Delta V_{q,n} = -q \frac{\omega_n}{2} (R/Q)_n(\beta)$$

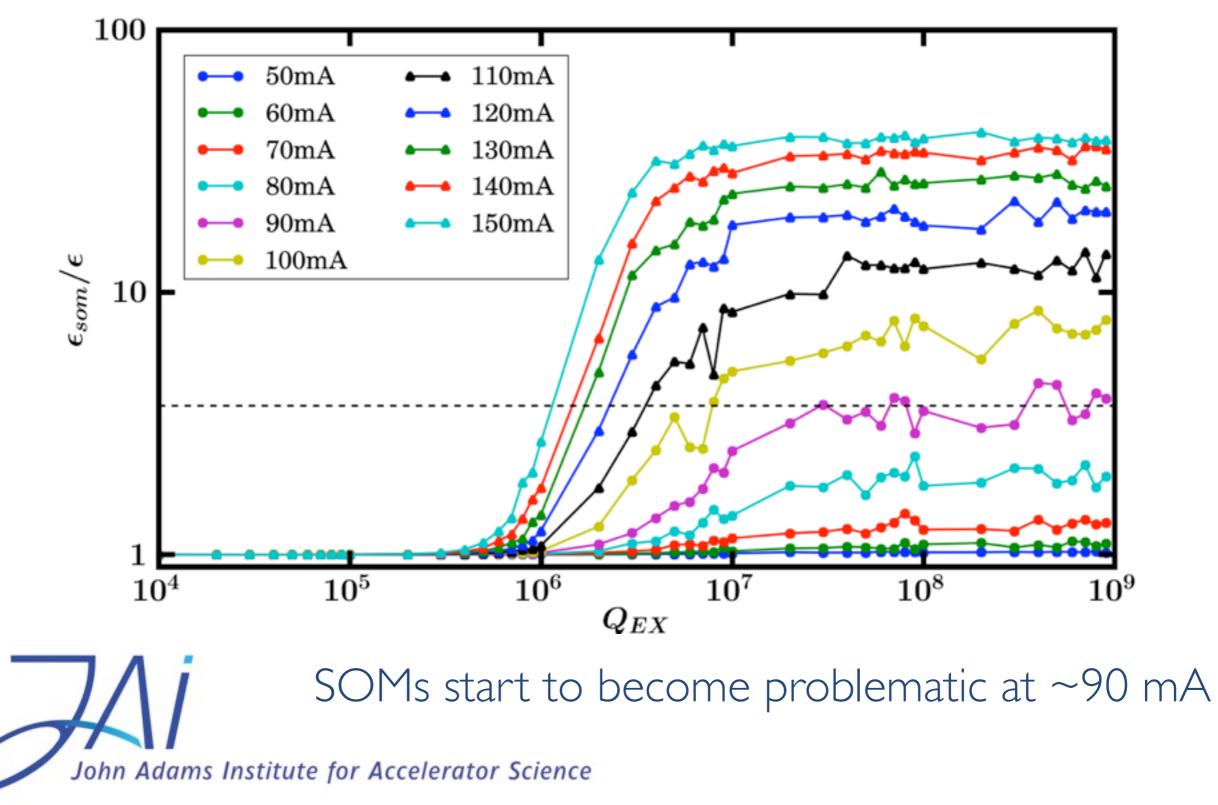
COMPARISON OF LINACS



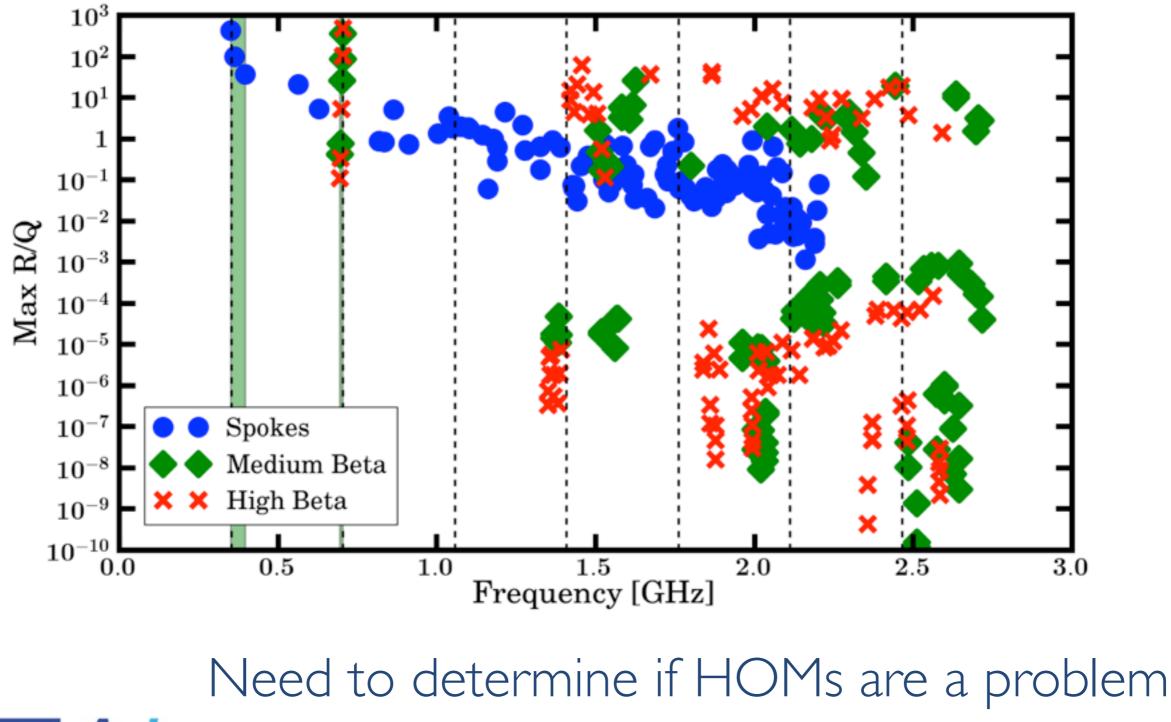
It is possible to design a linac susceptible to SOMs however the latest baseline shows no adverse effects John Adams Institute for Accelerator Science

CURRENT & DAMPING SCAN

 $T_{d,n} = 2Q_{L,n}/\omega_n \approx 2Q_{EX,n}/\omega_n$



HIGHER ORDER MODES

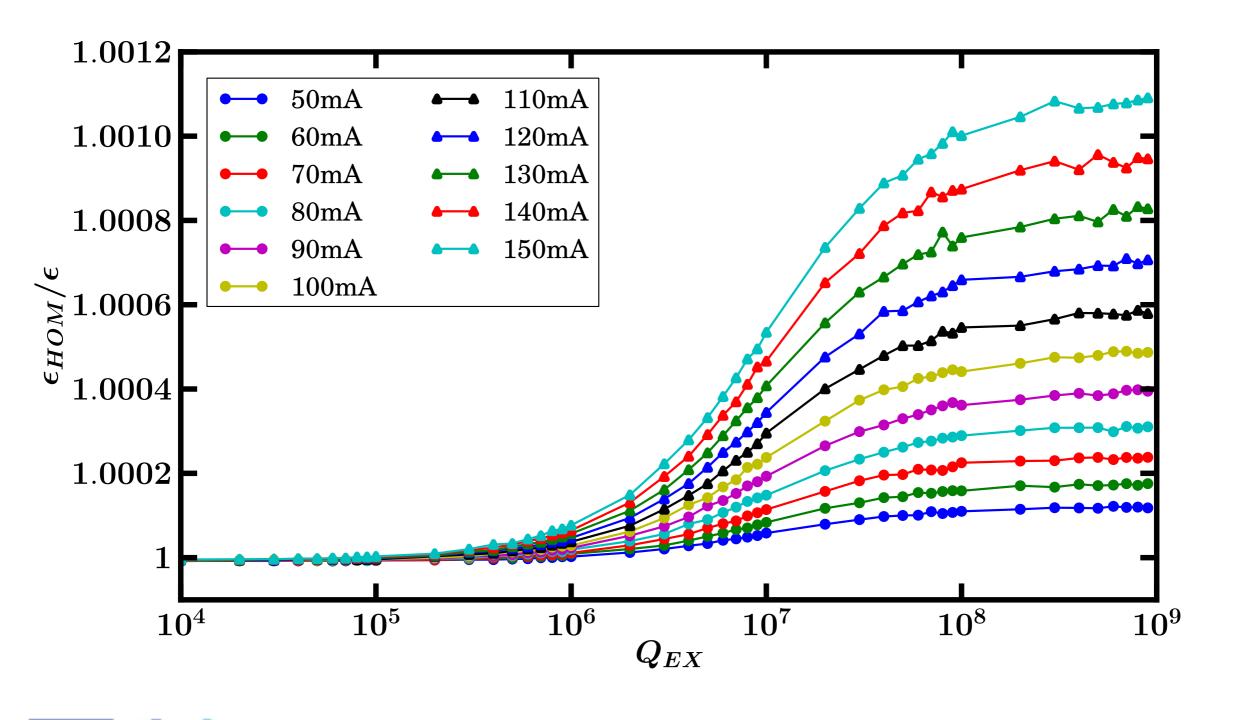


Are HOM couplers needed?

 $f_{ML} = n \cdot 352.21 \text{MHz}$

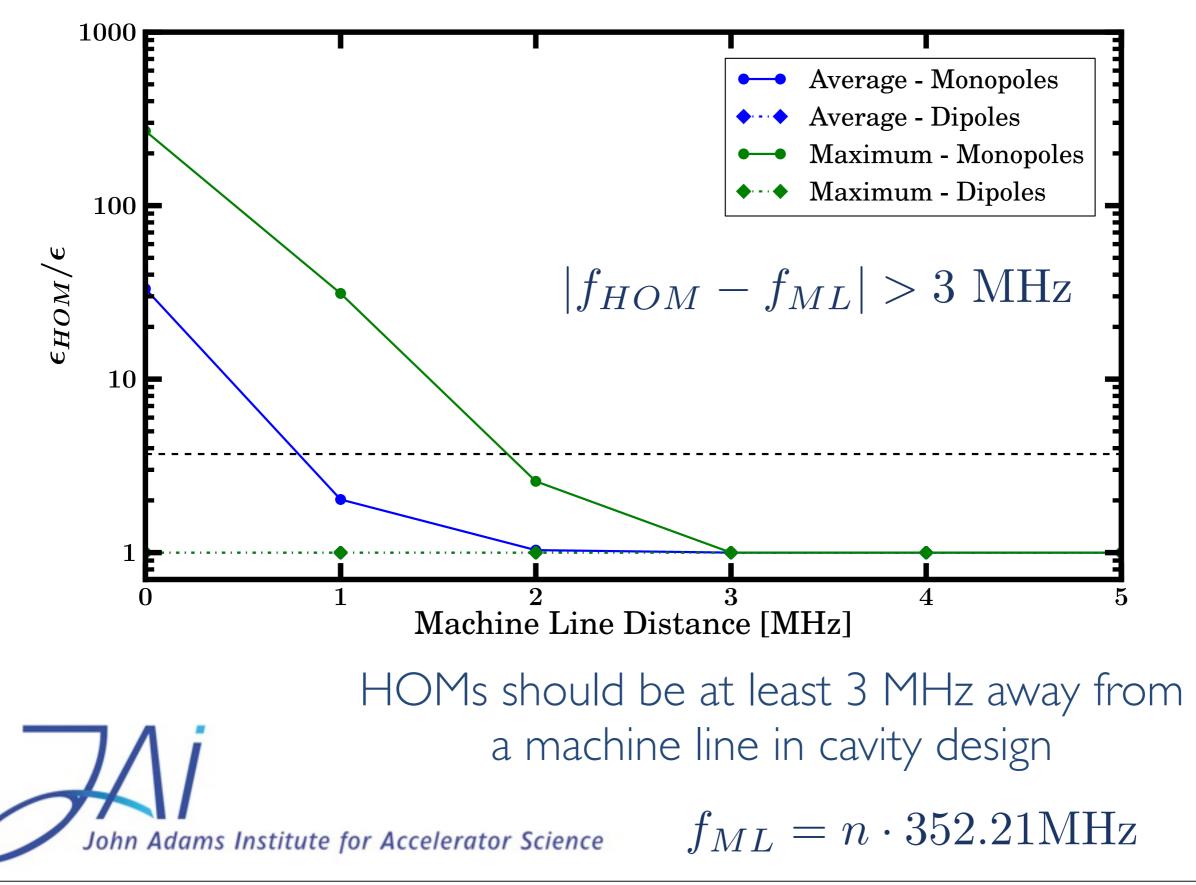
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CURRENT & DAMPING SCAN

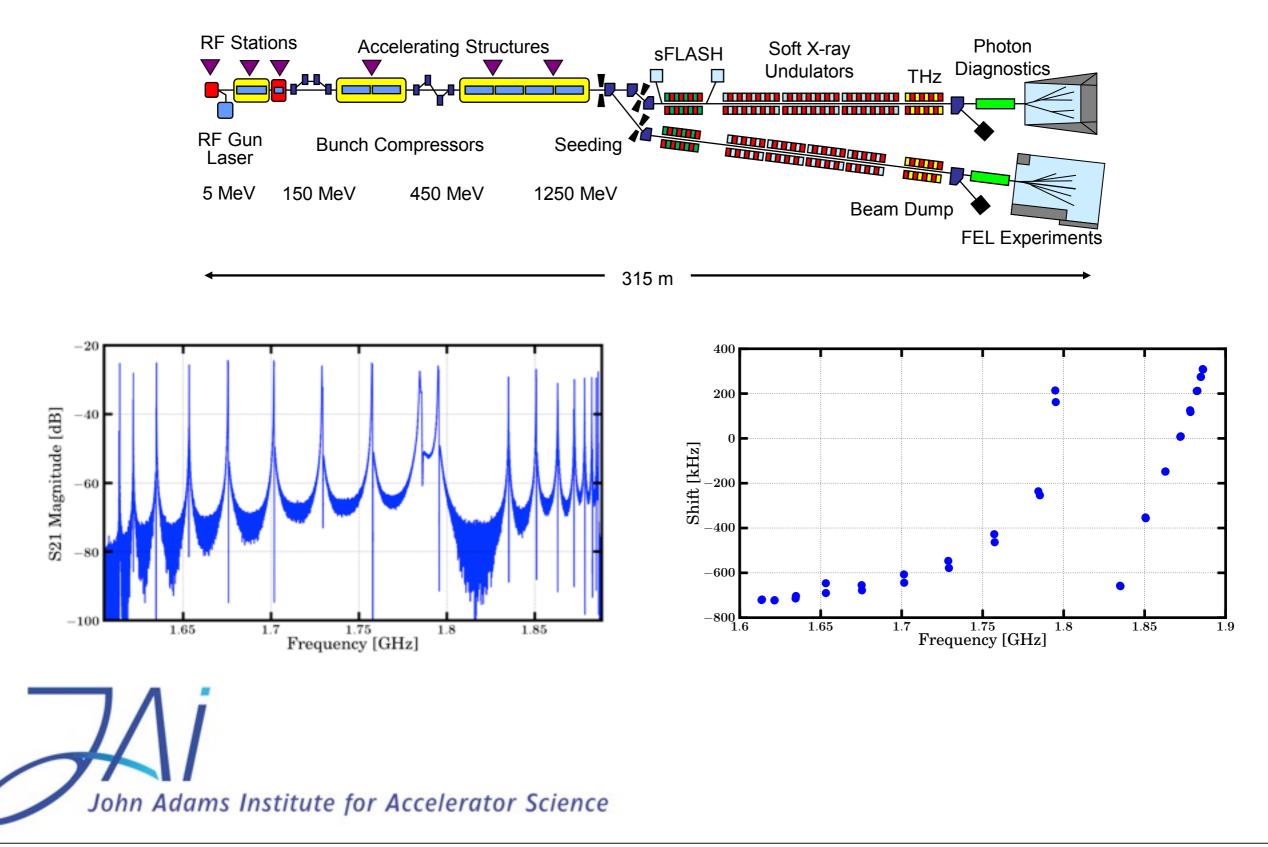


Away from a machine line, HOMs are of no concern John Adams Institute for Accelerator Science

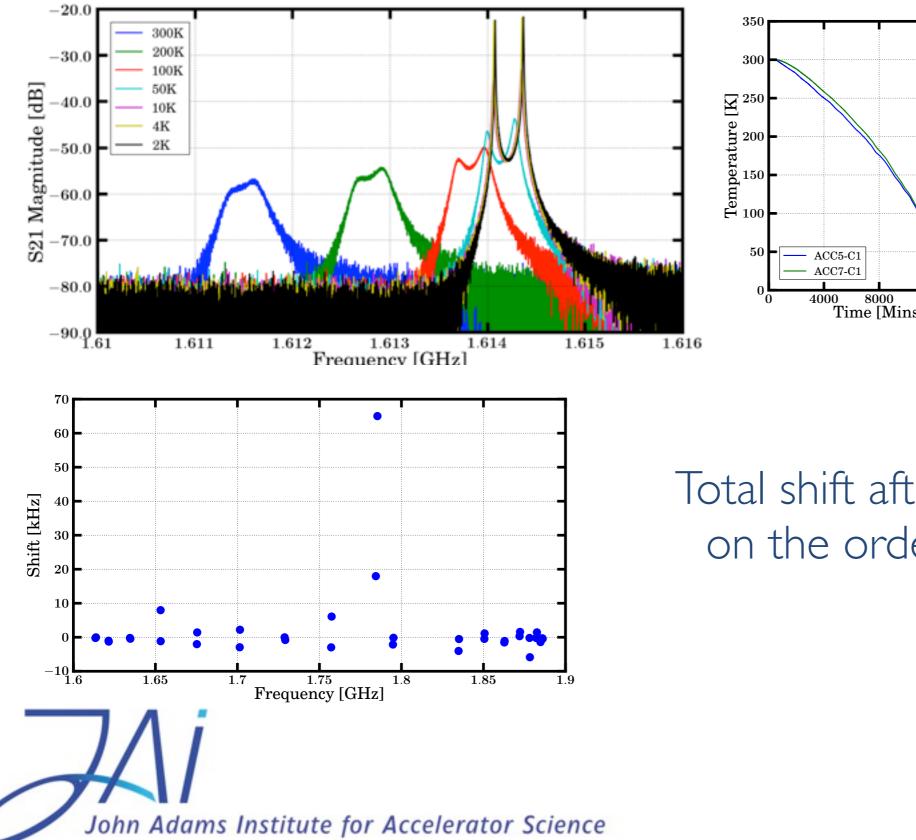
SAFE DISTANCE

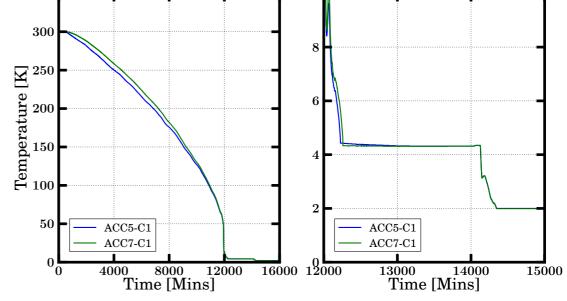


DETUNING STUDIES



WARMUP, COOLDOWN AND RETUNED



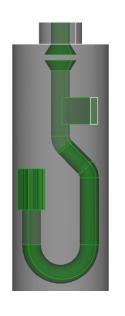


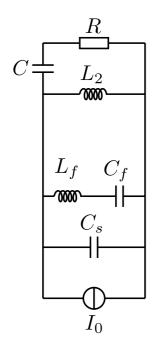
Total shift after all procedures on the order of a few kHz

HOM COUPLER STUDIES

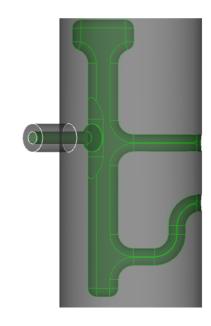


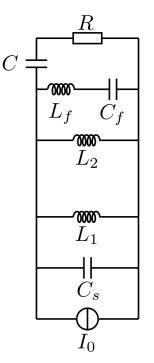
INITIAL DESIGNS



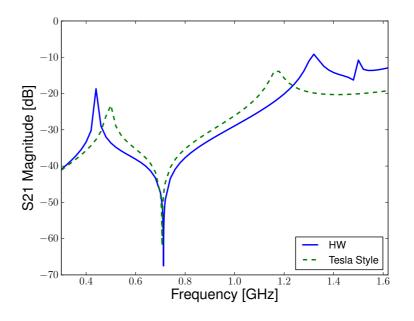


Designed by Rostock University (C. Potratz, H.W. Glock)





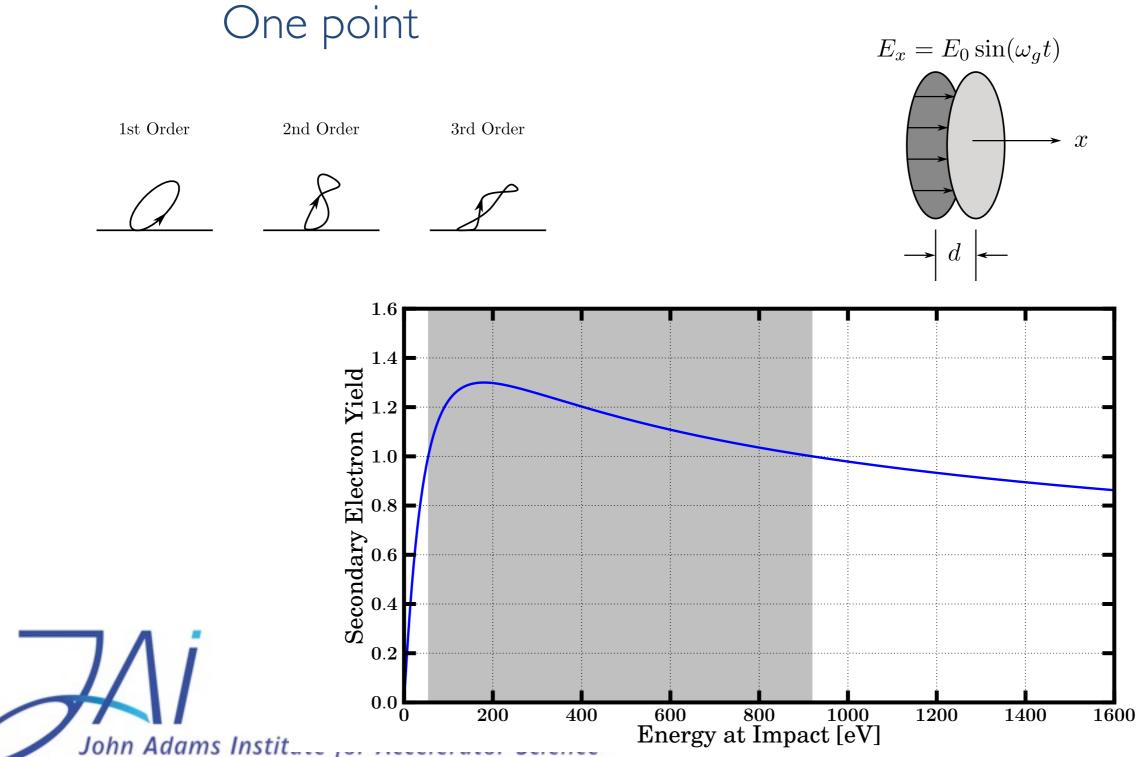
Rescaled SNS coupler (R. Calaga)



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MULTIPACTING





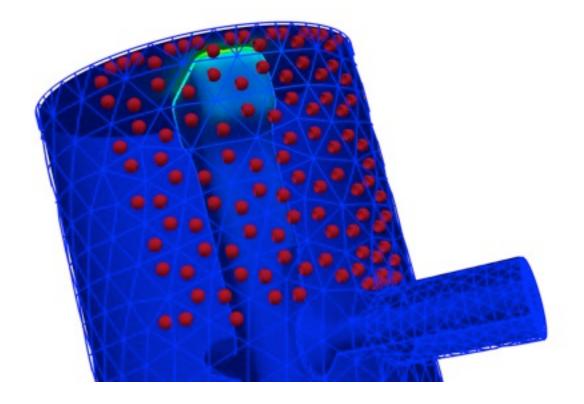
TRACK3P

Define bounding box for emission

Particles emitted from centre of mesh elements within box

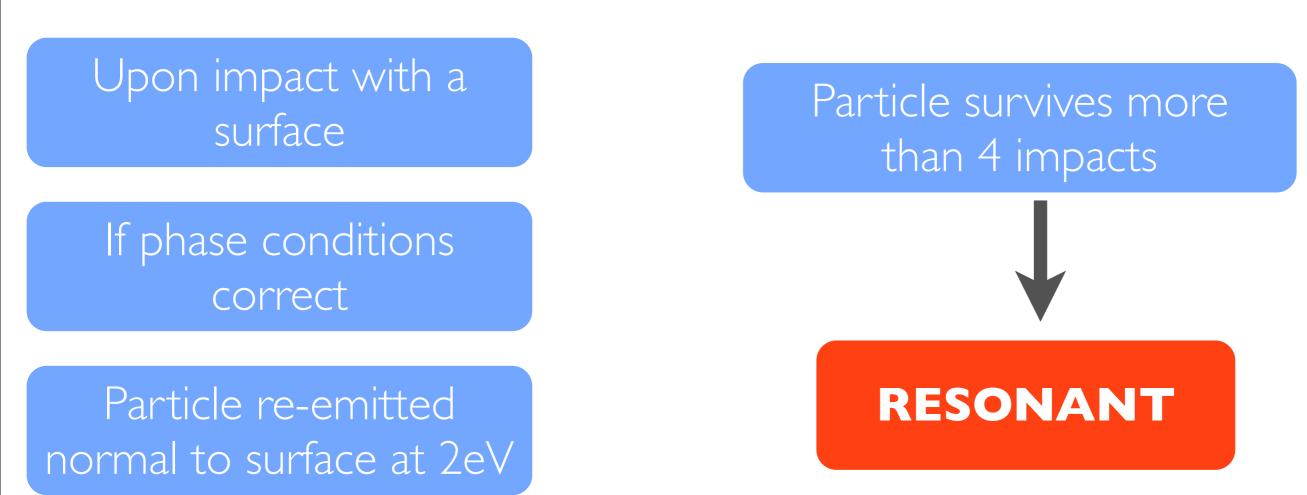
Occurs every 3.6° for 1 RF cycle

Particles tracked for a further 19 RF cycles





TRACK3P

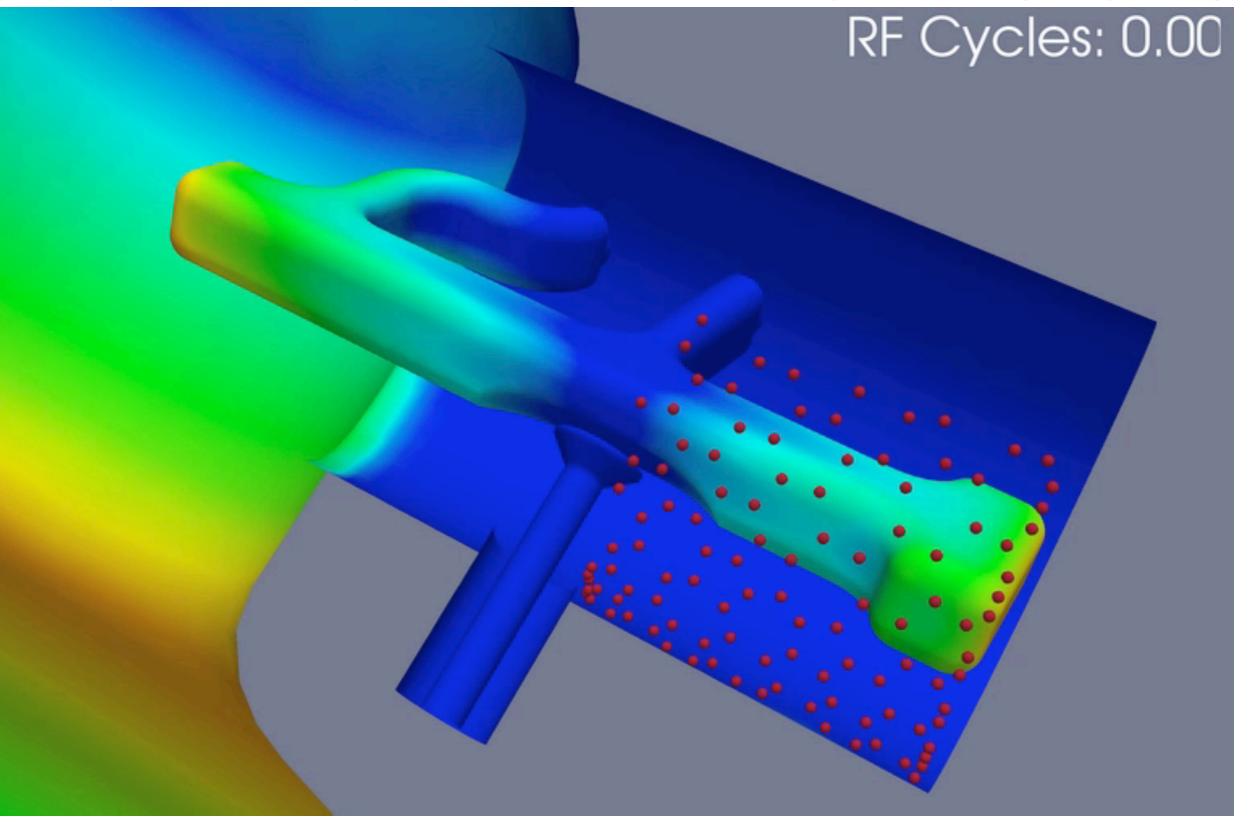


Note: 20RF cycles means cannot resolve trajectories higher than 5th order

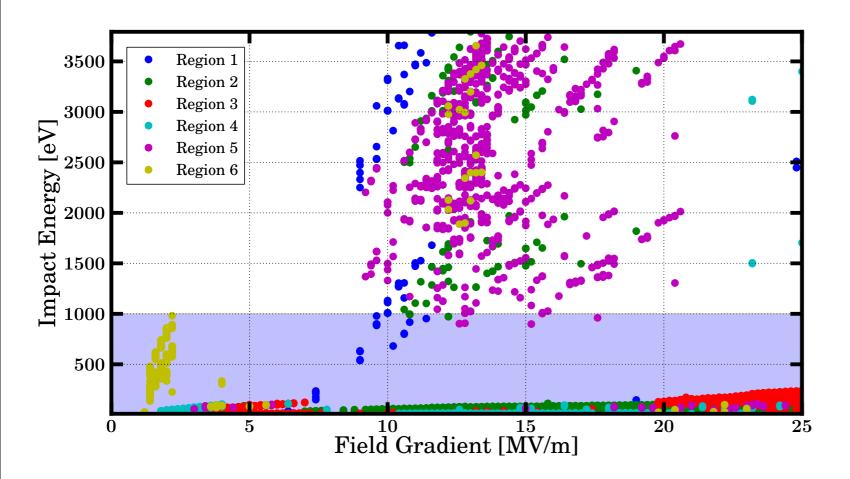


MULTIPACTING

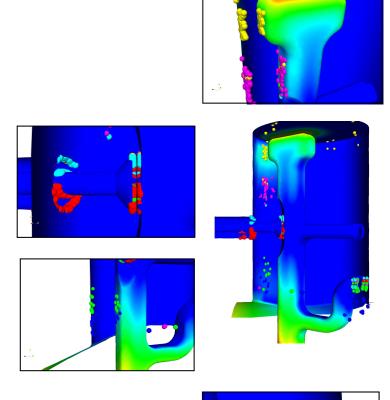
http://twiki.ph.rhul.ac.uk/twiki/pub/PP/Public/RobAinsworthRCDesign704/RC-Coupler-highQuality.mov

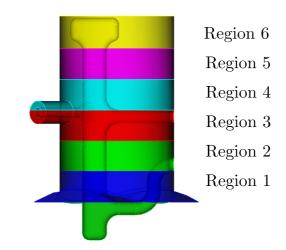


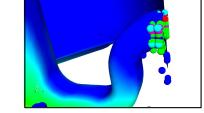
MP IN TESLA STYLE



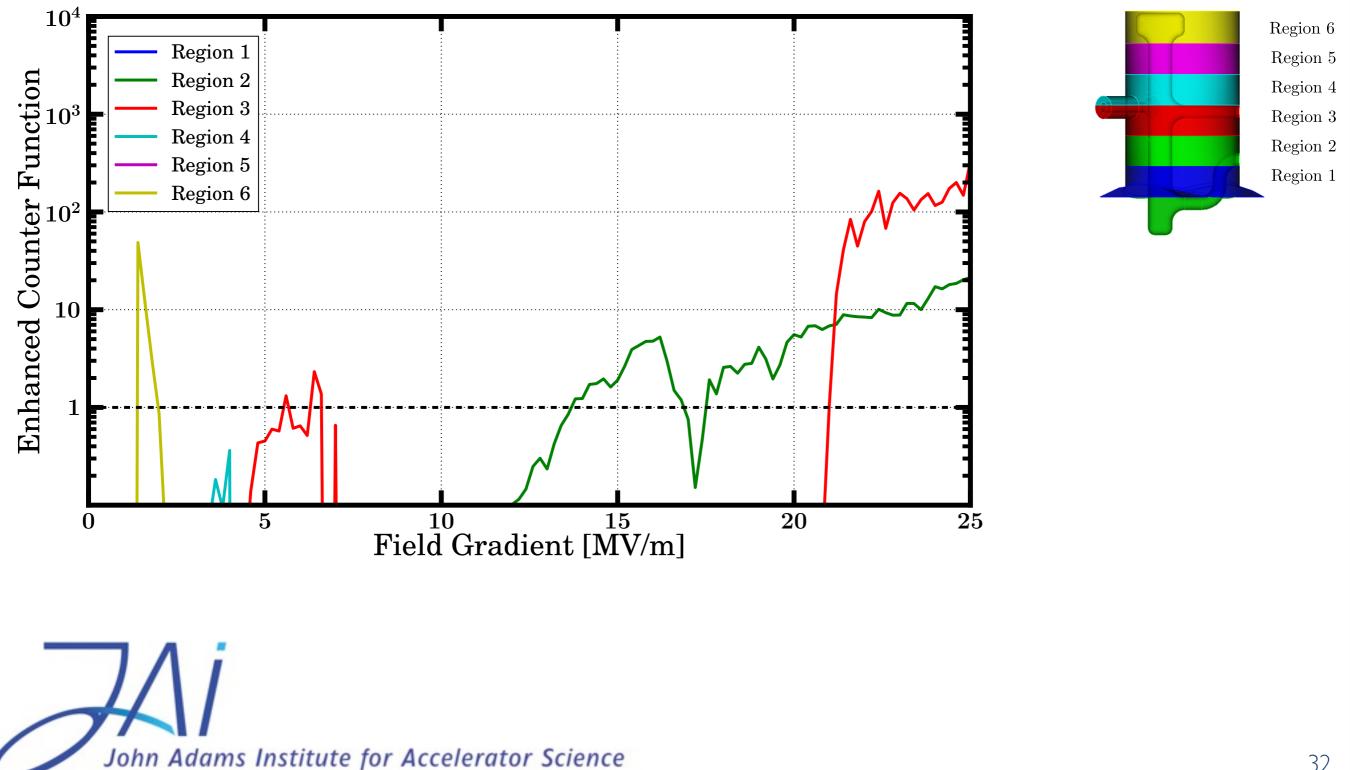
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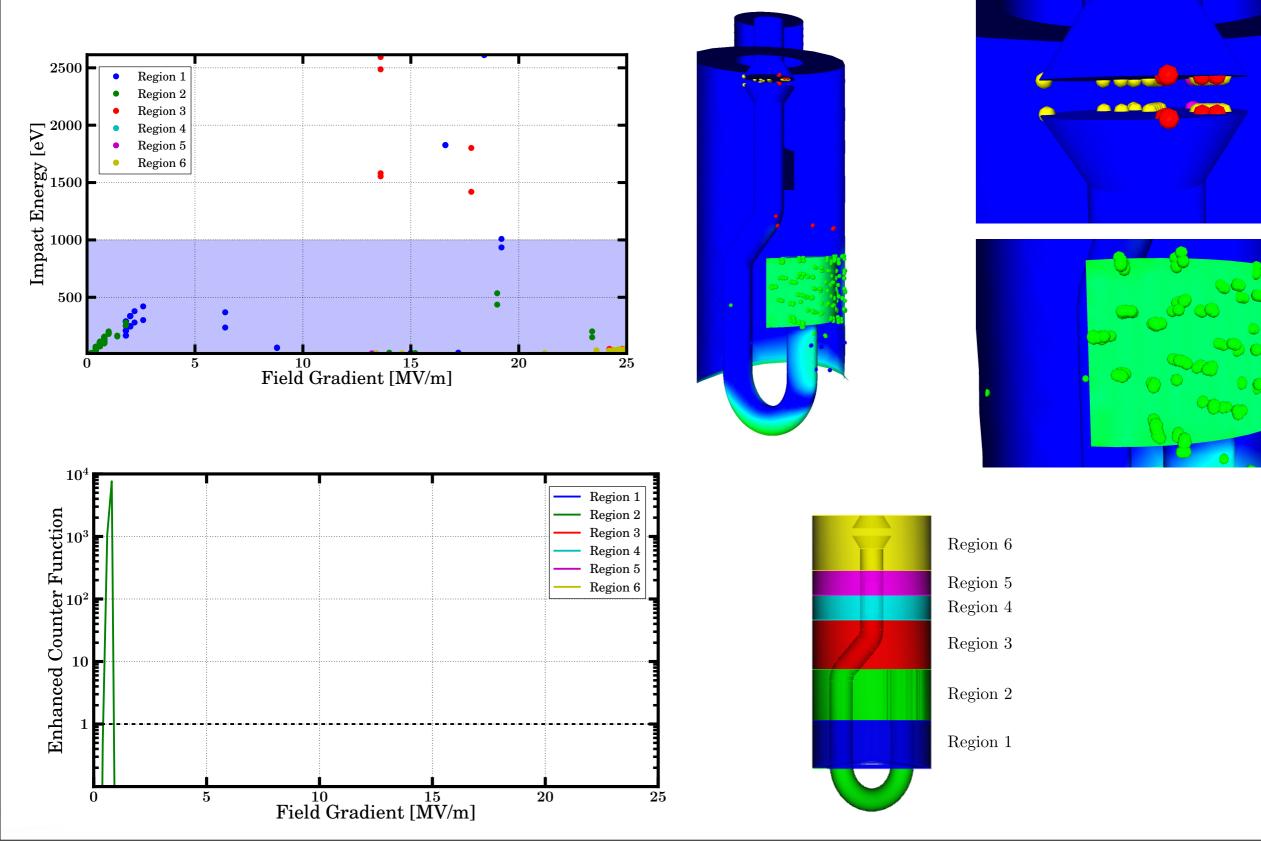




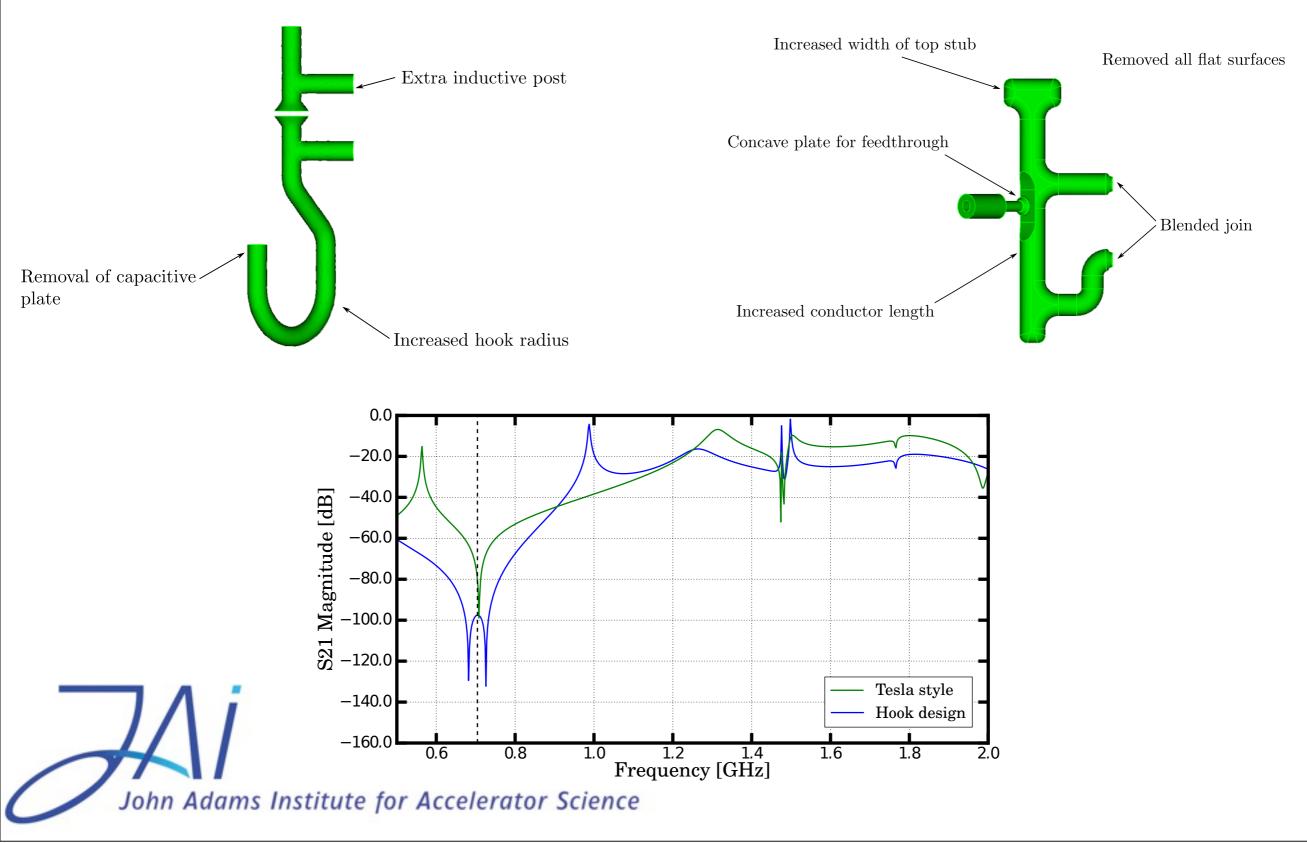
MP IN TESLA STYLE



MP IN ROSTOCK DESIGN



MODIFICATIONS

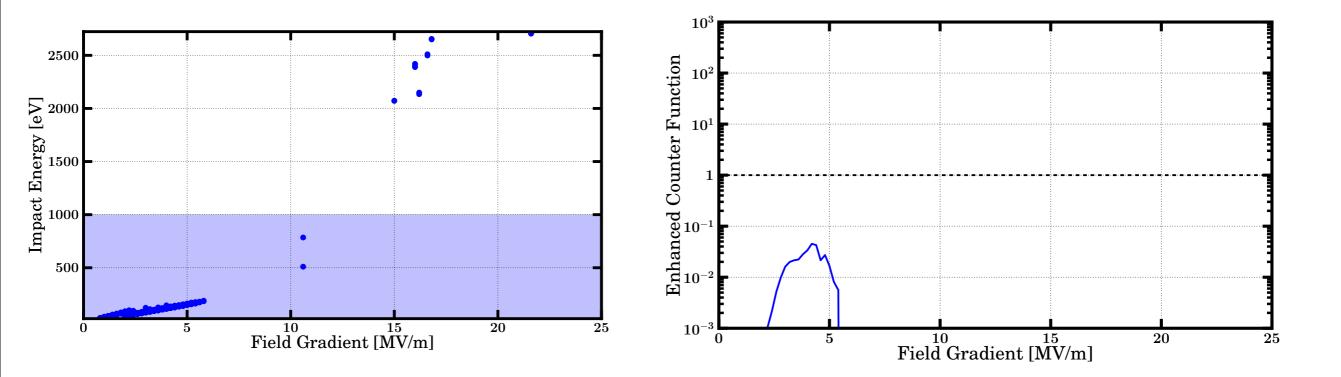


SUMMARY

- SOMs
 - It is possible to design a linac susceptible to SOMs
 - May baseline shows no problems up ~90 mA
- HOMs
 - High R/Q modes are not a concern far from ML
 - $|f_{hom} f_{ml}| > 3 \text{ MHz}$
 - HOM Couplers are not required!
 - →Limits future flexibility (chopping schemes > 100kHz)

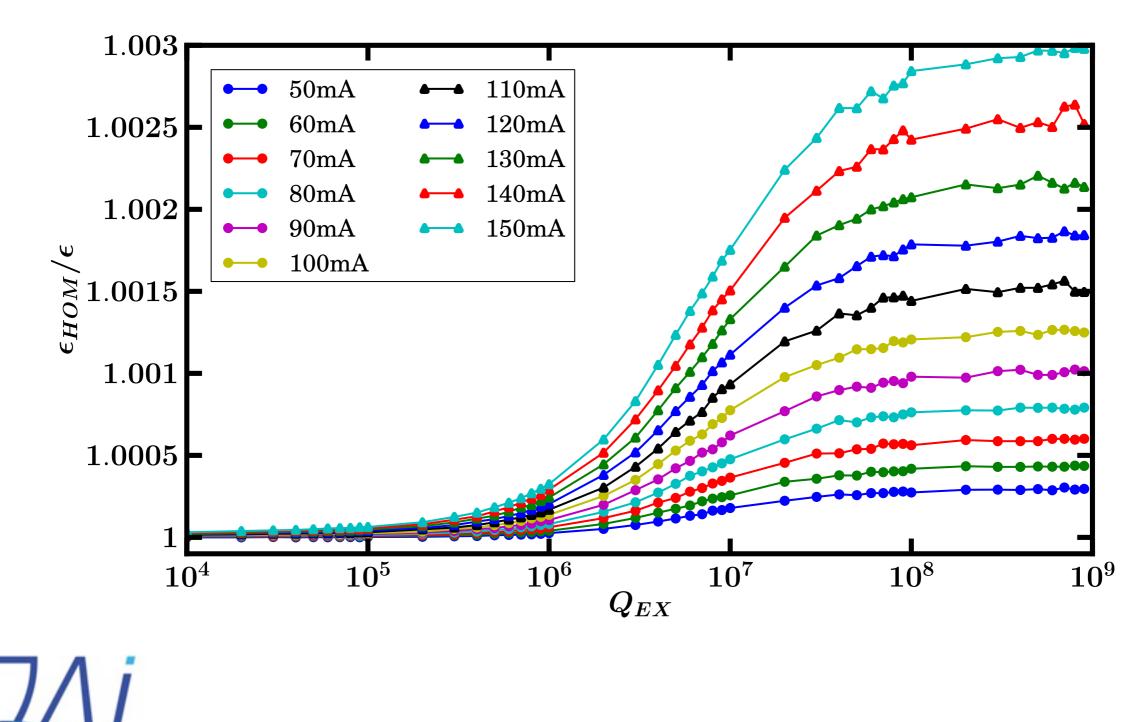
• Modified HOM couplers to reduce multipacting

MODIFIED HOOK



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TRANSVERSE



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