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Chopping and Transport of Low-Energy Ion Beams for FRANZ

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Outline

1) Introduction: Neutron Production

2) Overview: The FRANZ Facility

3) LEBT and Chopper System
   a) E×B Chopper Concept
   b) Numerical Simulations
   c) Experimental Results

3) Conclusion

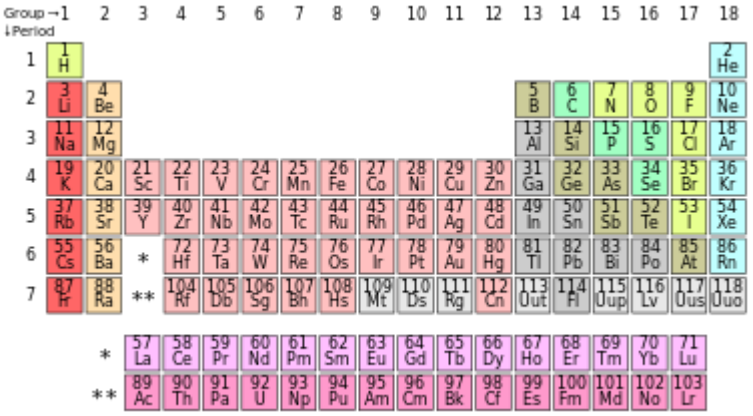
Introduction: Neutron Research

- Material Science
- Sensitivity for magnetic properties
- High penetration depth in material
- Sensitivity for different isotopes
- Sensitivity to light elements (e.g. hydrogen)
- Neutron imaging
- Test radiation durability (detectors, fusion materials)
- Cancer treatment (BNCT)
- Neutron capture process relevant for ADS, nuclear astrophysics, …

Introduction: Nuclear Astrophysics

Stellar nucleosynthesis:

- About 50% of the element abundances beyond iron are produced via the s-process.
- s-process takes place in AGB stars.
- Neutron temperature: $k_B T$ = 8 to 90 keV [Reifarth et al., 2014].
- Modelling requires neutron capture cross-sections from 1 to 400 keV.

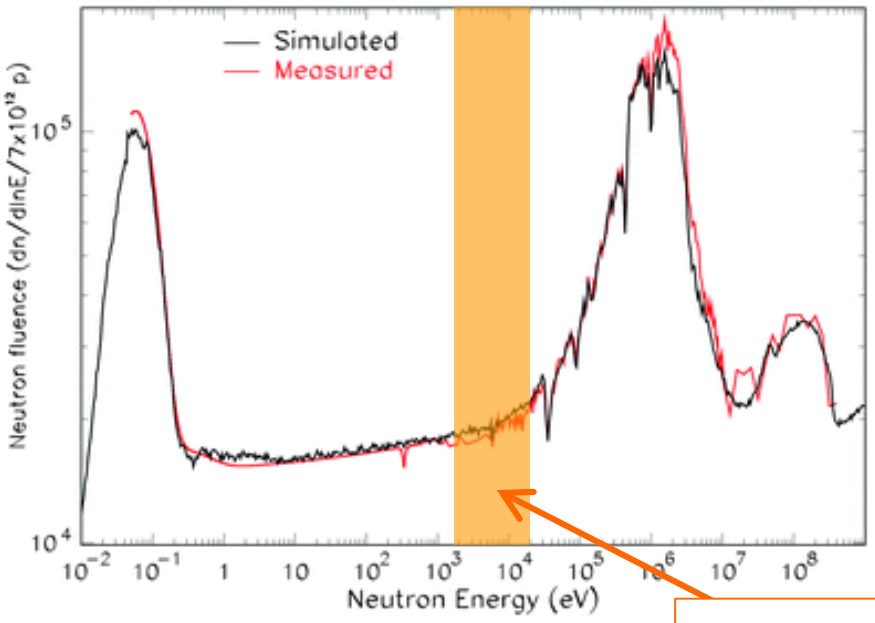


Introduction: Neutron Production Facilities

	Fission Reactors	Spallation Sources	Small-Scale Accel.-Driven Facilities
Typical production mechanism	fission of ^{235}U	high energy protons (100s MeV to GeV) on heavy metal target.	protons/deuterons (several MeV) on Li or Be target.
Costs	> 100 M€	> 1 G€	$\sim 1 \ldots 10$ M€
Neutron flux	high (average) flux $\approx$ 1e15 $\frac{n}{s \cdot cm^2}$	High (peak) flux $=$ 4e16 $\frac{n}{s \cdot cm^2}$ (ESS)	Moderate flux $<$ 1e7 $\frac{n}{s \cdot cm^2}$
Time structure	challenging	CW (SINQ), short pulse (SNS), long pulse (ESS)	CW to short pulsed
Neutron energy	MeV, moderated to thermal spectrum	$W_n < W_p$ (emerging particles); $1 \ldots 10$ MeV (evaporating particles)	$1 \ldots 500$ keV
Angle distribution	isotropic	forward / isotropic	kinematic collimation

Neutron Energy Spectrum

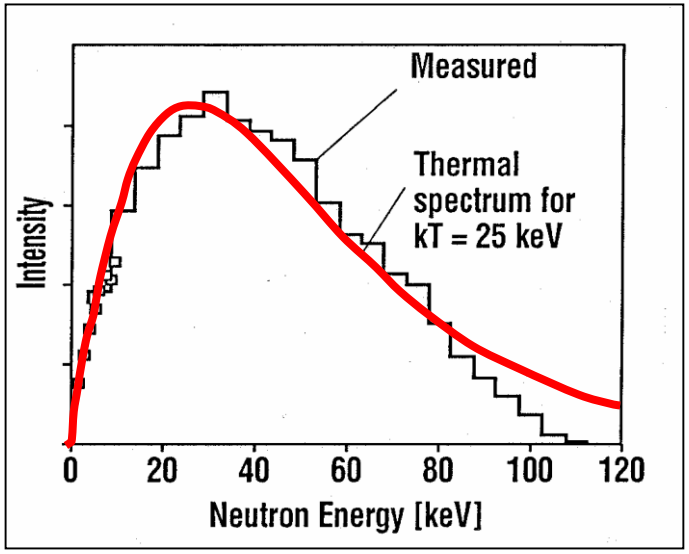
Spectrum from Spallation Source (20 GeV protons on Pb target)



Measured at n-TOF, CERN (flight path: 200m) [Colonna et al., 2010].

n energy: 1…100 keV

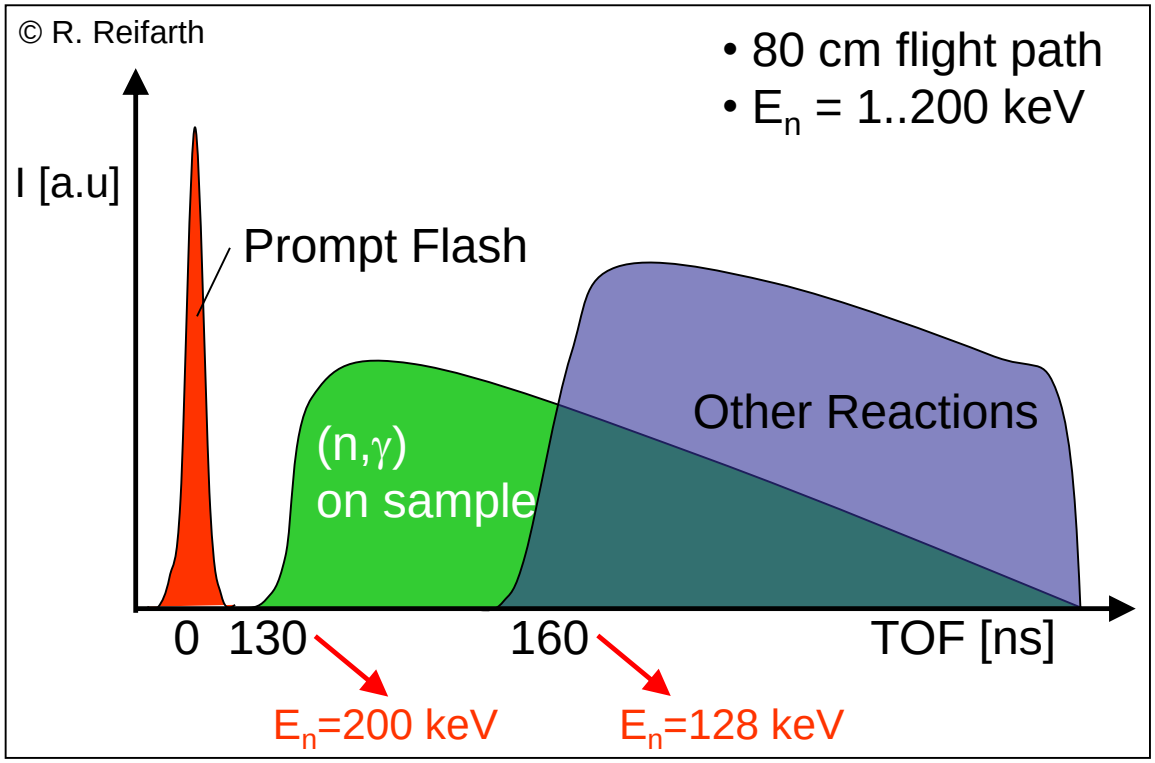
Spectrum from small-scale facility using the $^{7}\mathrm{Li}(\mathrm{p},\mathrm{n})^{7}\mathrm{Be}$ reaction.

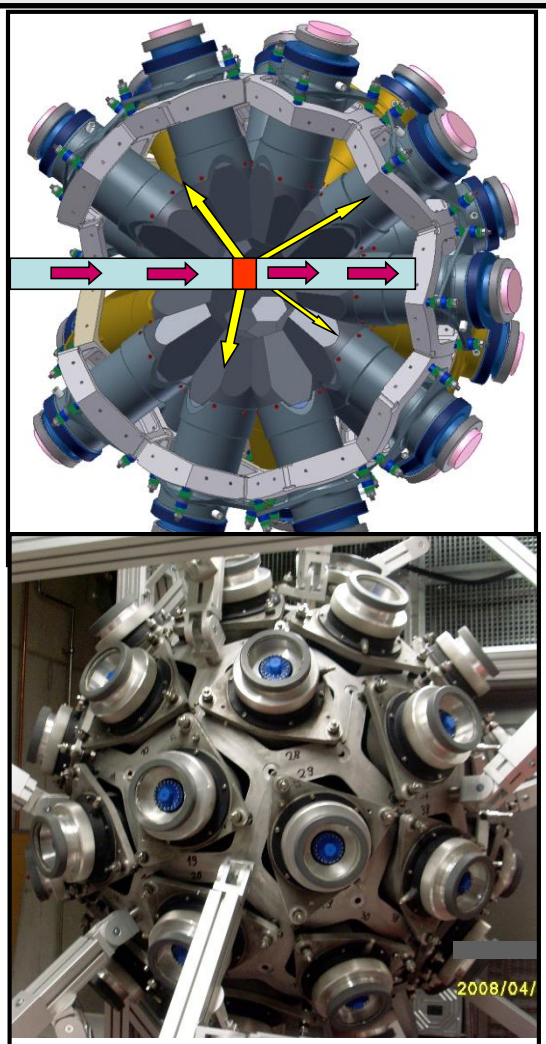


Measured at FZ Karlsruhe for a primary proton energy of 1.991 MeV (flight path: 0.8m) [Beer et al., 2001].

Time-of-Flight (TOF) Method

- TOF method allows to measure the neutron capture cross-sections as a function of the neutron energy.
- Pulsed primary beam and fast (<1 ns) gamma calorimeter required.
- Adequate neutron spectrum assures low background.





4π BaF_2 detector at Frankfurt.

Frankfurt Neutron Source FRANZ

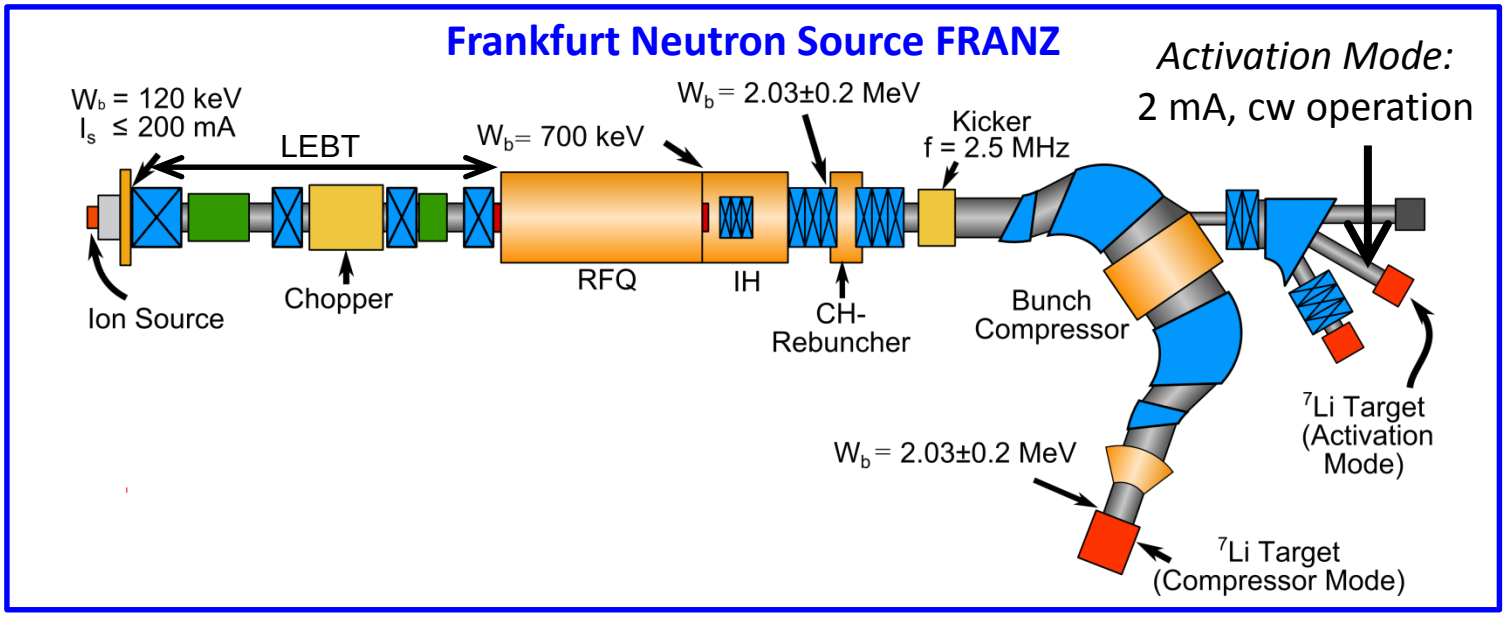
FRANZ is currently under construction at Frankfurt University:

- Deliver neutrons for nuclear astrophysics and material sciences
- Accelerator test bench
- Education of students in accelerator physics

Experimental Hall, IAP

Physics Building, Goethe-Universität Frankfurt

Frankfurt Neutron Source FRANZ



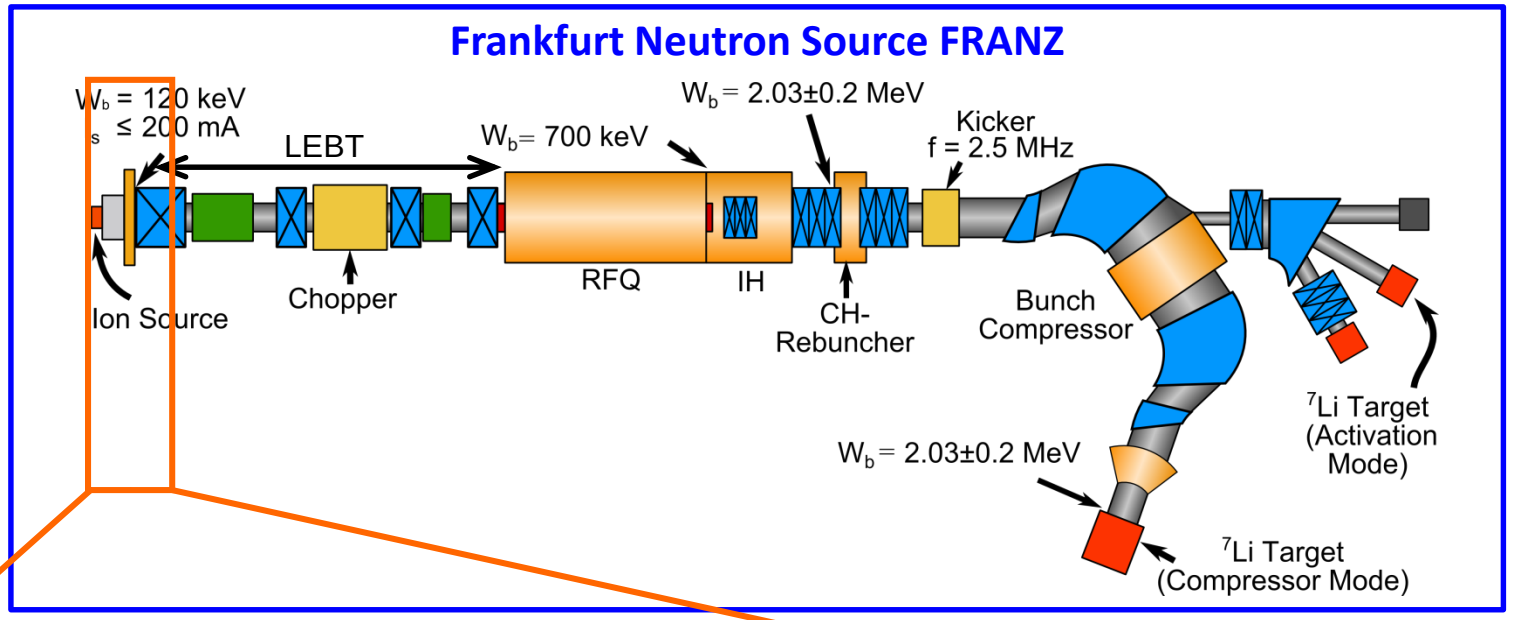
Goal in *Compressor Mode*:

- Deliver a high (peak) neutron flux,
- produced via the ^{7}Li(p,n)^{7}Be reaction,
- for the energy-dependent measurements of n-capture cross sections (using TOF).

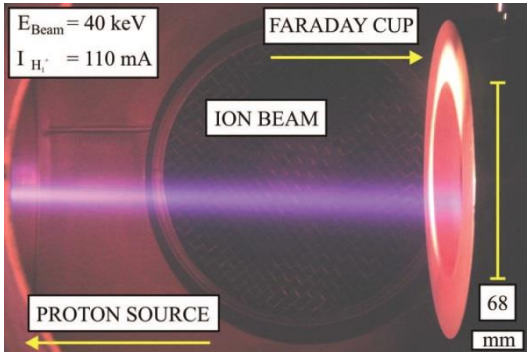
This requires a primary proton beam

- with high intensities (50-200 mA),
- at 2 MeV beam energy,
- with a challenging time structure (1 ns, 257 kHz).

Frankfurt Neutron Source FRANZ



High-Current Ion Source



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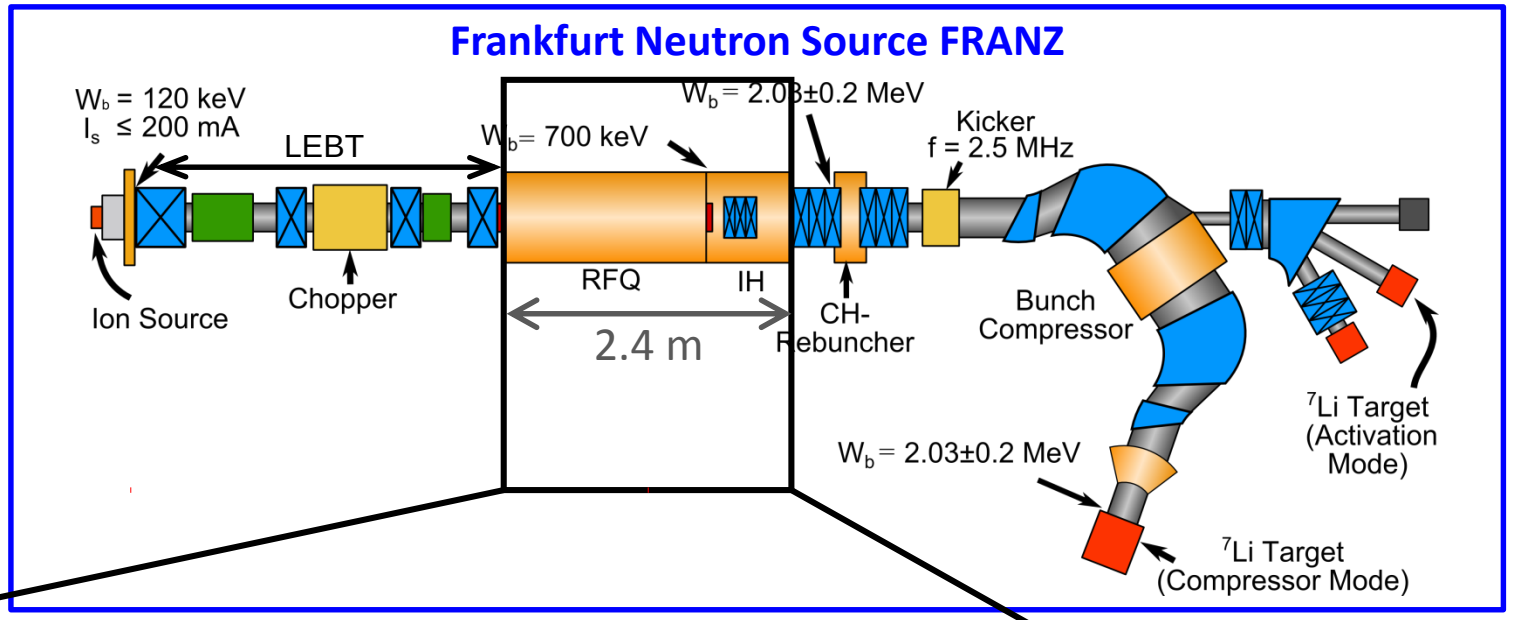
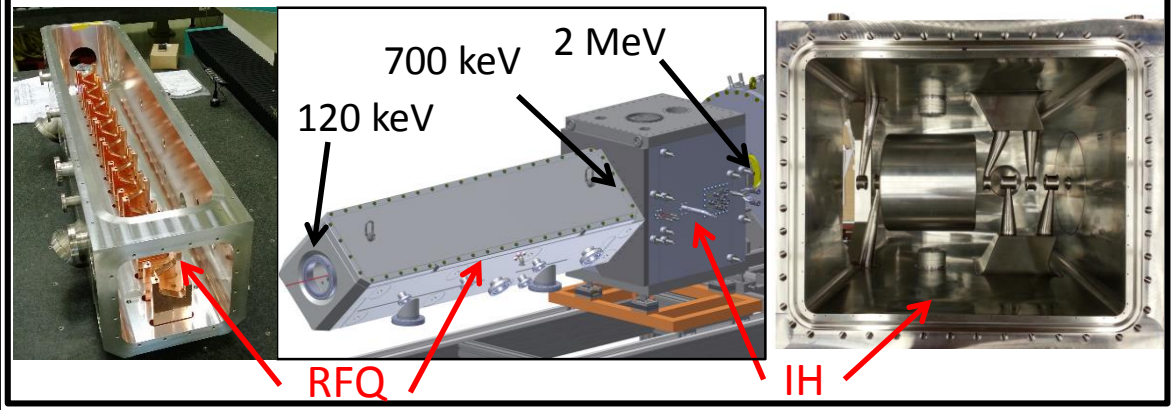
- Arc-discharge driven ion source
- Proton current: 50 mA (240 mA)
- Current density: 480 mA/cm²
- DC operation
- Proton fraction > 90 %
- Beam energy: 120 keV
- $\varepsilon_{rms,\,norm}$ < 0.08 mm· mrad

Frankfurt Neutron Source FRANZ



2 MeV Linac Section



- CW operated
- f_{rf} = 175 MHz
- RFQ under construction
- IH is being copper plated
- RFQ test module tested with P_{rf} ≈ 115 kW/m

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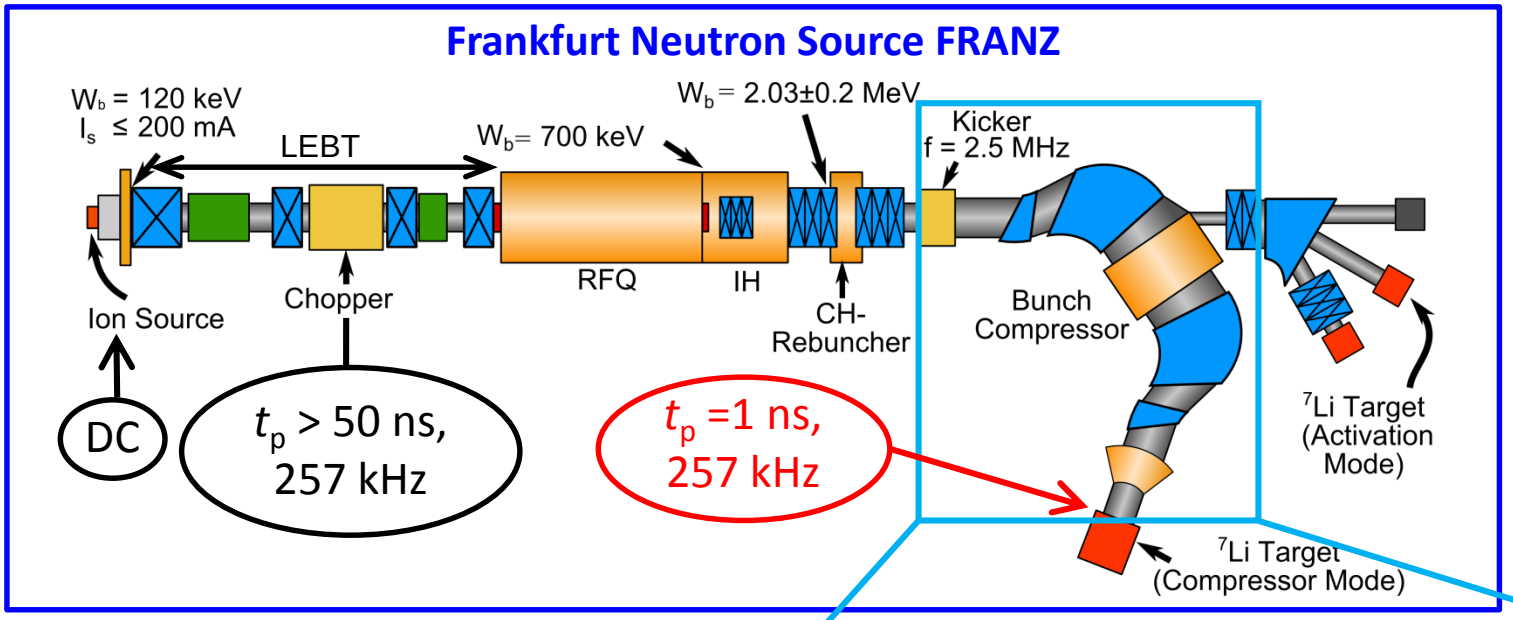
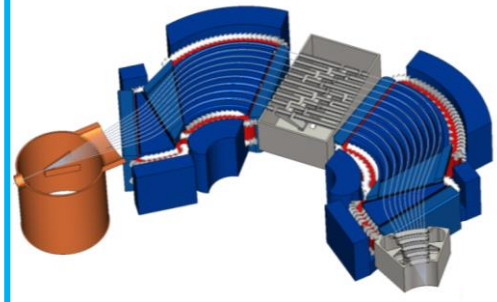
Frankfurt Neutron Source FRANZ



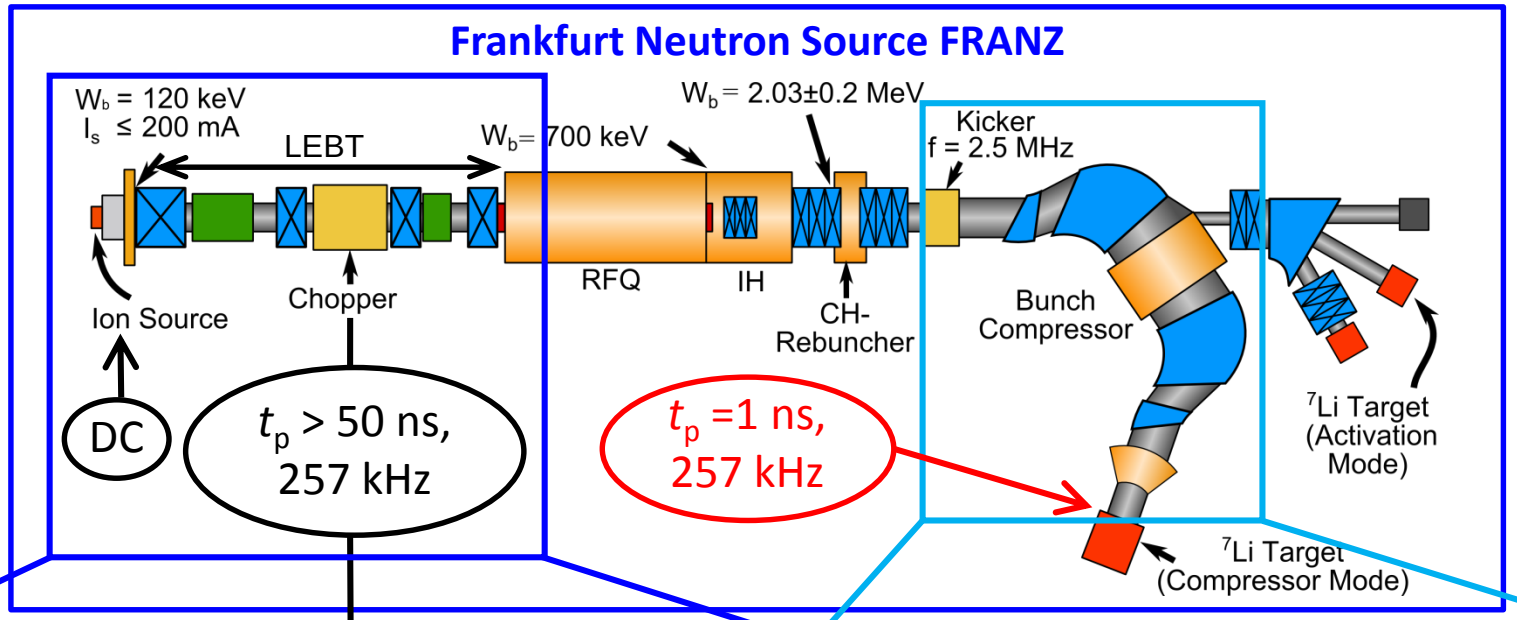
Bunch Compressor

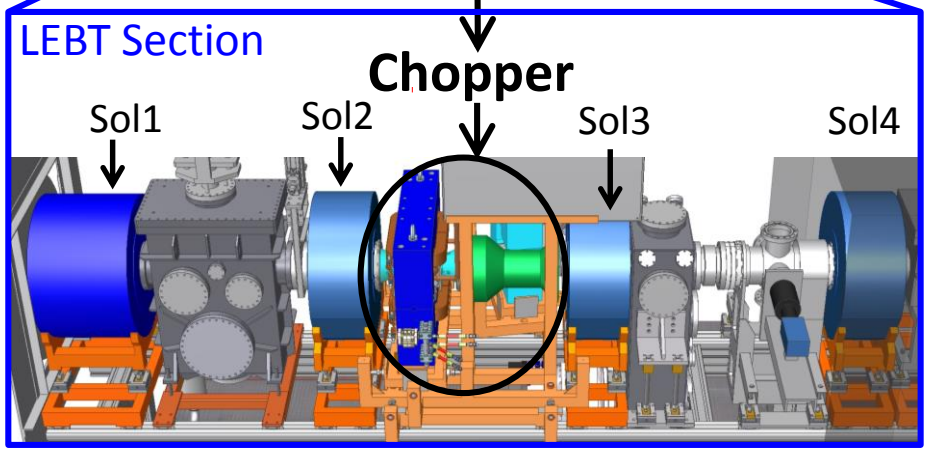


- Mobley Type
- Electric Kicker (f = 2.5 MHz)
- Magnetic Guiding System
- Rebuncher Cavities

L. P. Chau et al., LINAC'10, MOP100

Frankfurt Neutron Source FRANZ





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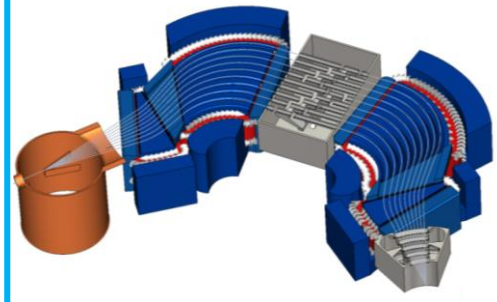

- Mobley Type
- Electric Kicker (f = 2.5 MHz)
- Magnetic Guiding System
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L. P. Chau et al., LINAC'10, MOP100

E×B Chopper: Motivation

Requirements: Chopping a dc beam at
– *low energy* (120 keV)
– *high intensity* (50 mA)
– *high repetition* rate (257 kHz),
– *producing a short beam pulse:* 50 ns / 3.9 µs.

Electric Deflection

Disadvantages: Risk of voltage breakdowns, especially at high beam intensities and especially for a high duty factor of the electric deflection field.

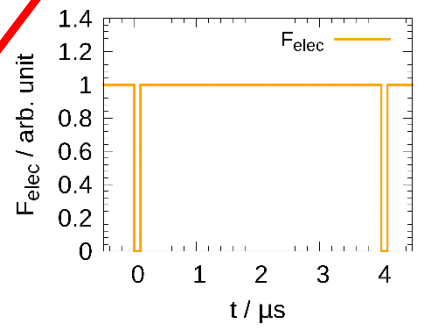
Magnetic Deflection

Disadvantages: High power consumption, especially at high repetition rates.

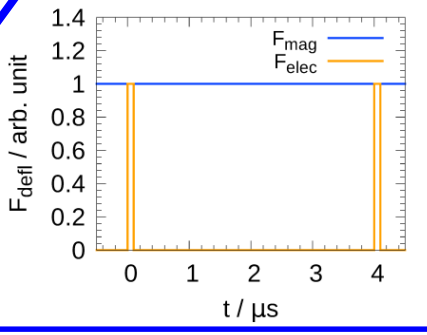
Concept

Combining static magnetic and pulsed electric deflection in an E×B (Wien-filter) field configuration.

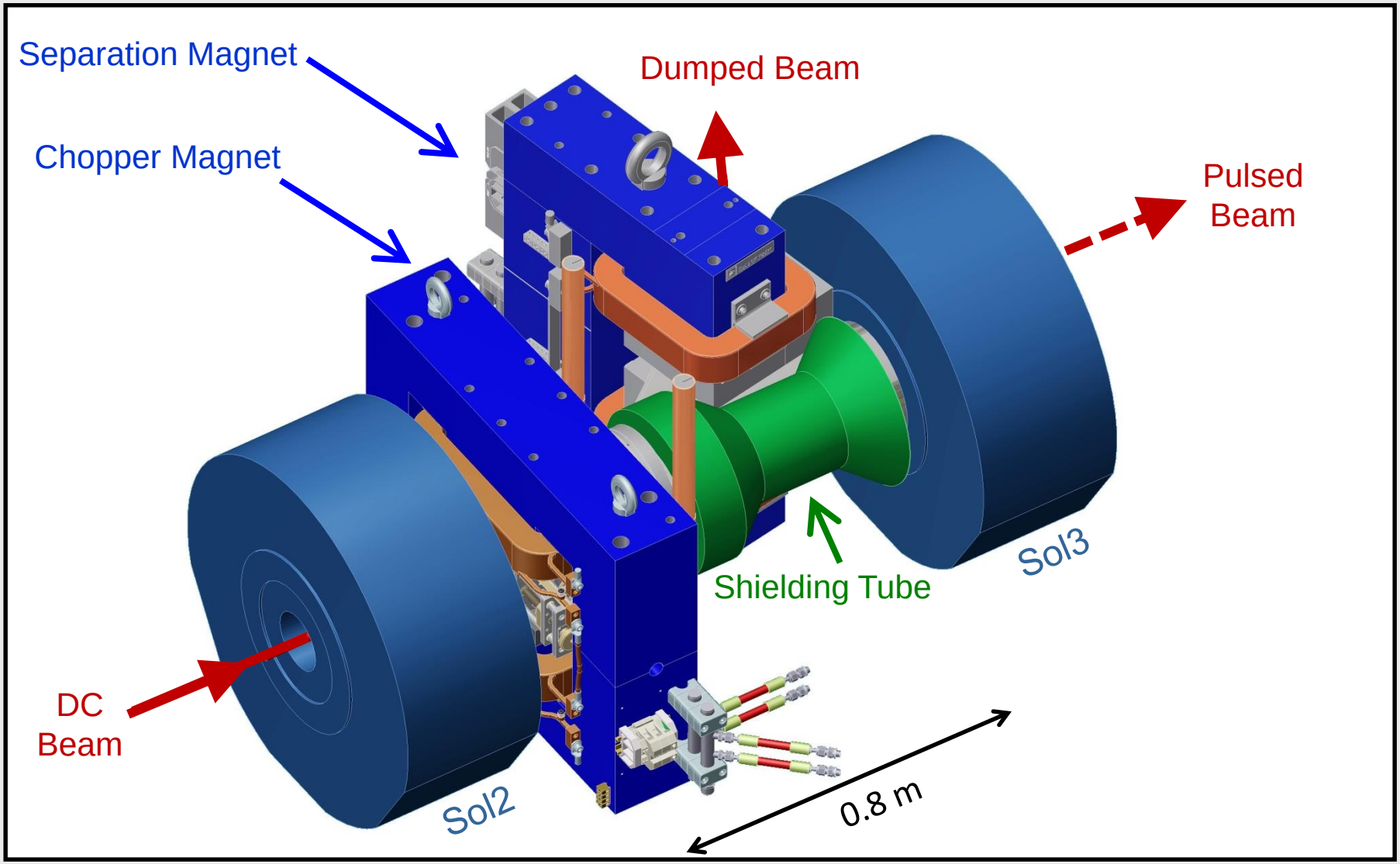
High duty cycle for electric field.



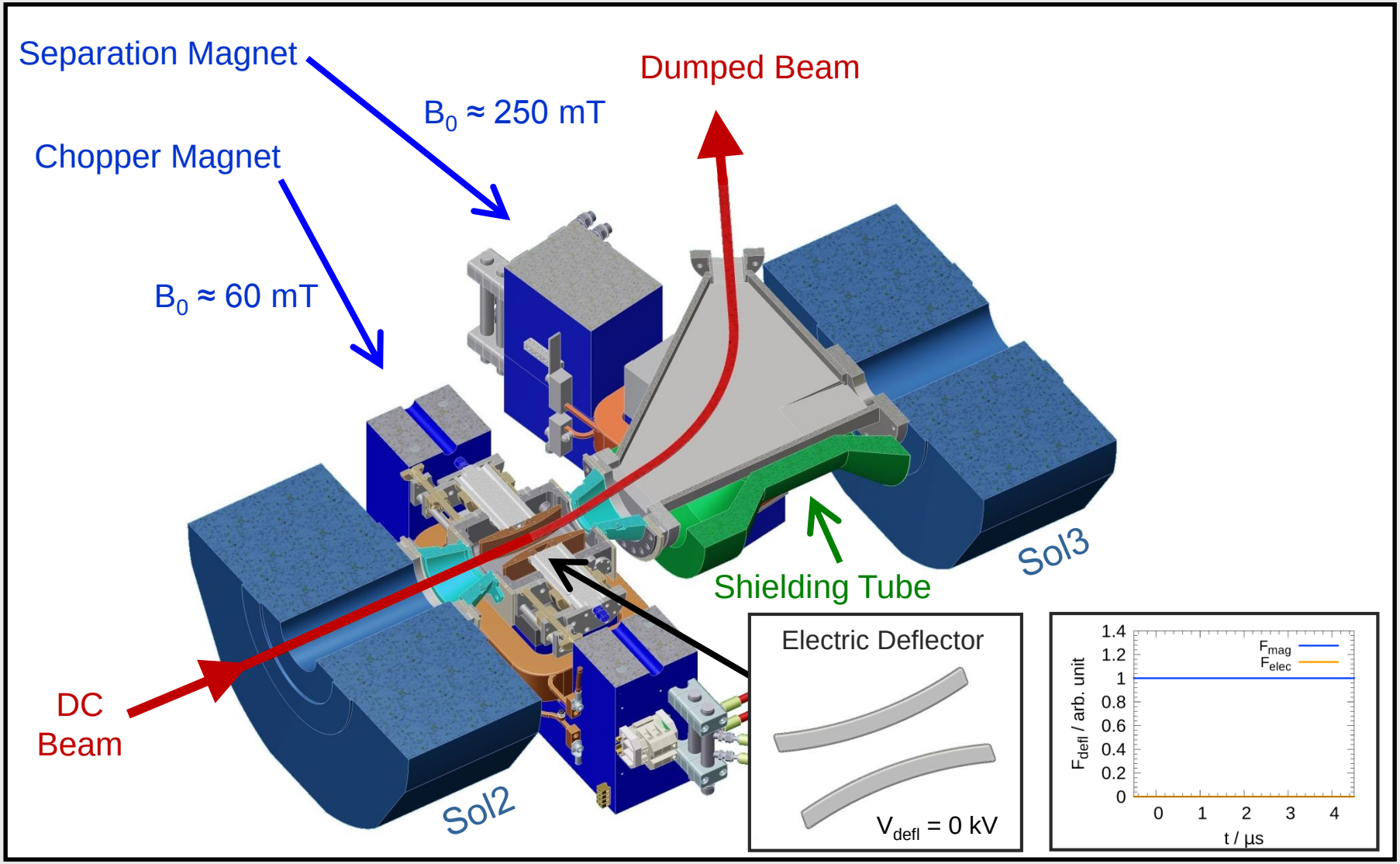
Low duty cycle for electric field.



E×B Chopper: Concept



E×B Chopper: Concept



E×B Chopper: Concept

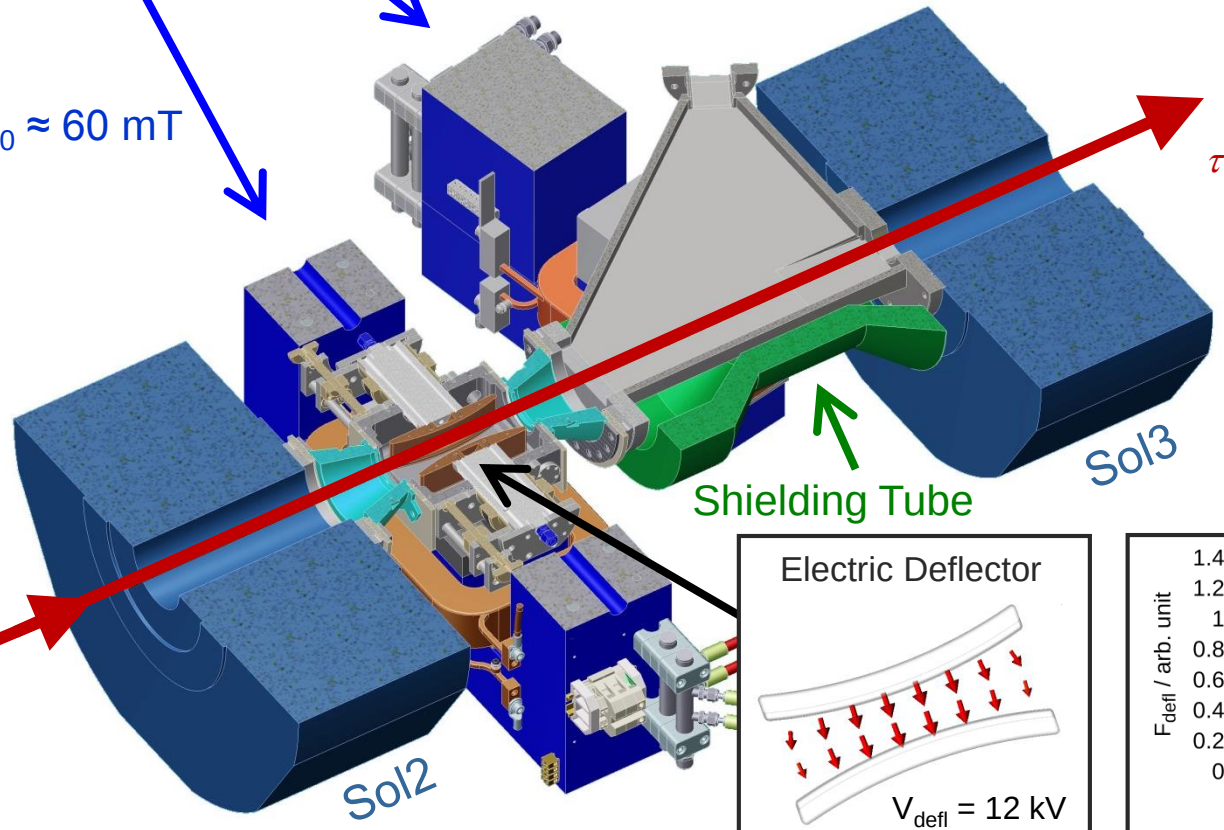
Separation Magnet

$B_0 \approx 250$ mT

Chopper Magnet

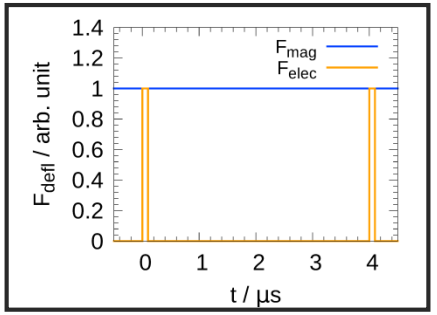
$B_0 \approx 60$ mT

$$\int (\vec{F}_{\mathrm{elec}} + \vec{F}_{\mathrm{mag}})\ \mathrm{d}z \stackrel{!}{=} 0$$



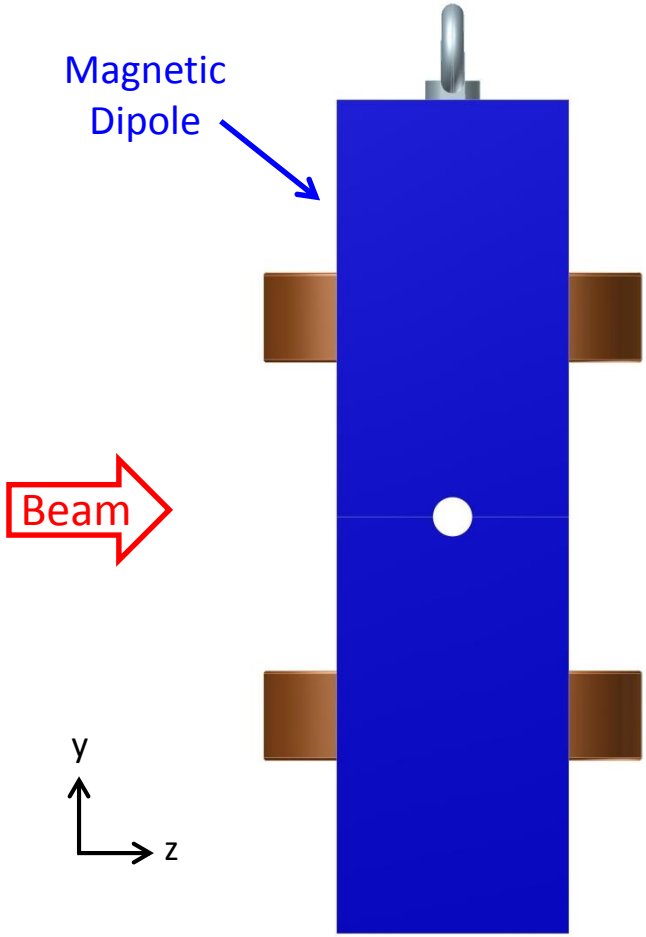
Pulsed Beam,
f_{rep} = 257 kHz,
τ = 50 ns … 350 ns

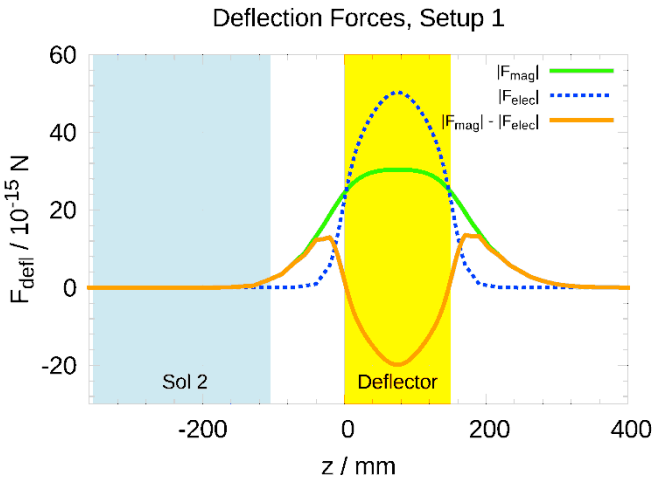
DC Beam

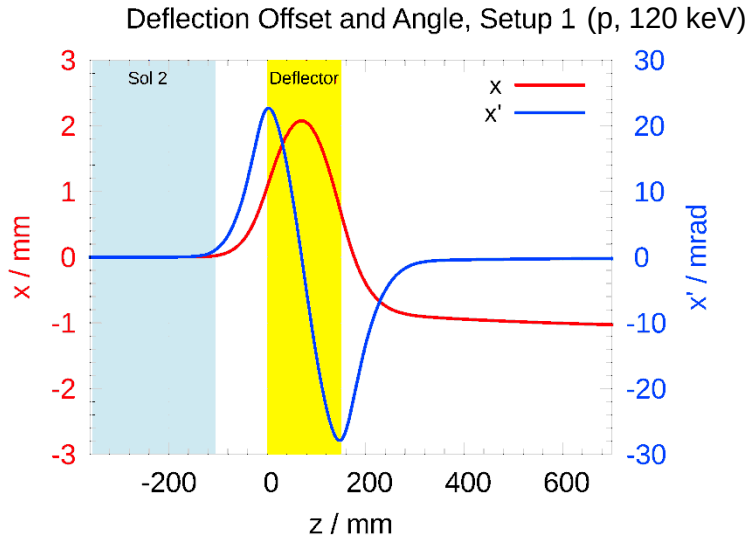


Beam Dynamics in Static E×B Fields

Longitudinal Matching of Deflection Forces







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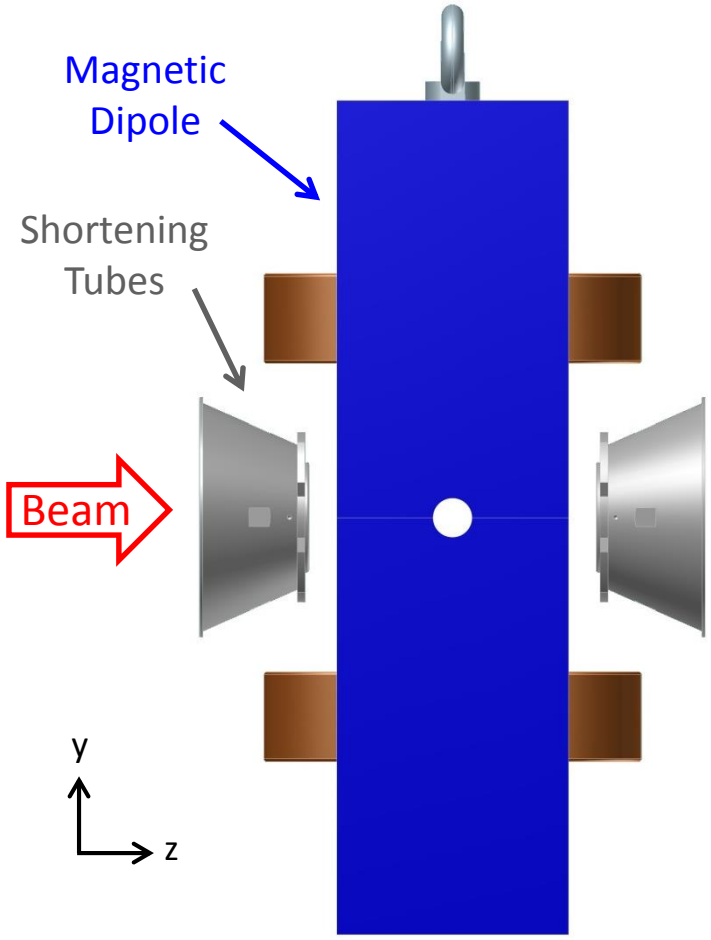

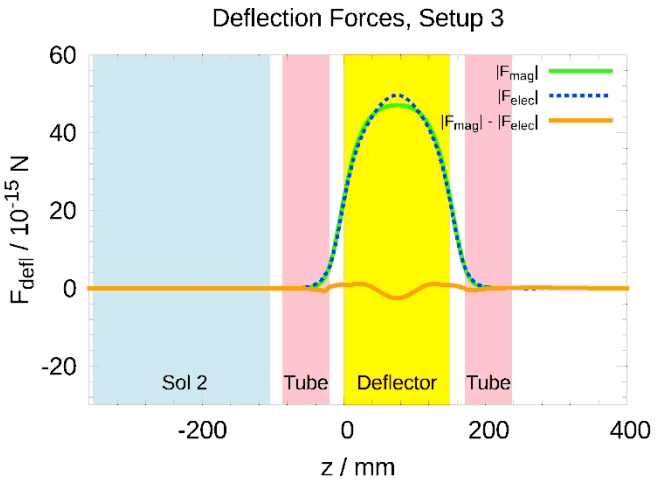

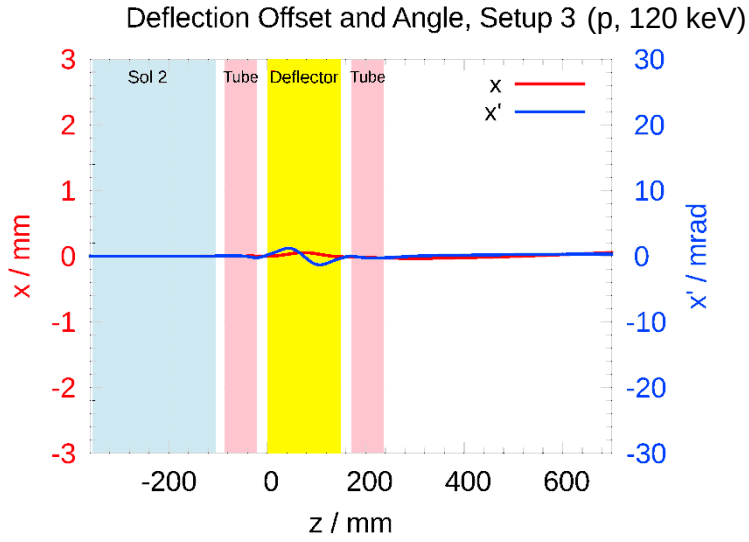

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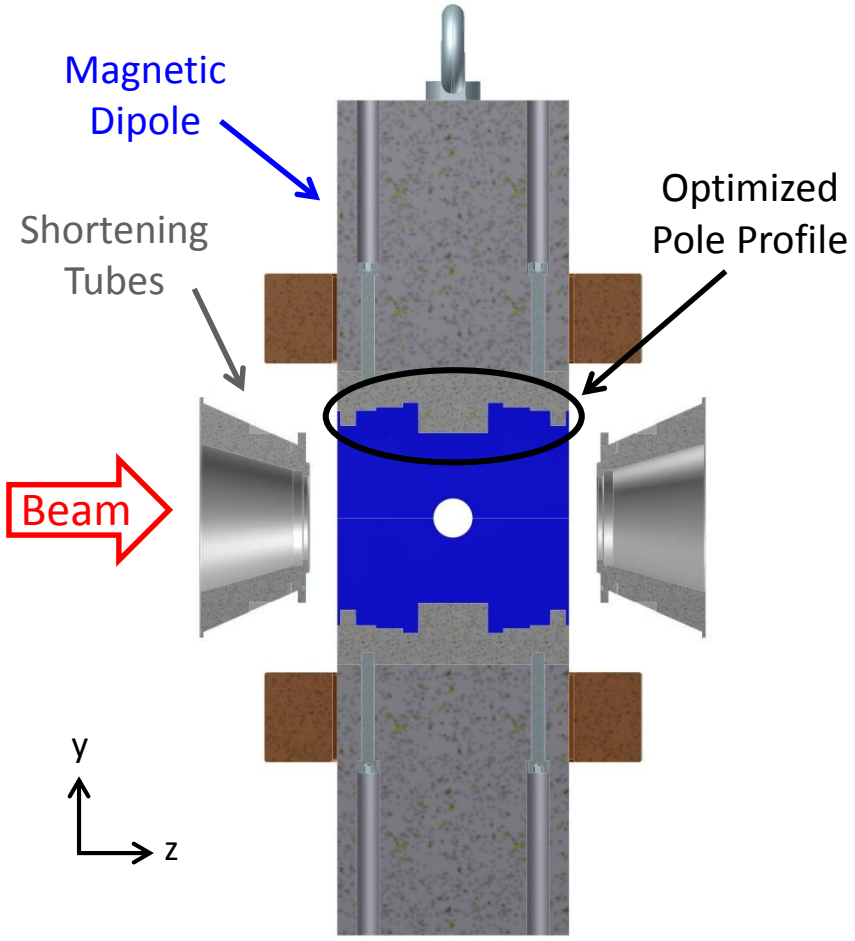
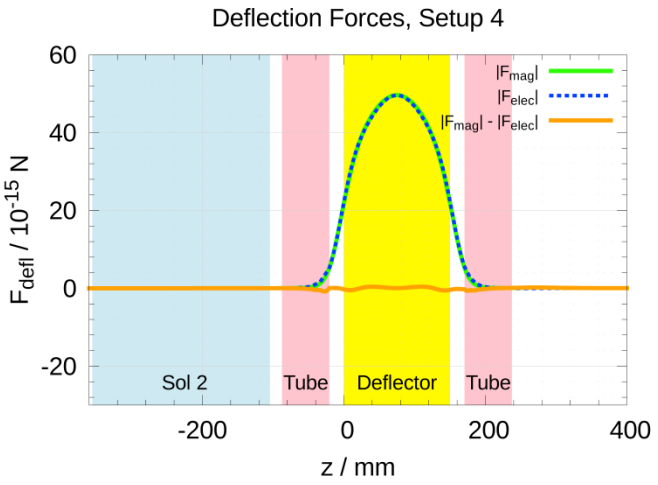
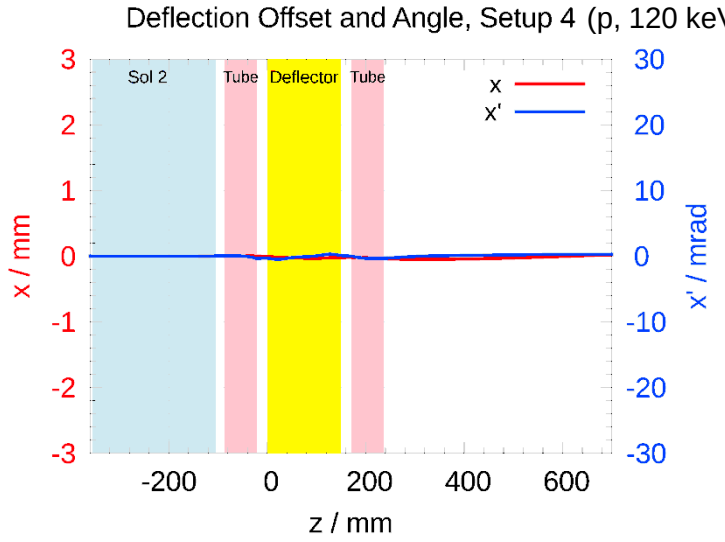
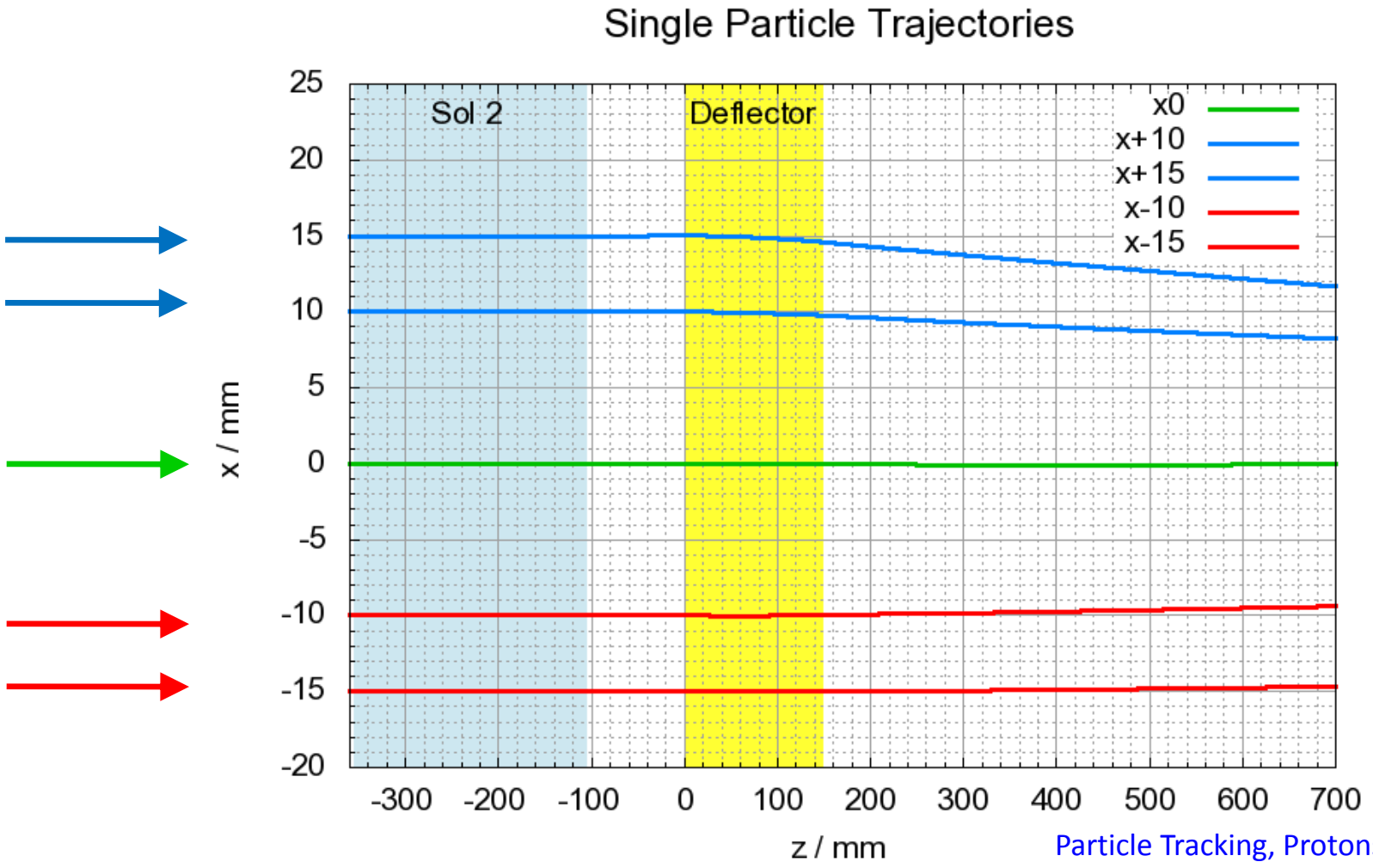






Beam Dynamics in Static E×B Fields

Transverse Matching of Deflection Forces

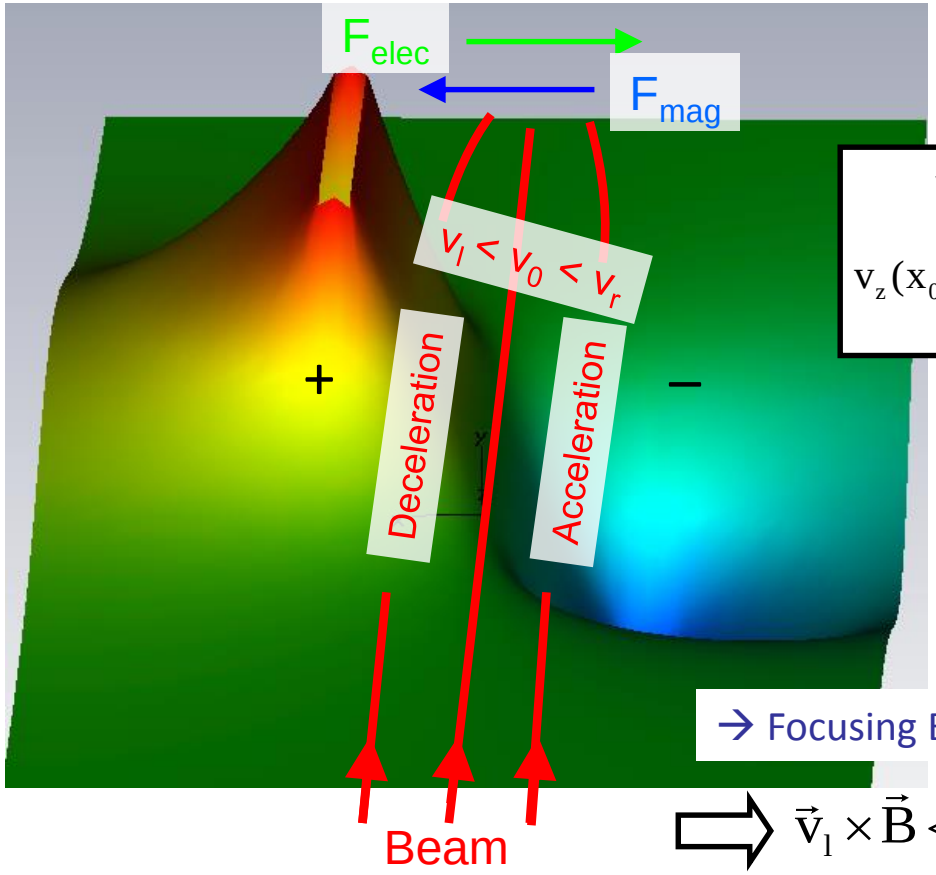


Particle Tracking, Protons, 120 keV.

Beam Dynamics in Static E×B Fields

Effect 1: Wien-Focusing Effect.

$$\int q \cdot (\vec{E} + \vec{v}_p \times \vec{B})\ \mathrm{d}z \stackrel{!}{=} 0$$



Velocity Change:

$$v_z(x_0) = \sqrt{\frac{2e(U_b + E_x x_0)}{m_p}}$$

→ Focusing Effect in *x* direction.

$$\Rightarrow \vec{v}_l \times \vec{B} < \vec{v}_0 \times \vec{B} < \vec{v}_r \times \vec{B}$$

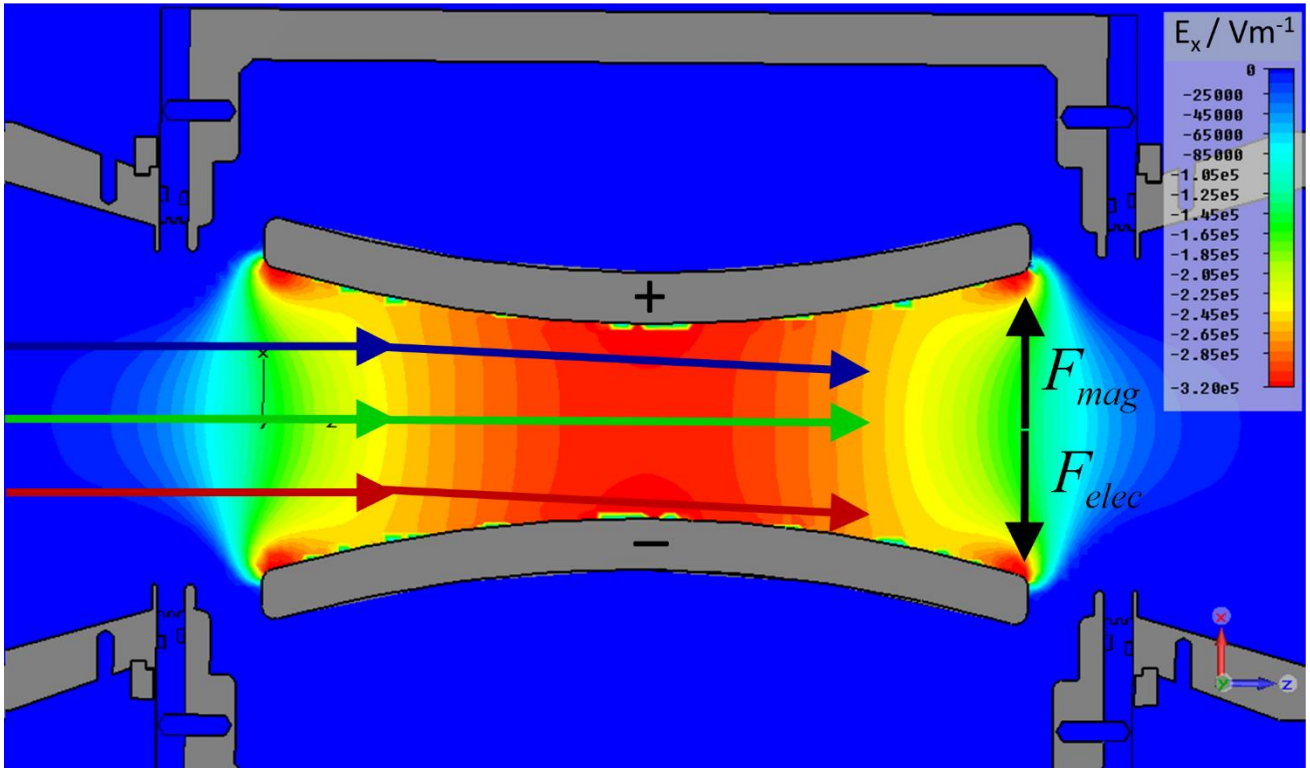
Beam Dynamics in Static E×B Fields

Effect 2: Given inhomogeneous field distribution.

$$\int F_{elec}\, dz\,|_{x=0mm} = \int F_{mag}\, dz\,|_{x=0mm}$$

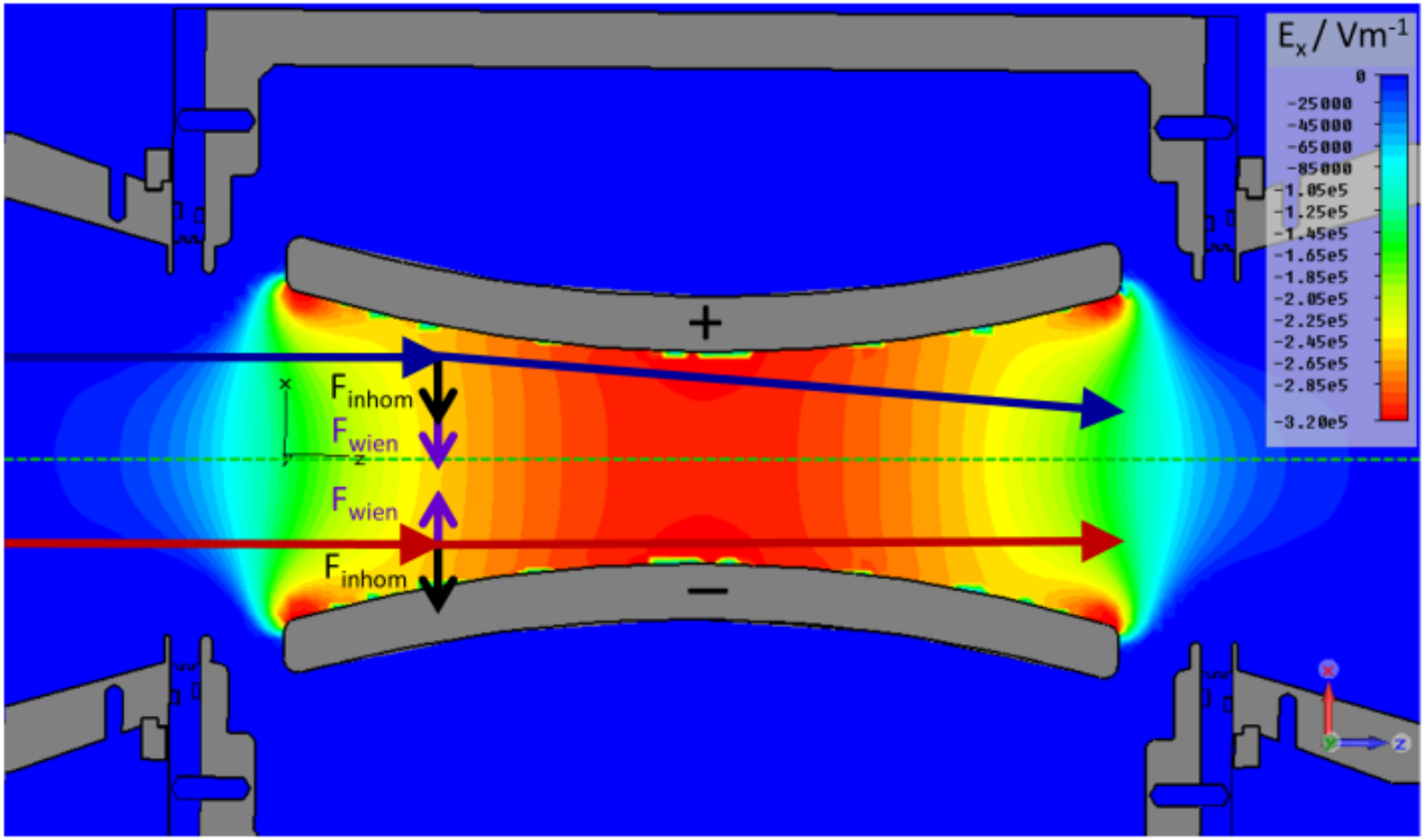
$$\int F_{mag}\, dz\,|_{x=\pm 15mm} < \int F_{mag}\, dz\,|_{x=0mm}$$

$$\int F_{elec}\, dz\,|_{x=\pm 15mm} > \int F_{elec}\, dz\,|_{x=0mm}$$

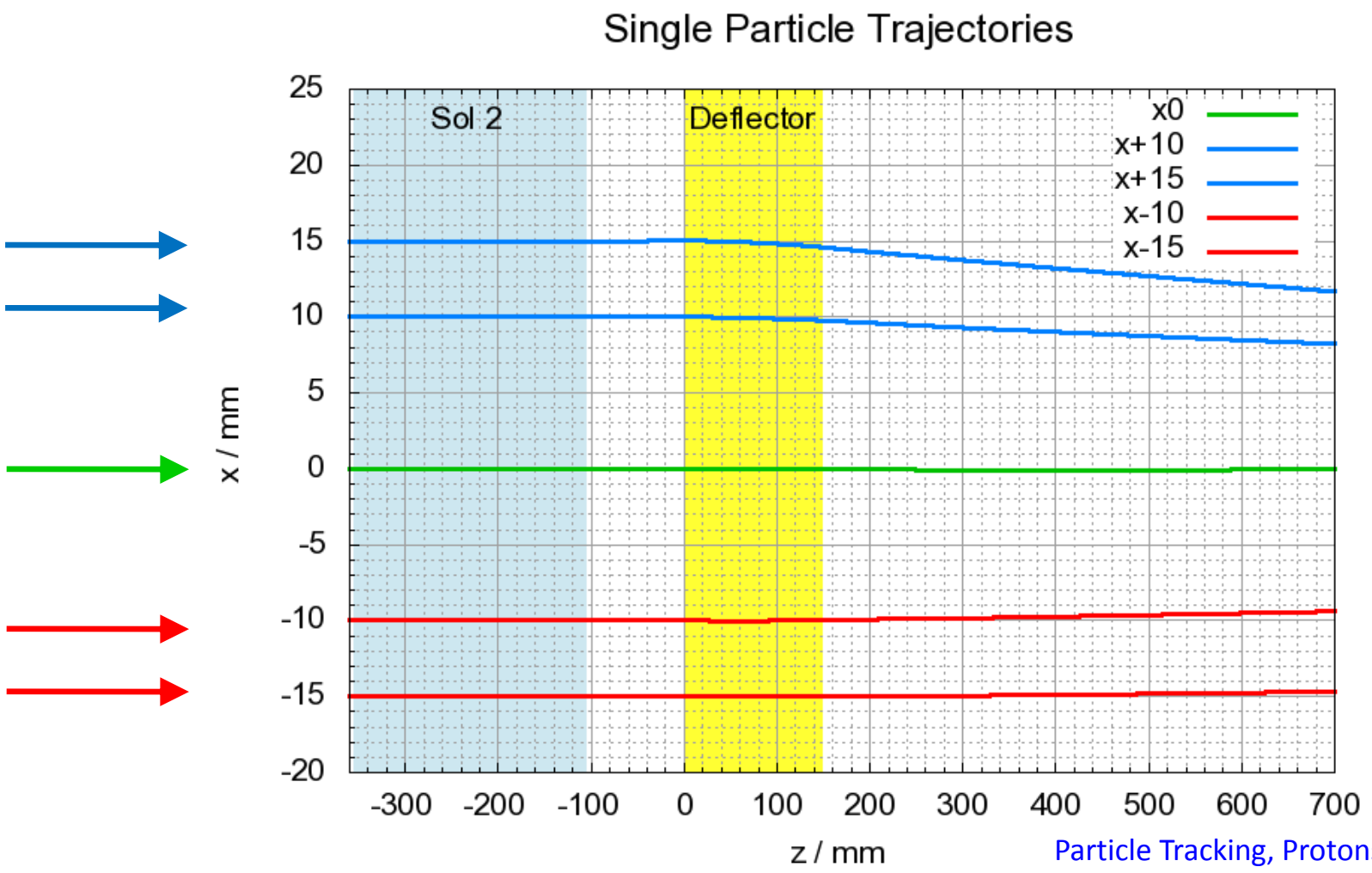


Beam Dynamics in Static E×B Fields

Superposition of both effects.



Beam Dynamics in Static E×B Fields



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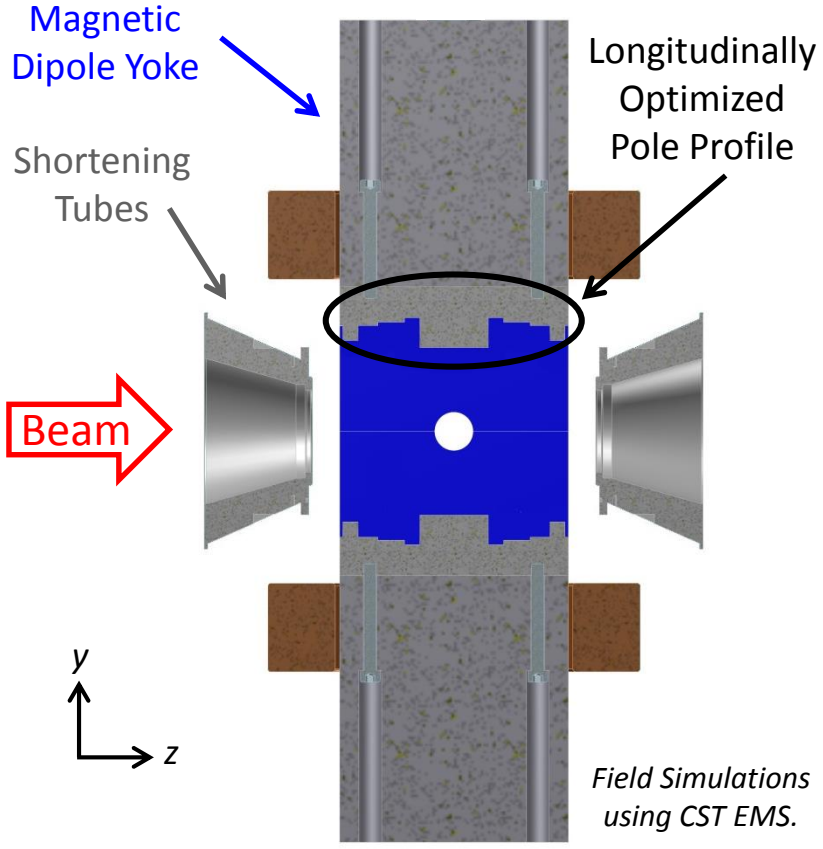
Beam Dynamics in Static E×B Fields

Longitudinal Matching of Deflection Forces



Field Simulations using CST EMS.

- Minimizing horizontal beam movement
- Minimizing position offset

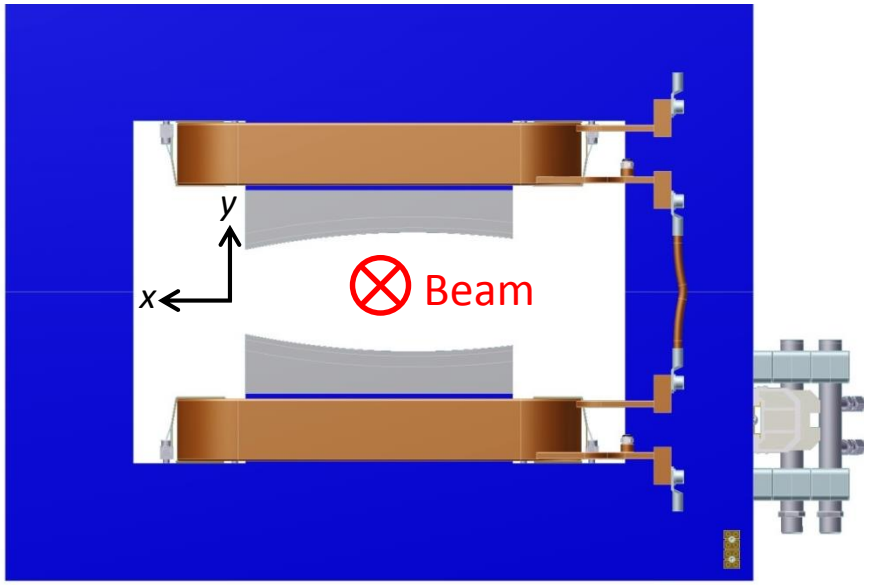
Transverse Matching of Deflection Forces

Optimized Pole Profile:

$$y(x) = \frac{1}{2} h_{gap} \cdot \frac{1}{\sqrt{1 - b \cdot \frac{E_x}{V_{acc}} \cdot x}} - c \cdot x^2$$

Compensation of Velocity Change

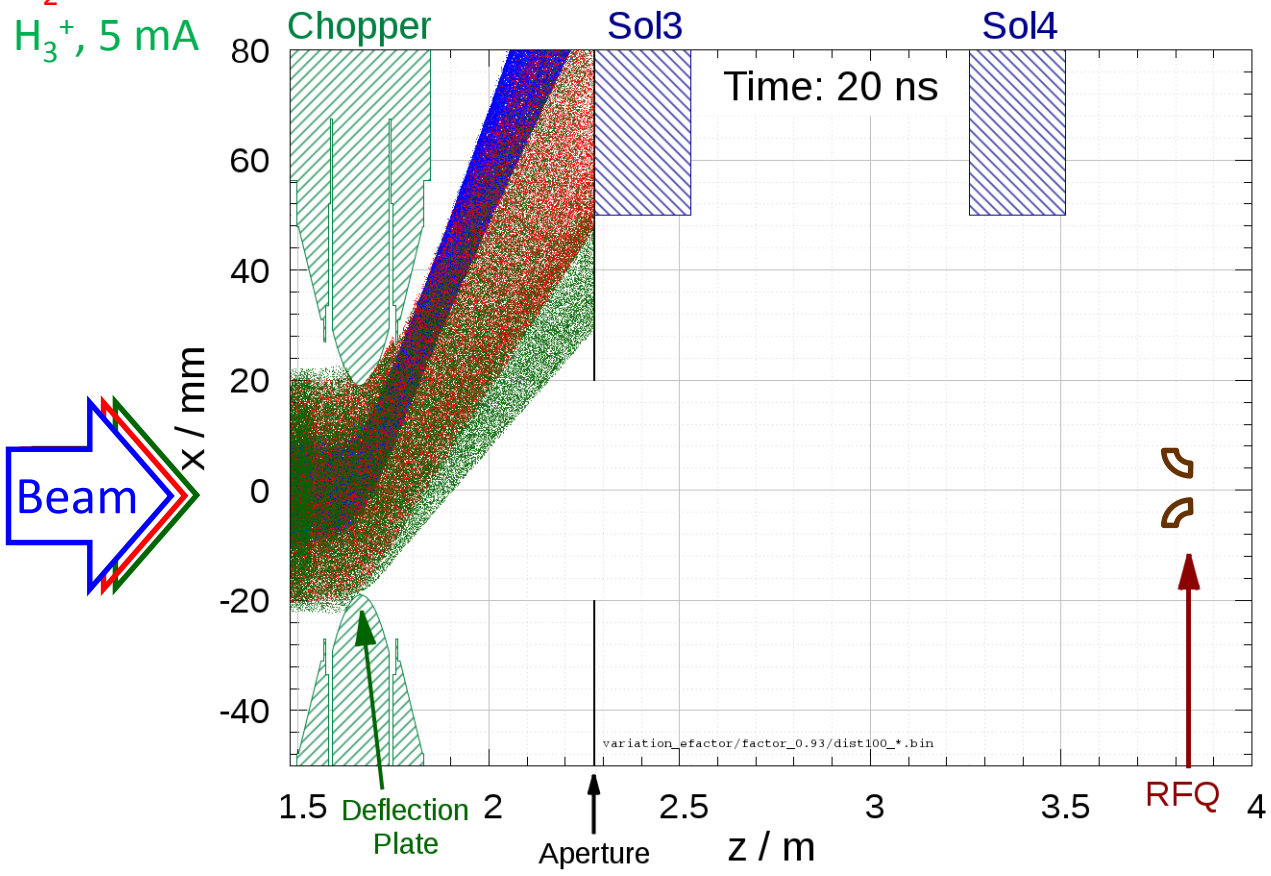
Field Homogenization



- Focusing in both transverse planes
- Preserving cylindrical symmetry

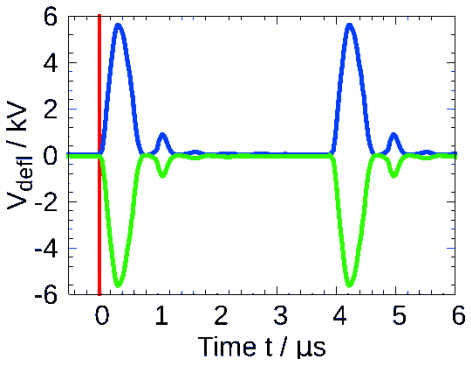
Beam Shaping Simulation

p, 50 mA
H_2^+, 5 mA
H_3^+, 5 mA



Input Data

- W_b = 120 keV
- I_{proton} = 50 mA
- Matched Input Distribution
- 3d *E*-field of deflect. plates
- 3d *B*-field of chopper magnet
- 3d *B*-field of solenoids
- Measured HV Pulse



Beam dynamics calculations using PIC-Code Bender. → By Daniel Noll.

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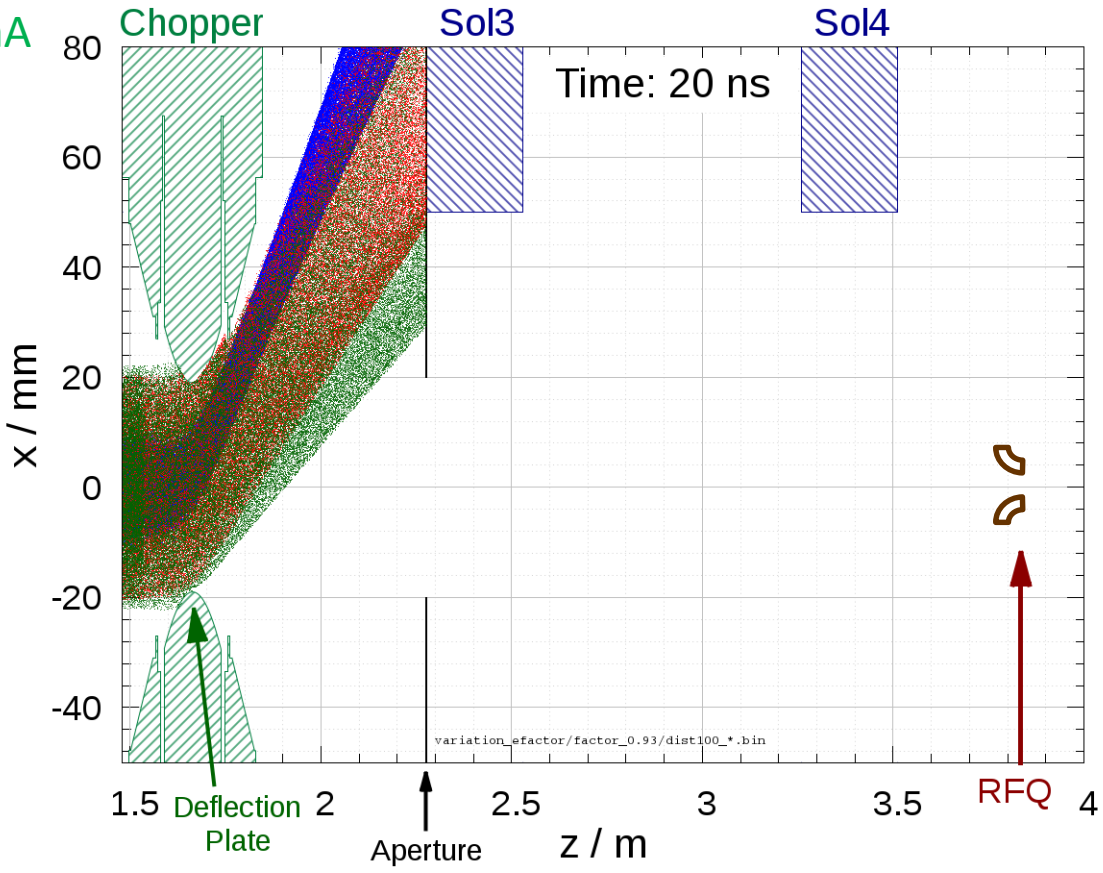
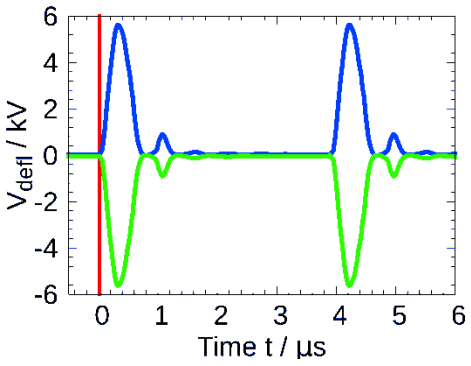


Voltage Pulse



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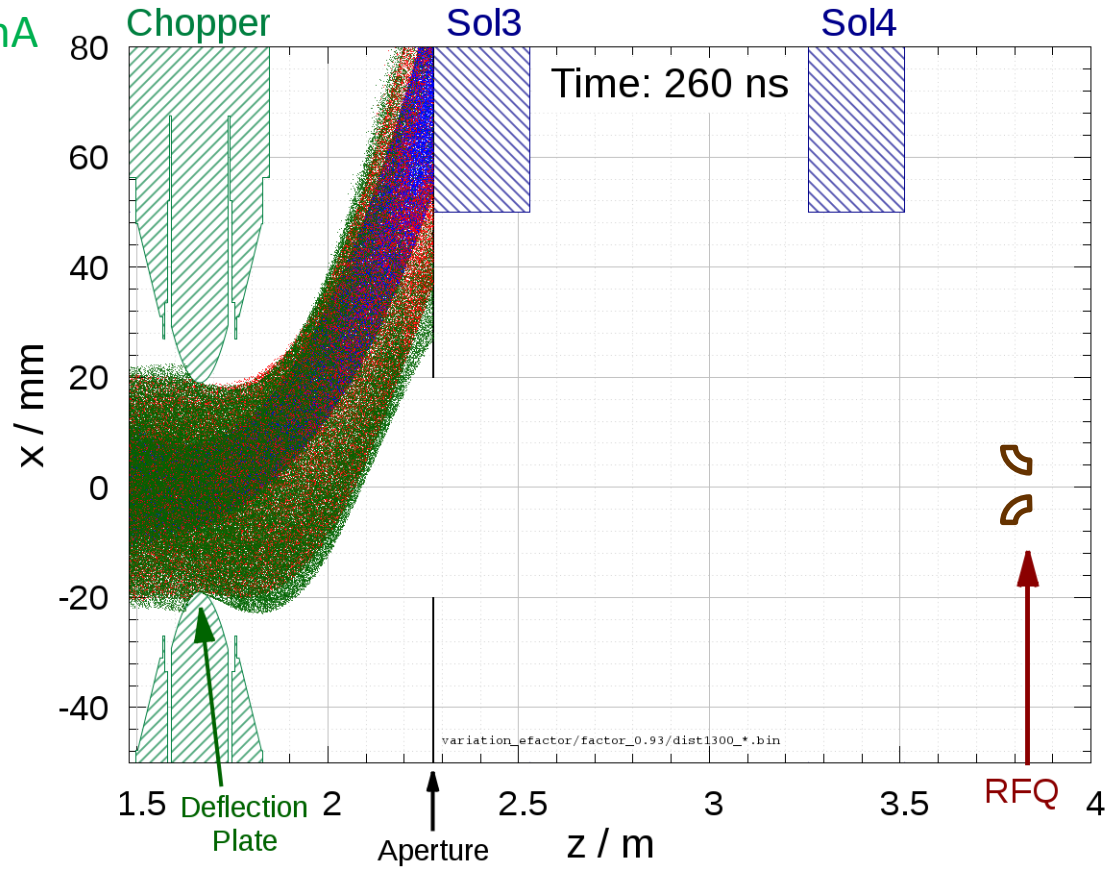

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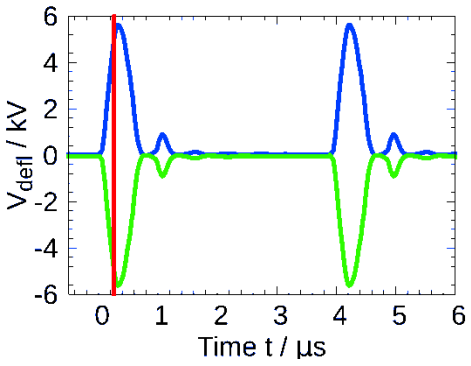

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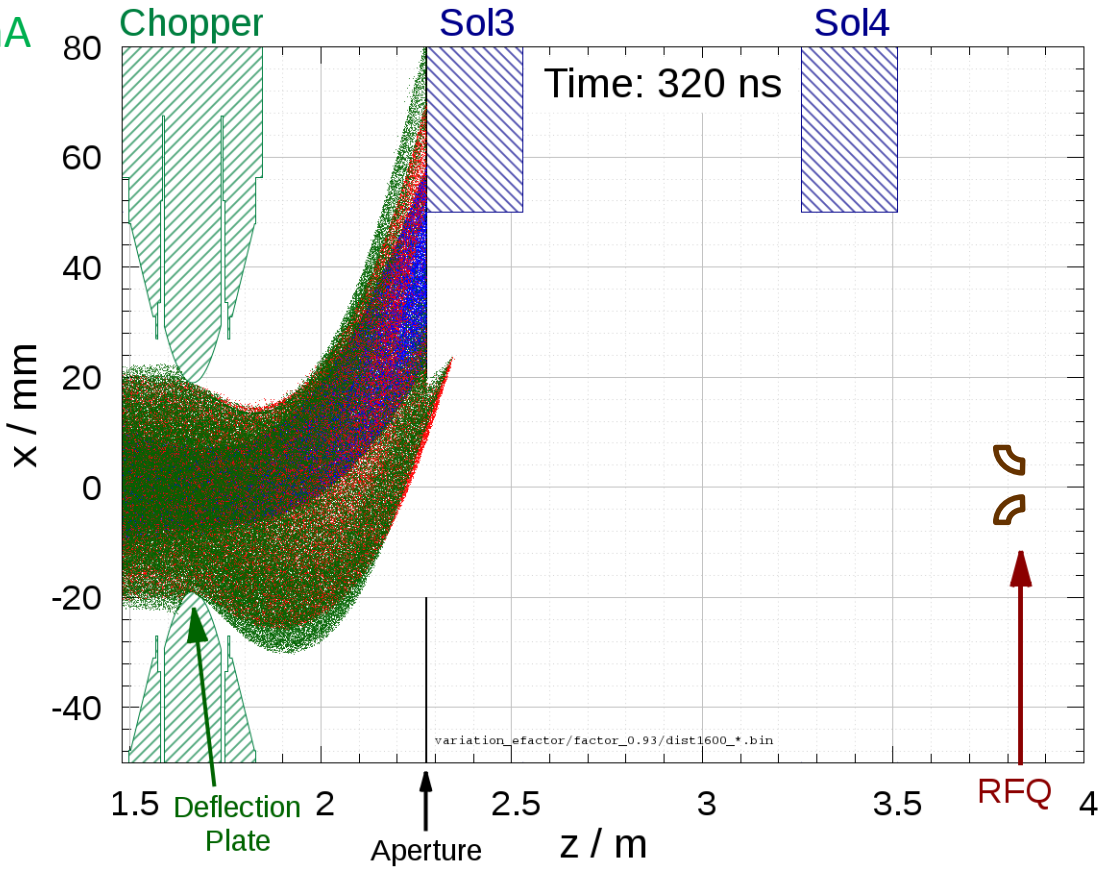
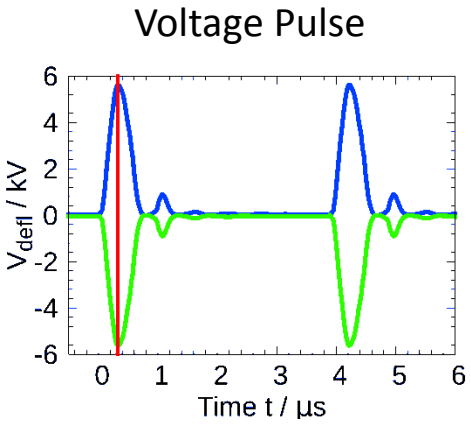
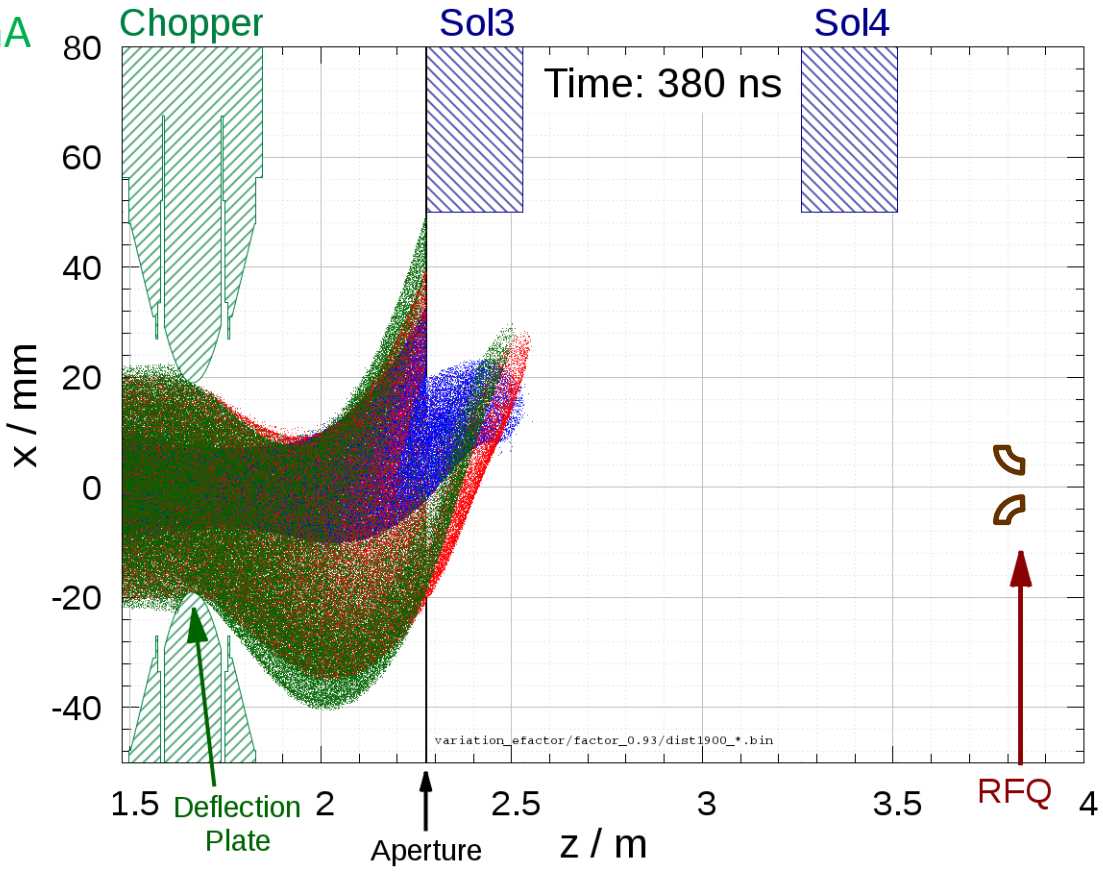


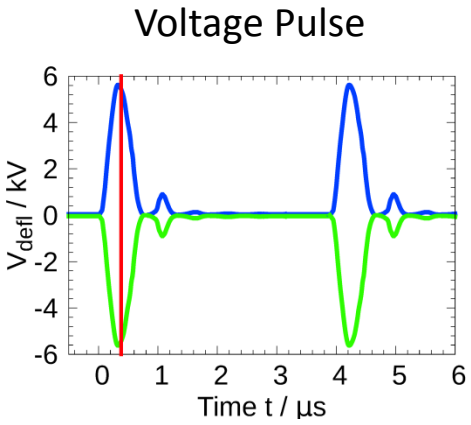


Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

p, 50 mA
H_2^+, 5 mA
H_3^+, 5 mA





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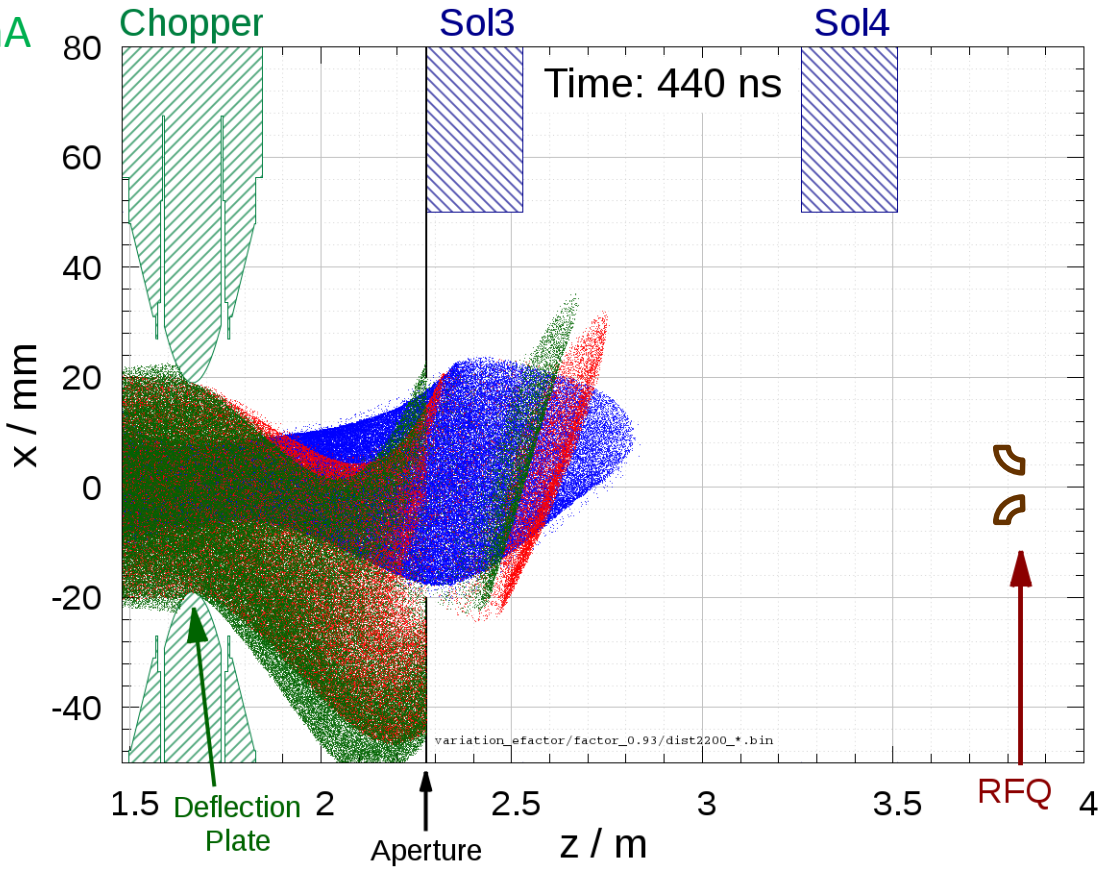

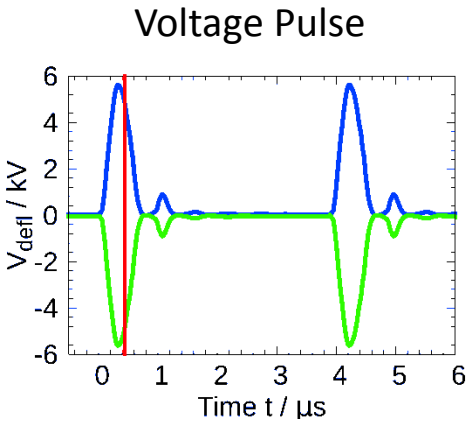

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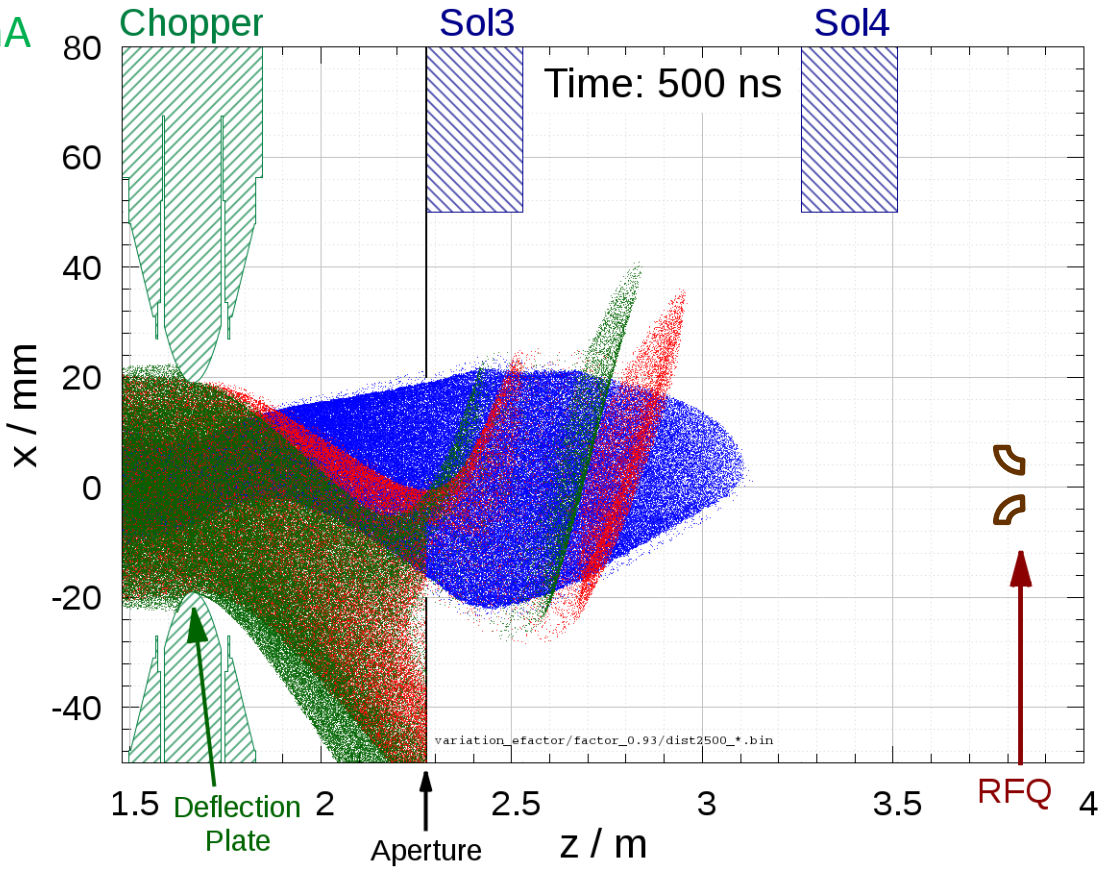

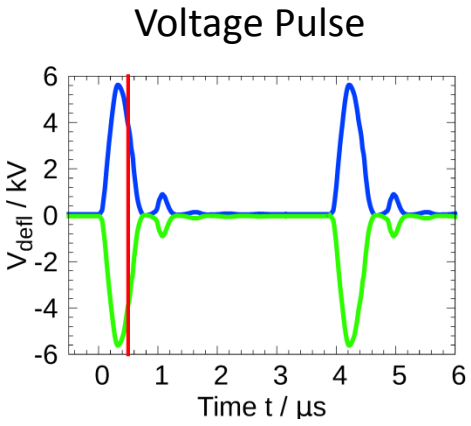

Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

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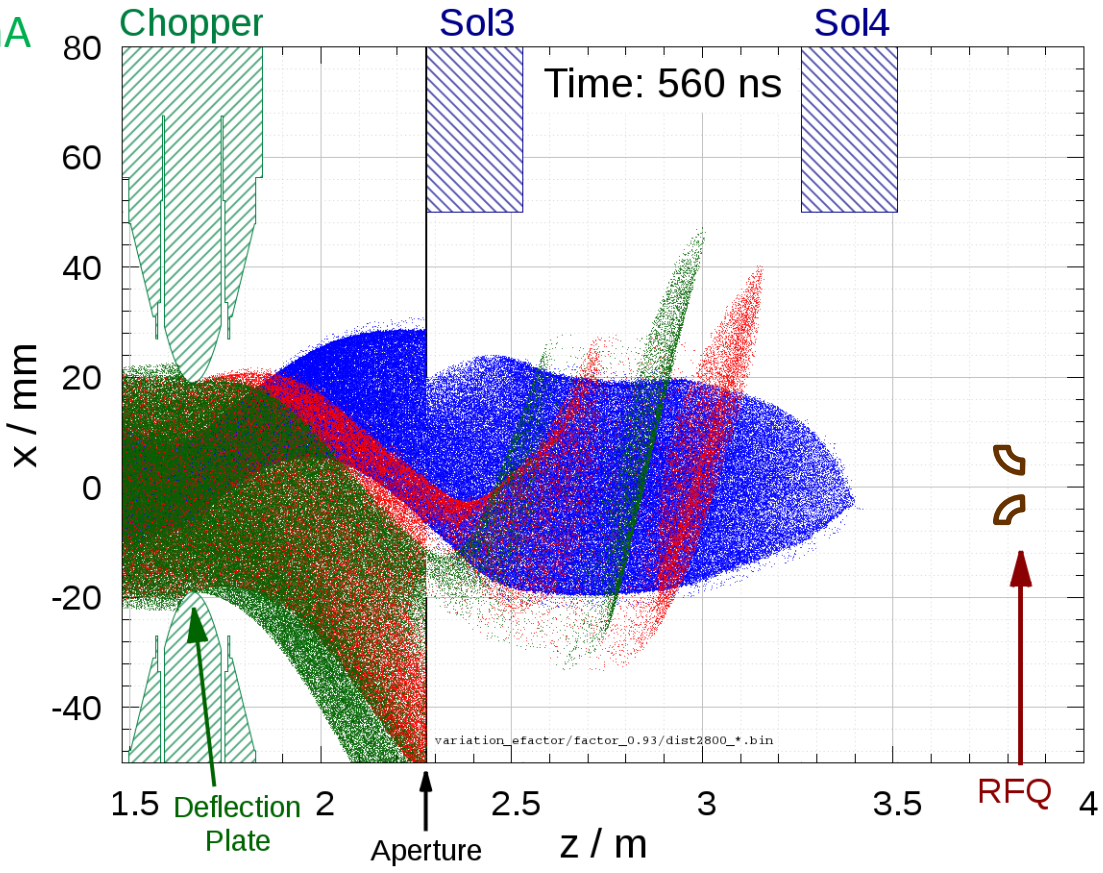
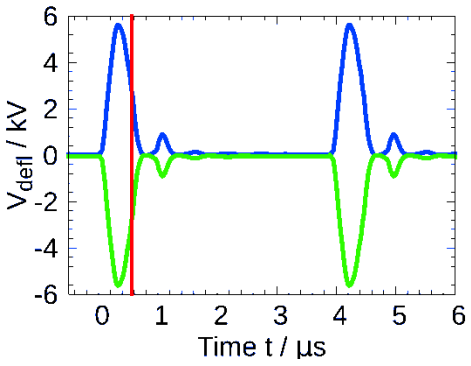


Voltage Pulse



Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

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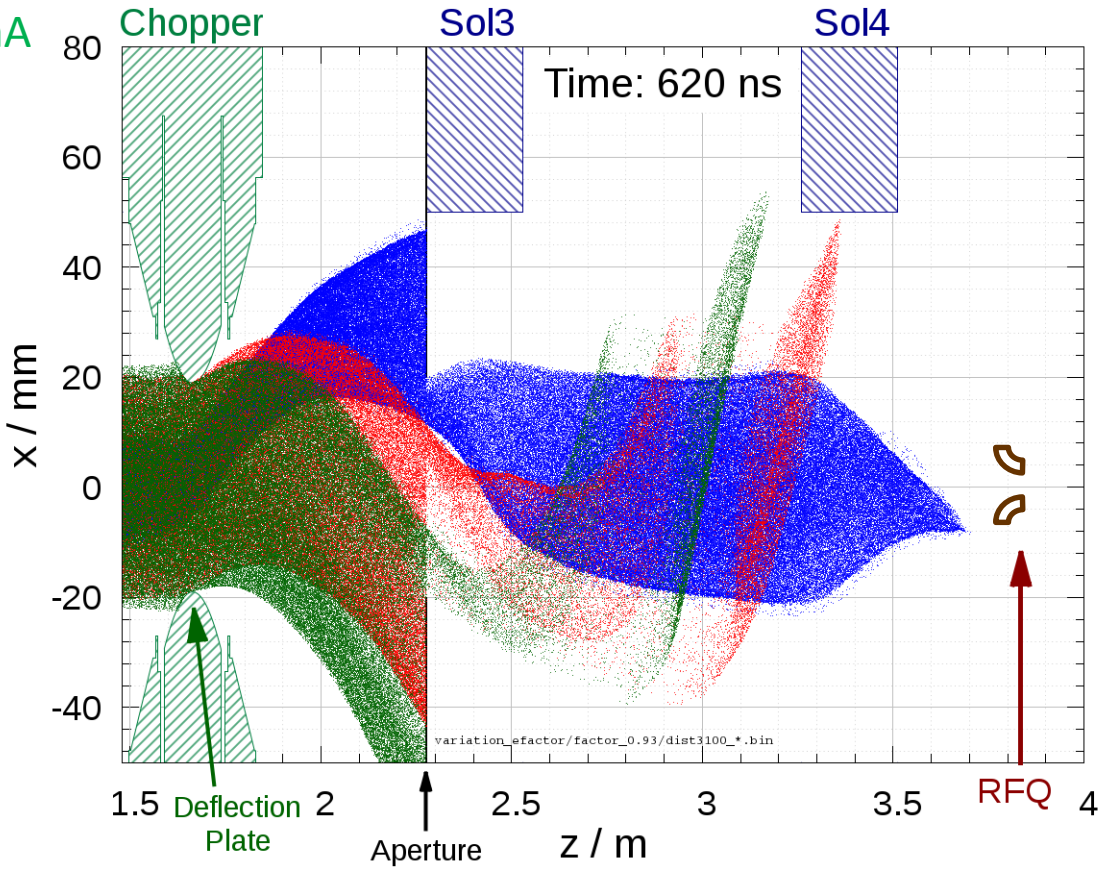

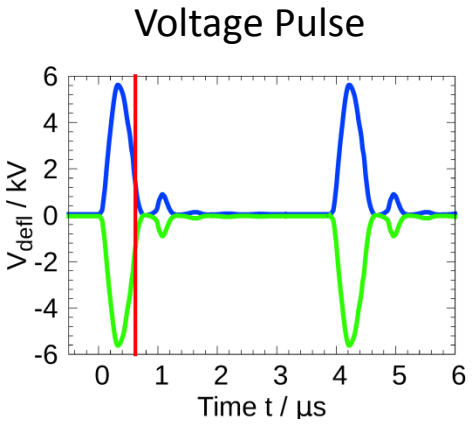

Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

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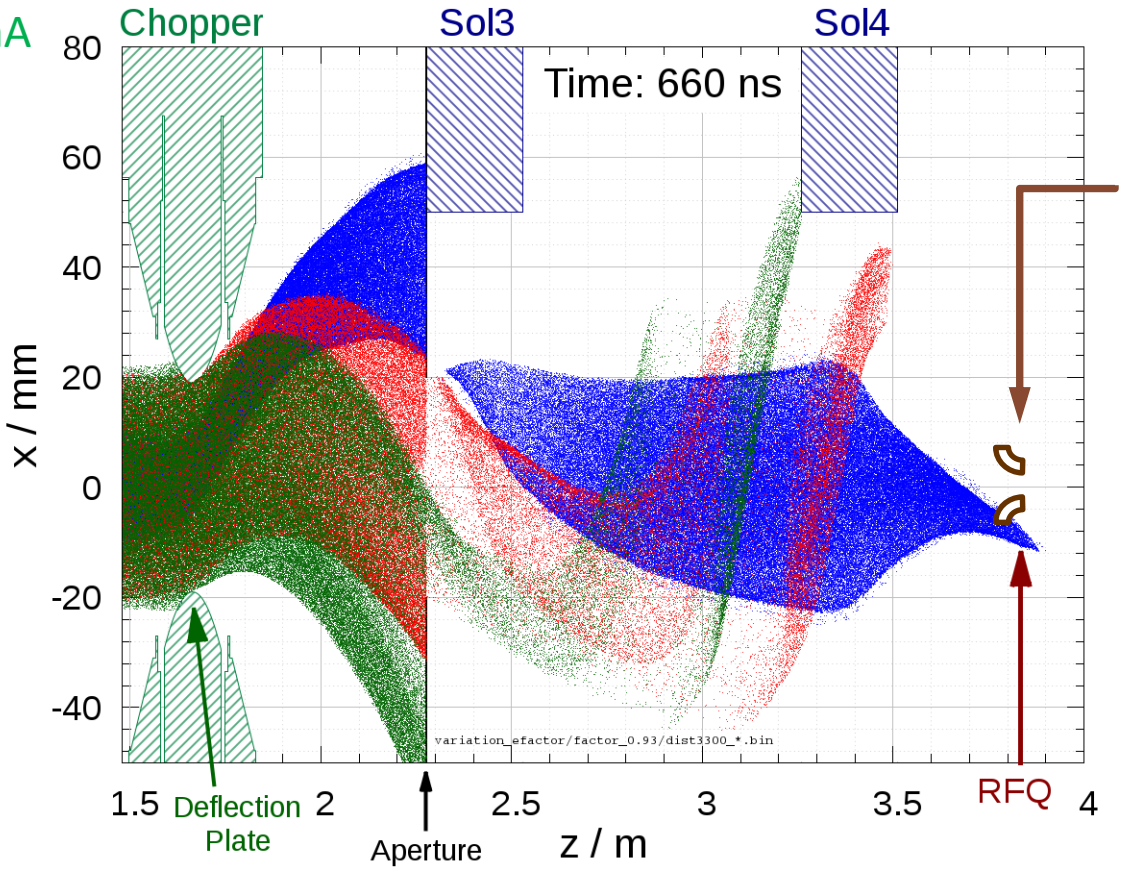

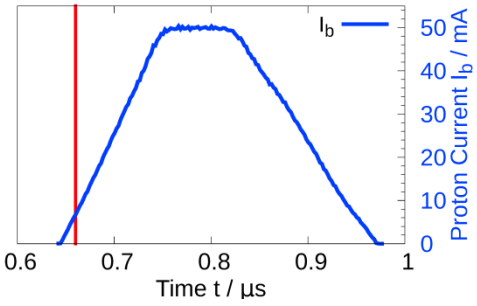

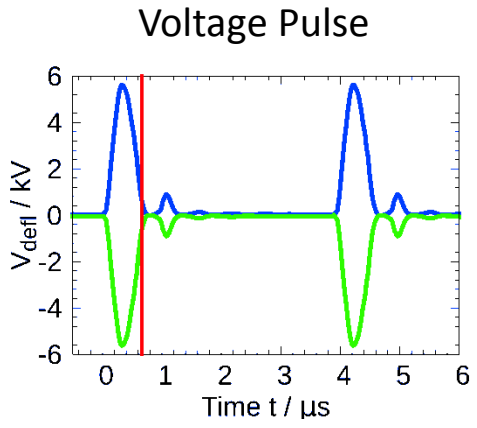

Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

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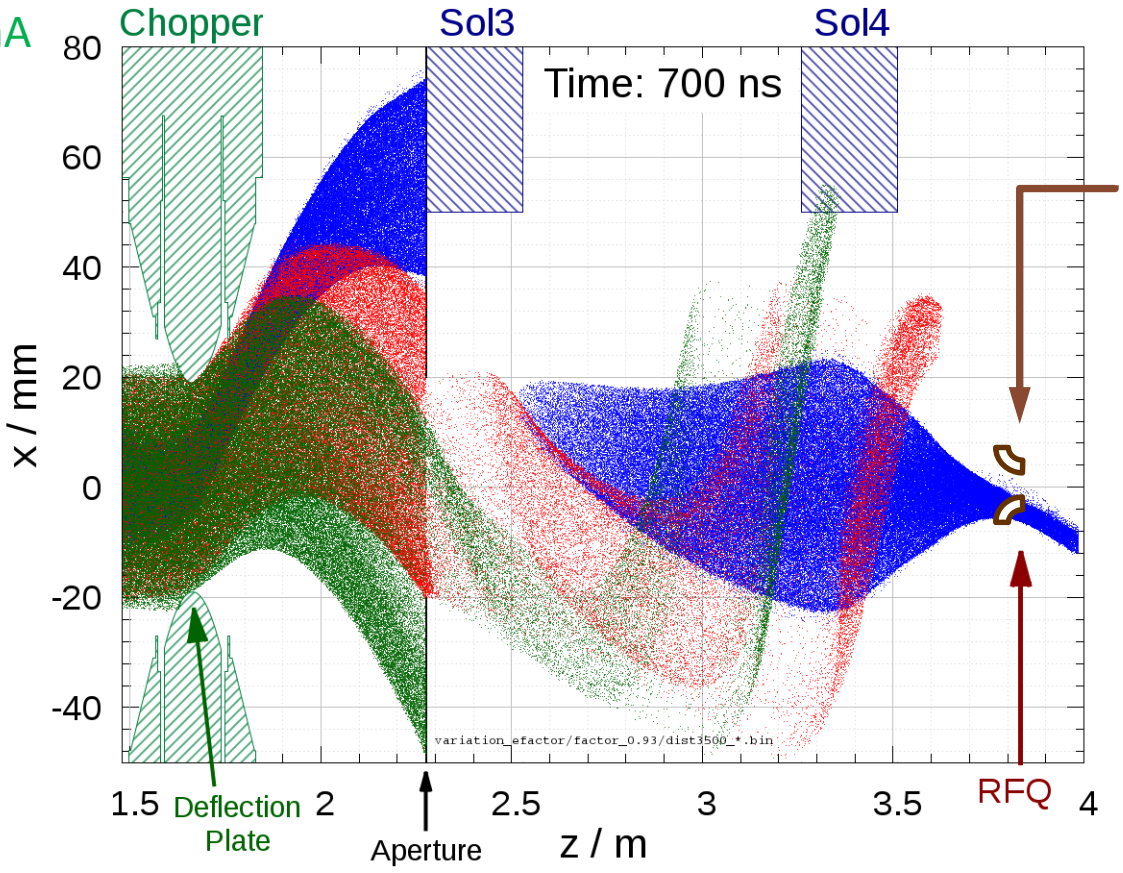
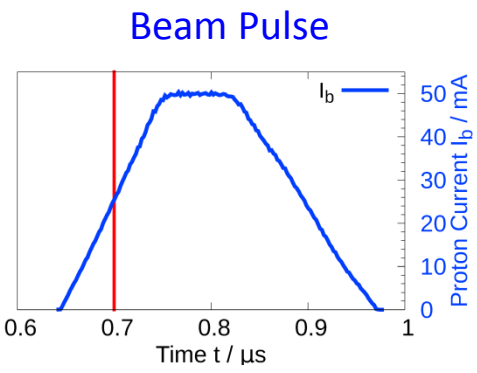
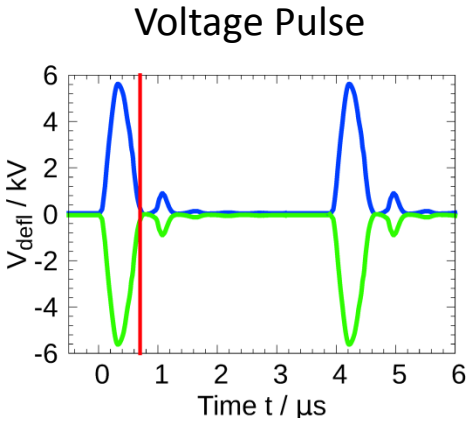
H_3^+, 5 mA







Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

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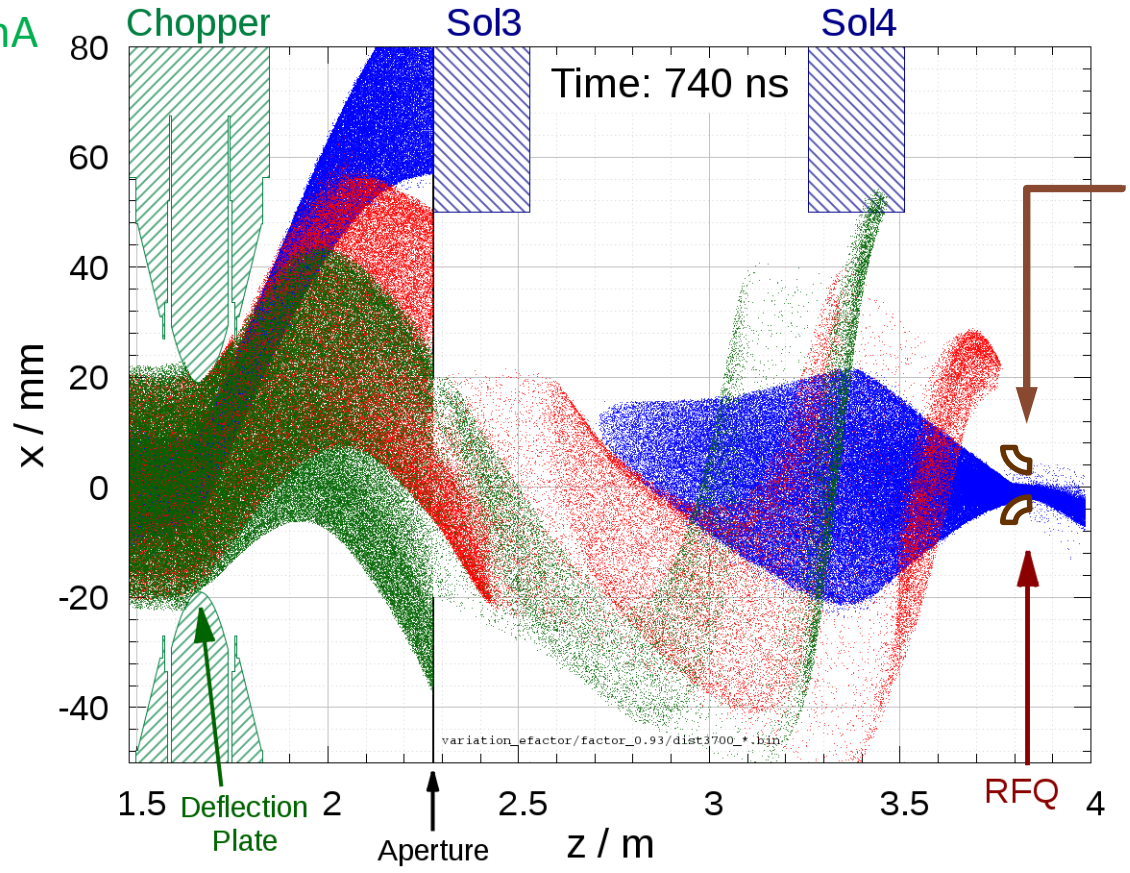

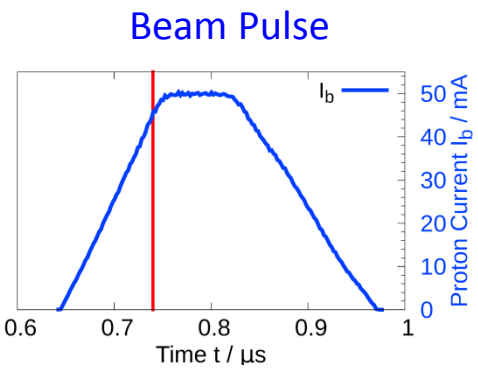

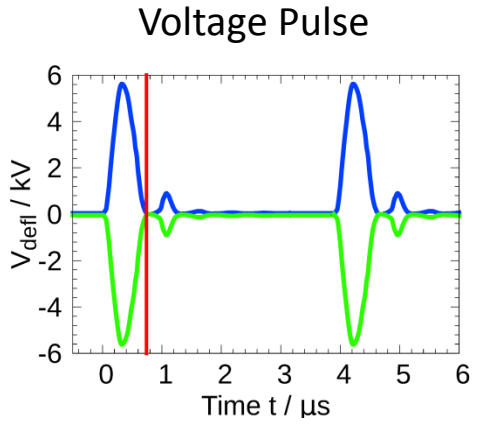

Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

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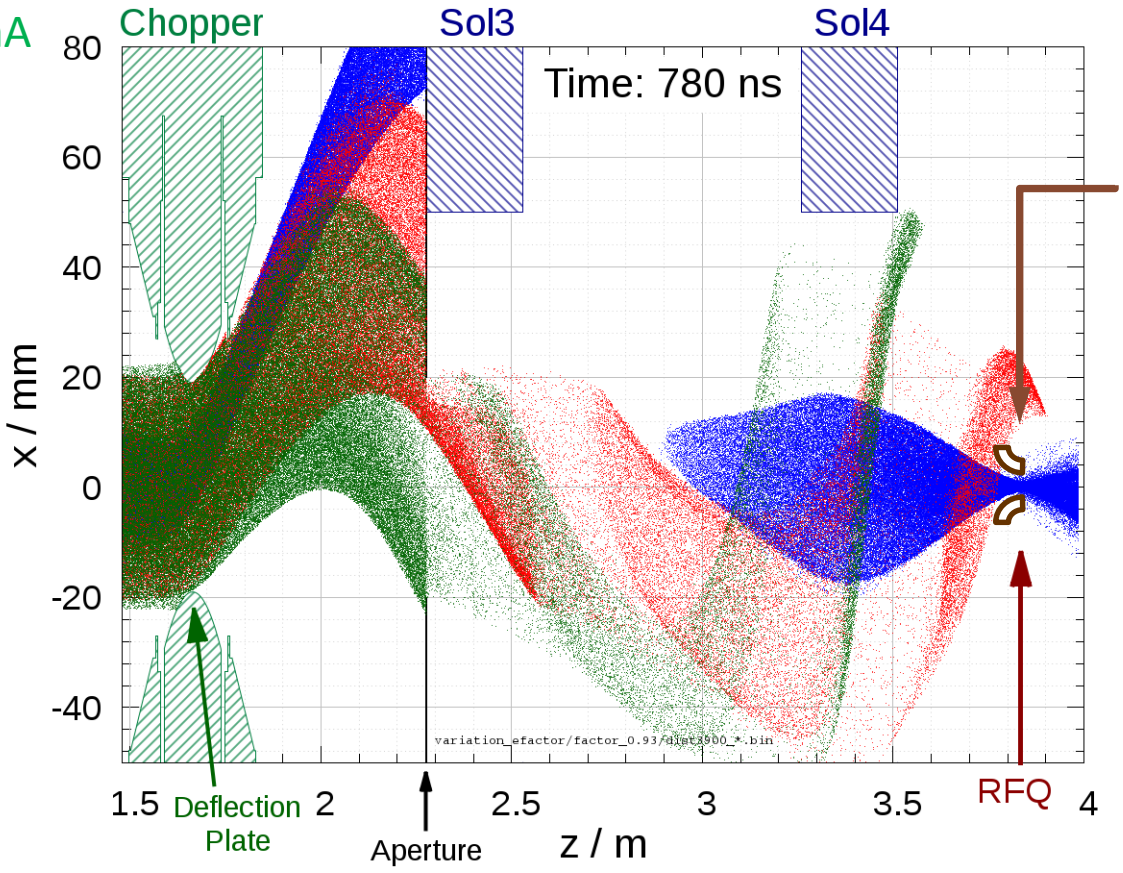
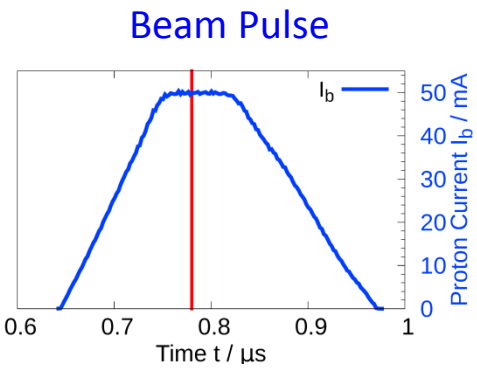
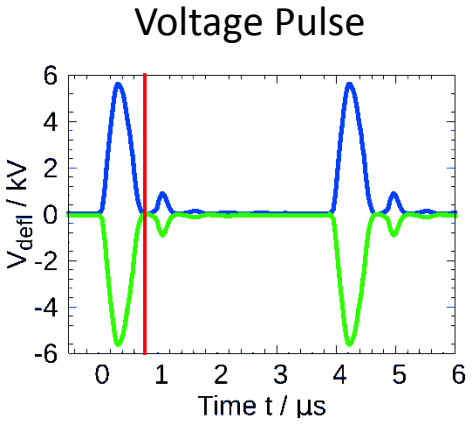


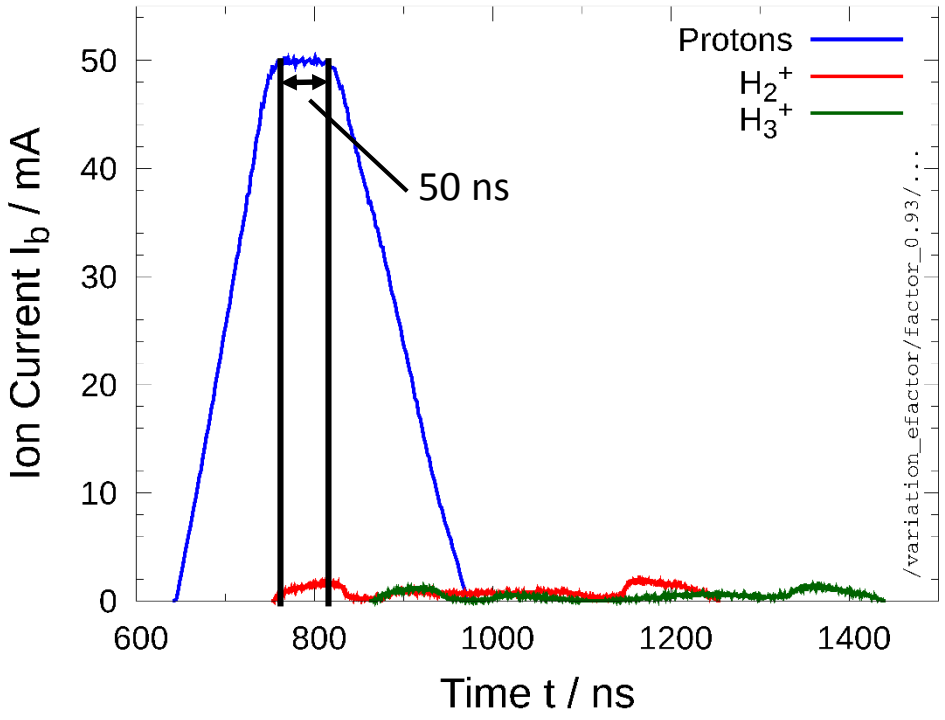




Beam dynamics calculations using PIC-Code Bender.

Beam Shaping Simulation

Simulated Pulse Shape at the RFQ Entrance



Simulated without collimator system in front of the RFQ.

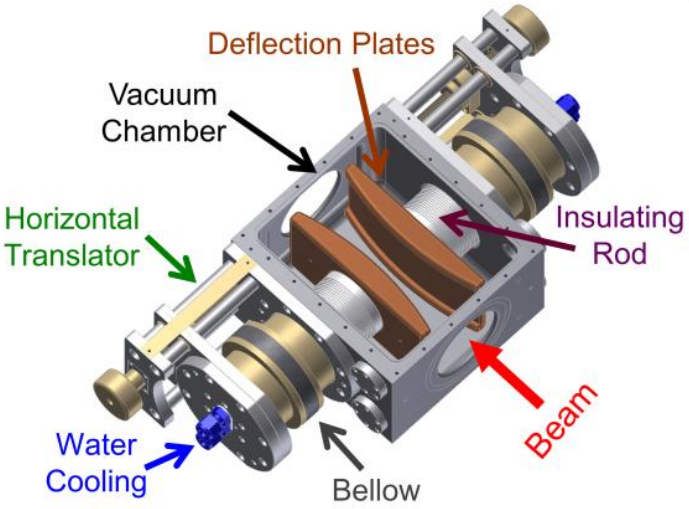
Results of Numerical Simulations:

- Time requirements fulfilled.
- 50 ns flat top:
  - Position offset below ±0.3 mm (necessary condition: *longitudinal* matching of deflection forces).
  - Low emittance.
  - Cylindrical symmetry preserved (necessary condition: *transverse* matching of deflection forces).
- Low transmission for H_2^+ and H_3^+ ions (pulsed velocity filter).

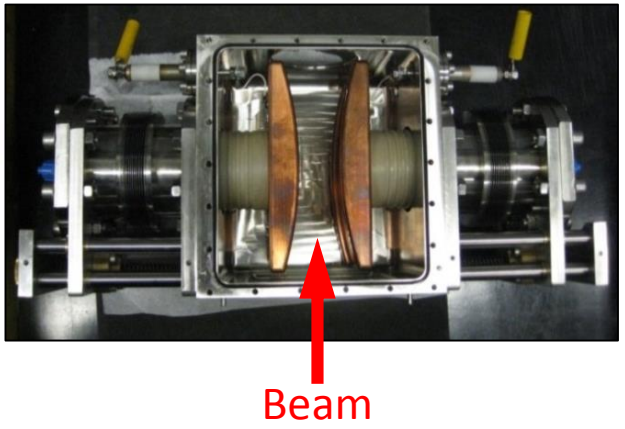
Chopper Hardware Design

Electric Deflector

$V_0 = \pm 6$ kV
$f_{rep} = 257$ kHz
$l_{plate} = 15$ cm
$h_{plate} = 8$ cm

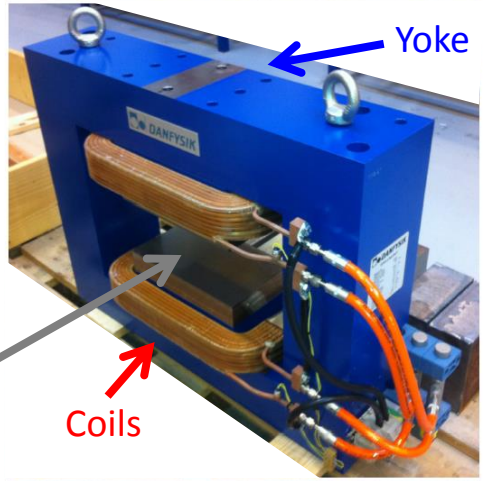


Deflection Chamber

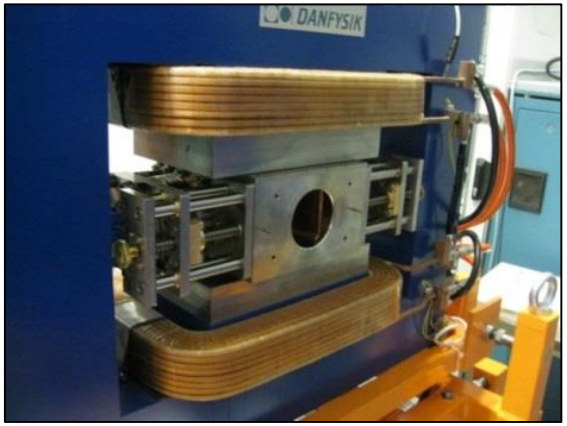


Magnetic Dipole

$B_0 = 130$ mT
$I_{coil} = 130$ A
$l_{dipole} = 15$ cm
$h_{gap} = 11$ cm



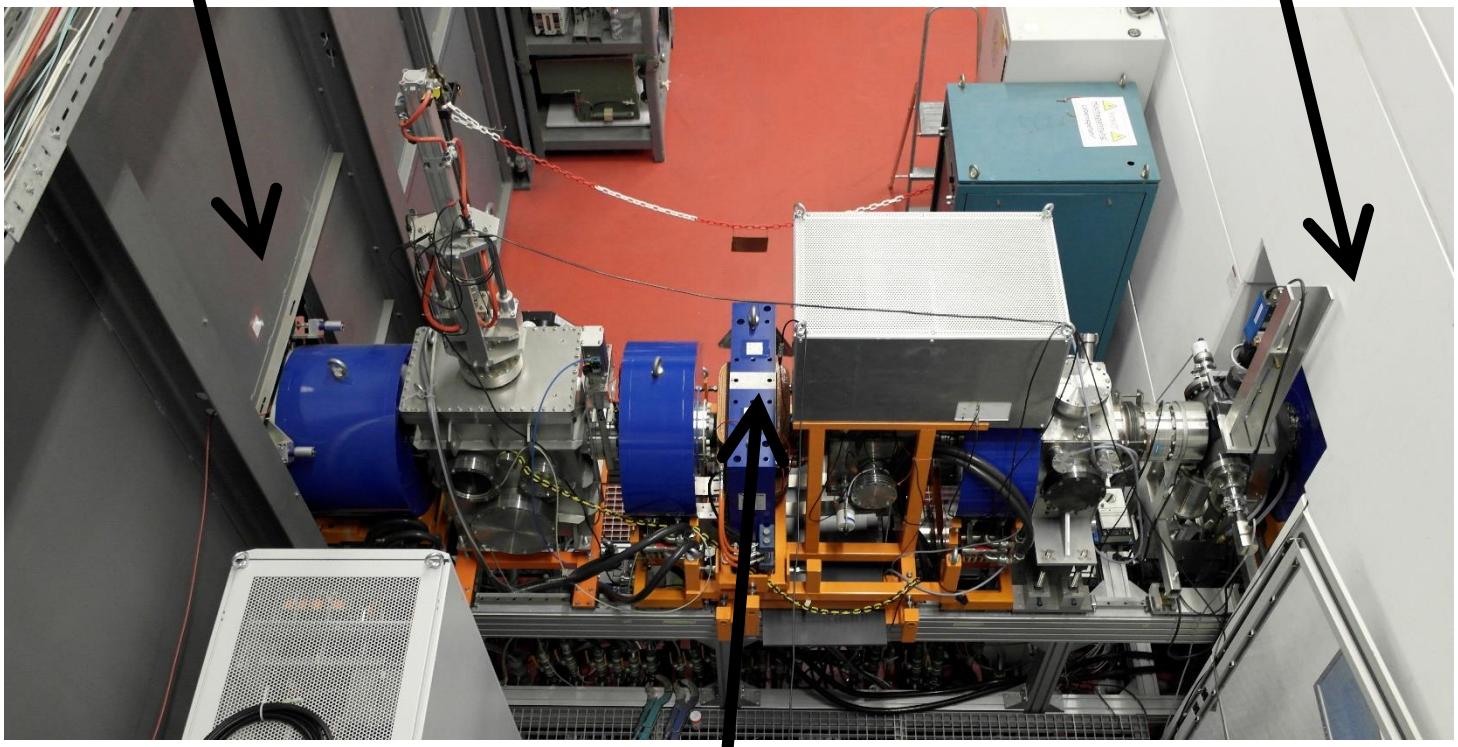
Deflection Chamber in Dipole



Commissioning

HV Terminal: 150 kV

Concrete Shielding
for linac and neutron target

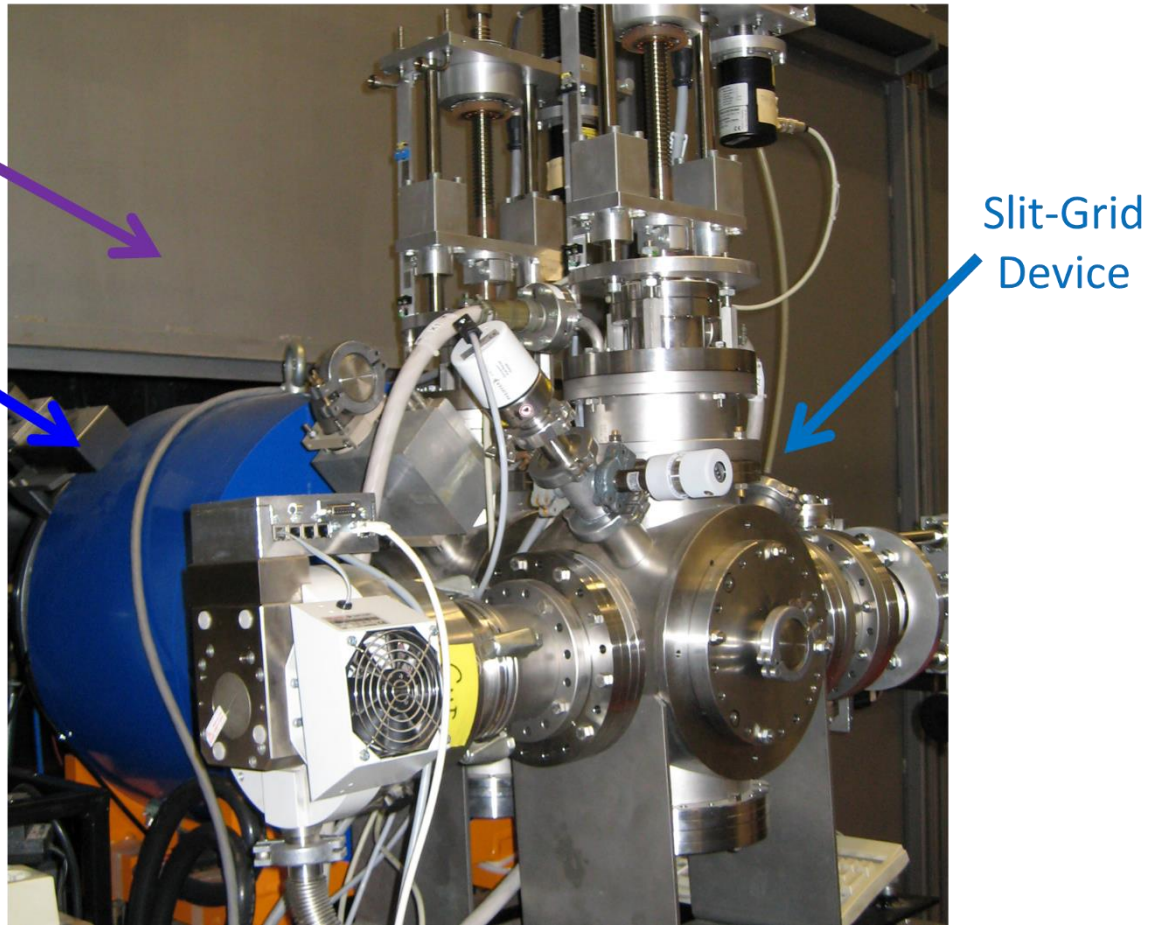


LEBT Section and E×B chopper

Measurements: DC Beam

Emittance measurement behind Solenoid 1

He^+,
10 keV,
0.9 mA

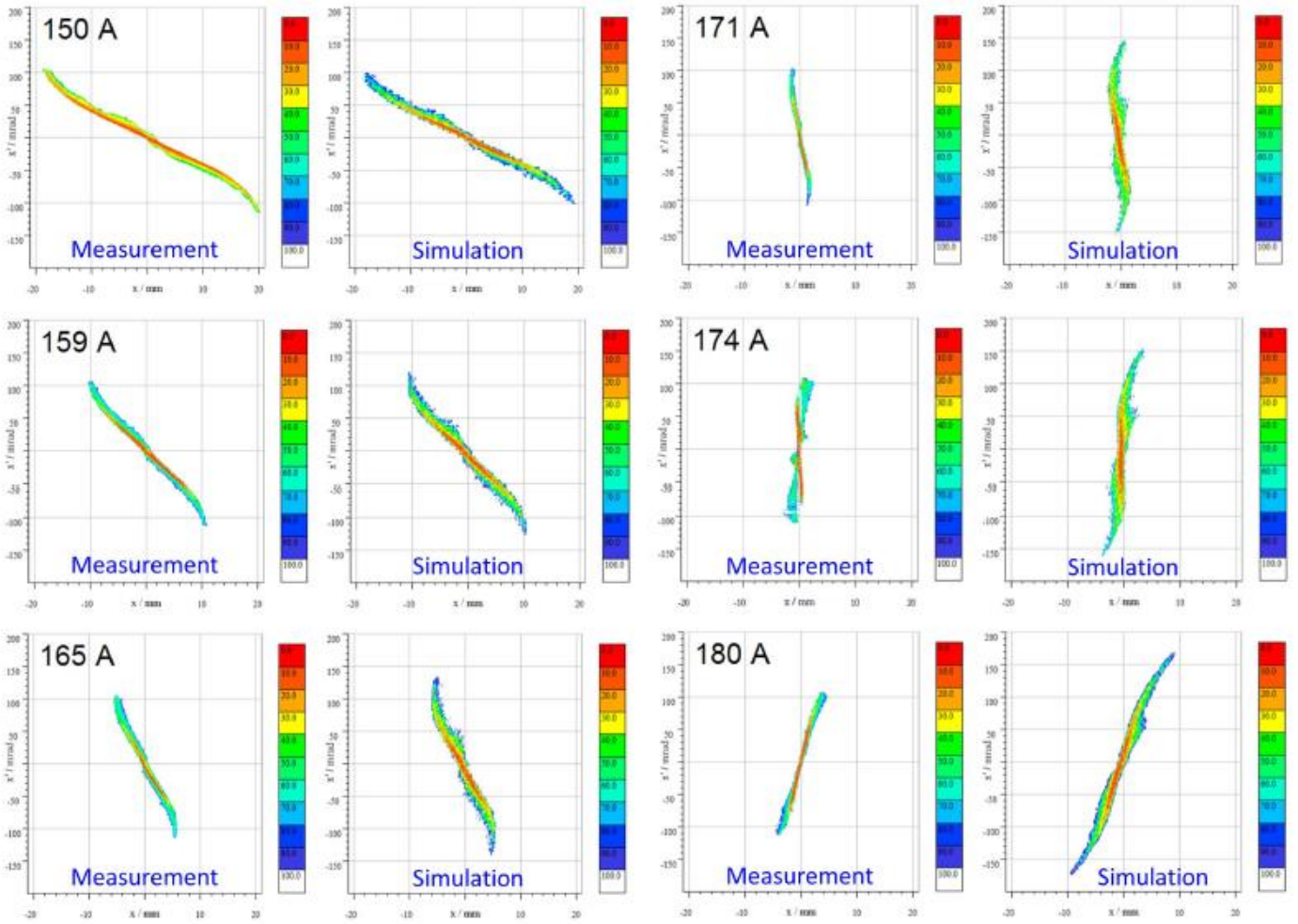


Measurements: DC Beam

He^+,
10 keV,
0.9 mA

Measured using slit-grid device, installed behind Sol1.

Simulated using Lintra code, assuming 85% space charge compensation.

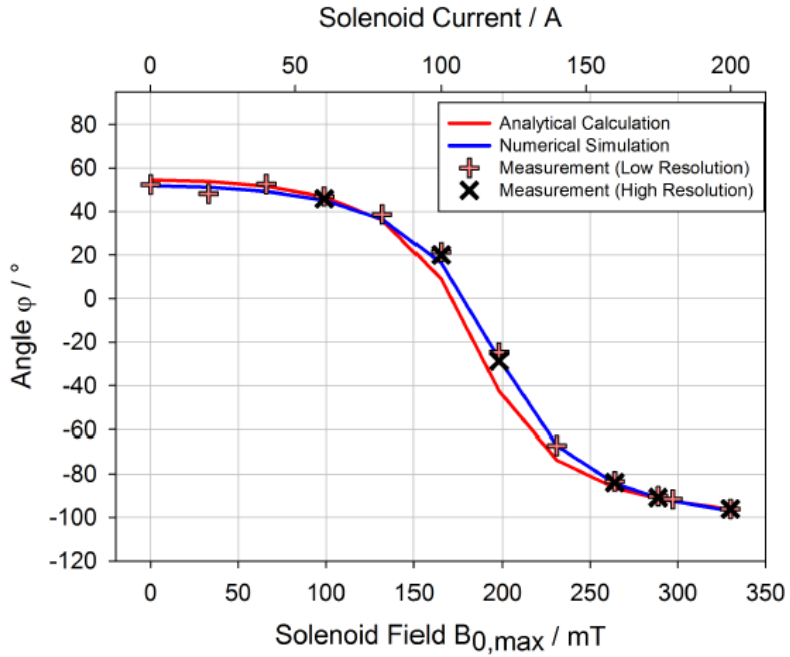


Measurements: DC Beam

He^+,
10 keV,
0.9 mA

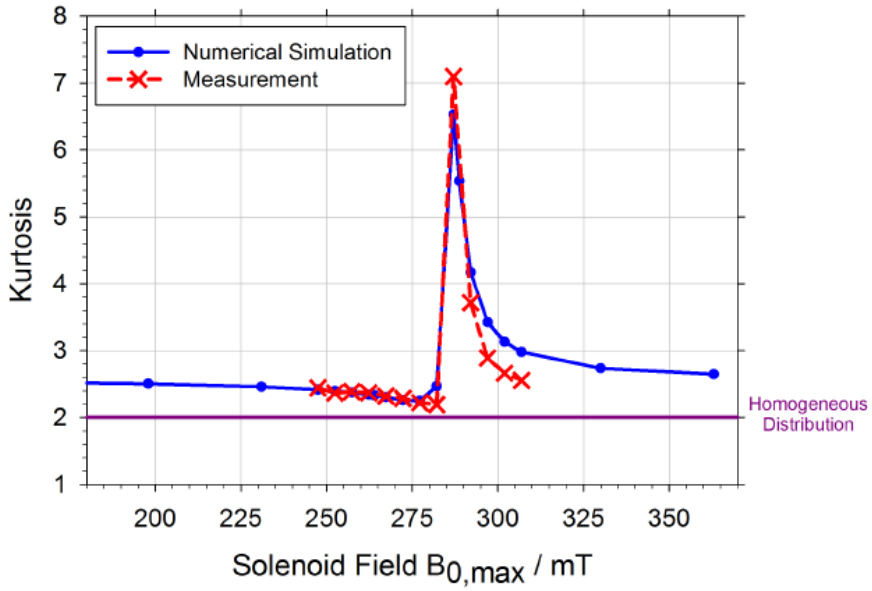
Phase-space angle

$$\tan 2\varphi = \frac{2\alpha}{\gamma - \beta}$$

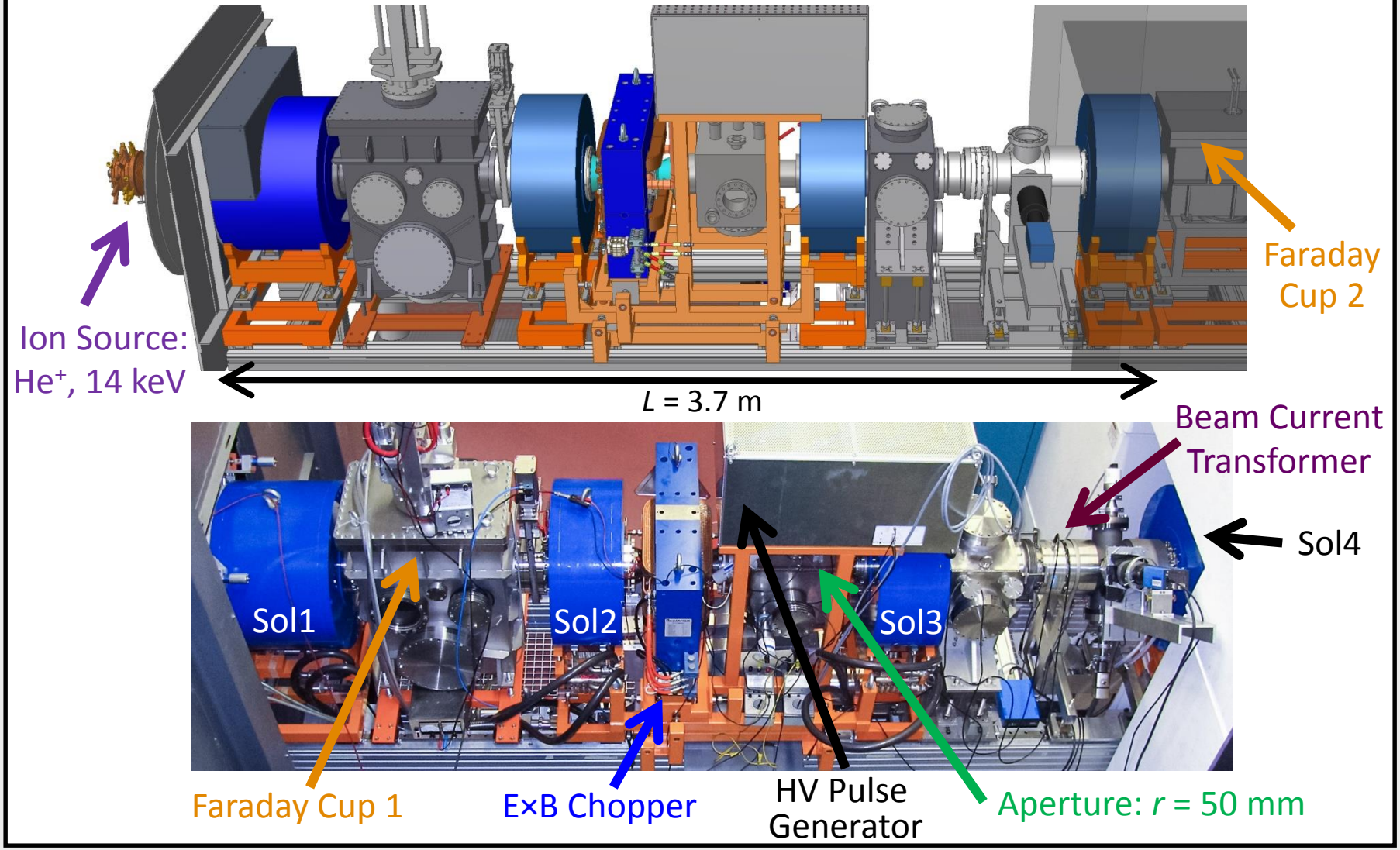


Kurtosis

$$\kappa = \frac{\overline{x^4}}{\overline{x^2}^2}$$

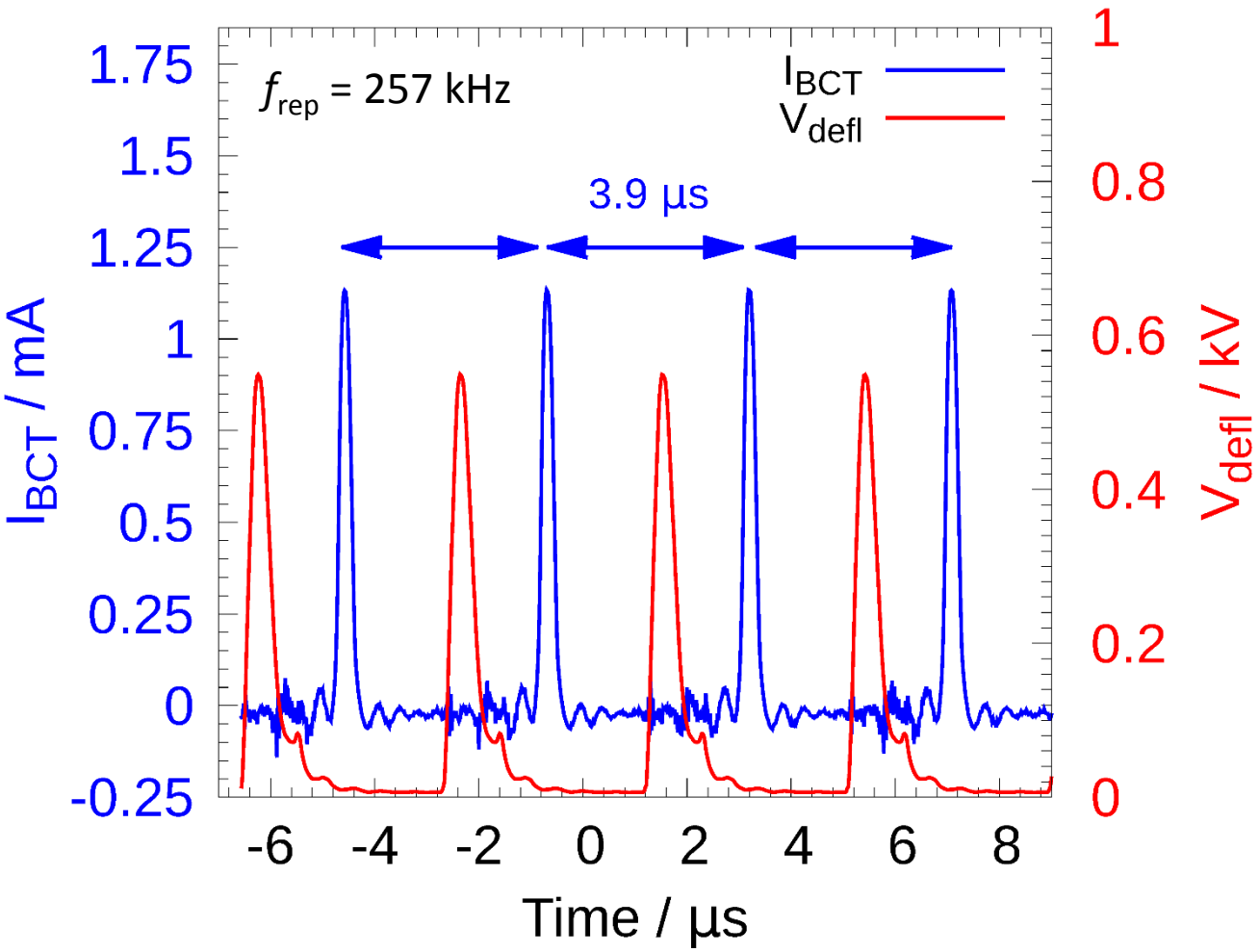


FRANZ LEBT: Overview



Measurements: Repetition Rate

- Beam chopping at 257 kHz experimentally achieved.
- Ratio of Pulsed to DC Beam Current of 95.2% ± 1.6% achieved.



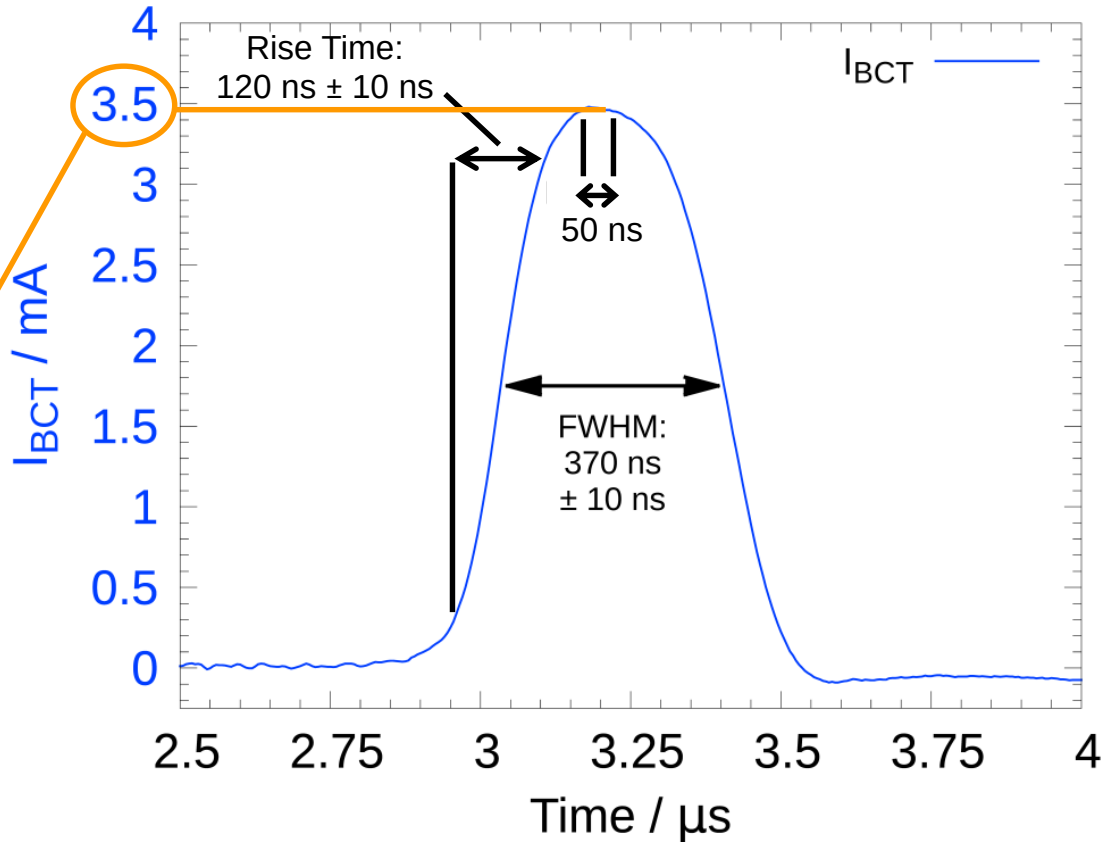
He^+, 14 keV
$r_{aperture}$ = 50 mm
I_{dipole} = 40.0 A

Measurements: Pulse Shape

- Reliable chopping and transport was achieved even for high-perveance beams.

Gen. perveance K = 2.73e-3
(equivalent to 175 mA, p, 120 keV).

$$K = \frac{1}{4\pi\epsilon_0}\sqrt{\frac{m_\mathrm{p}}{2q}}\frac{I_\mathrm{b}}{V_\mathrm{acc}^{3/2}}$$



He$^+$, 14 keV
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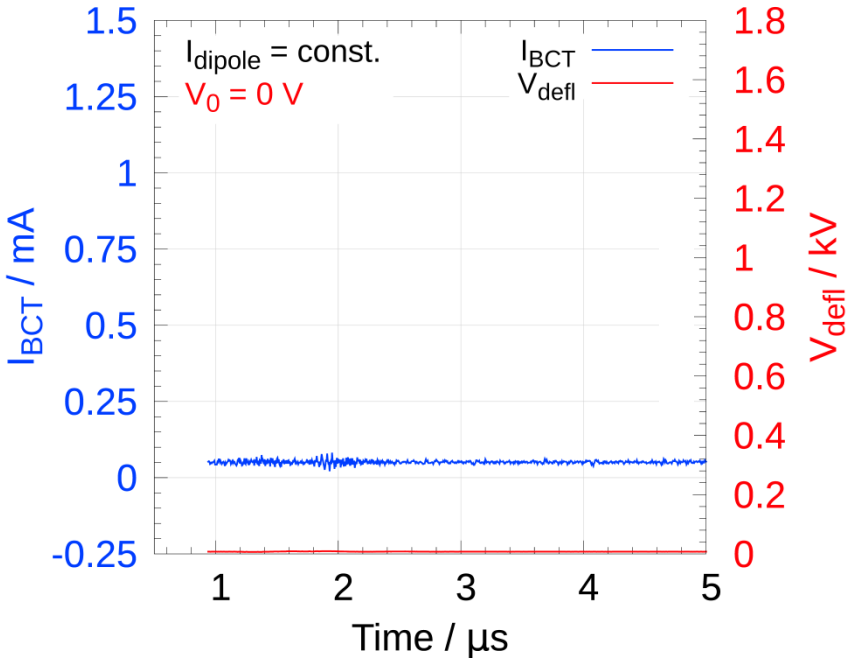
Measurements: Variation of Wien Ratio

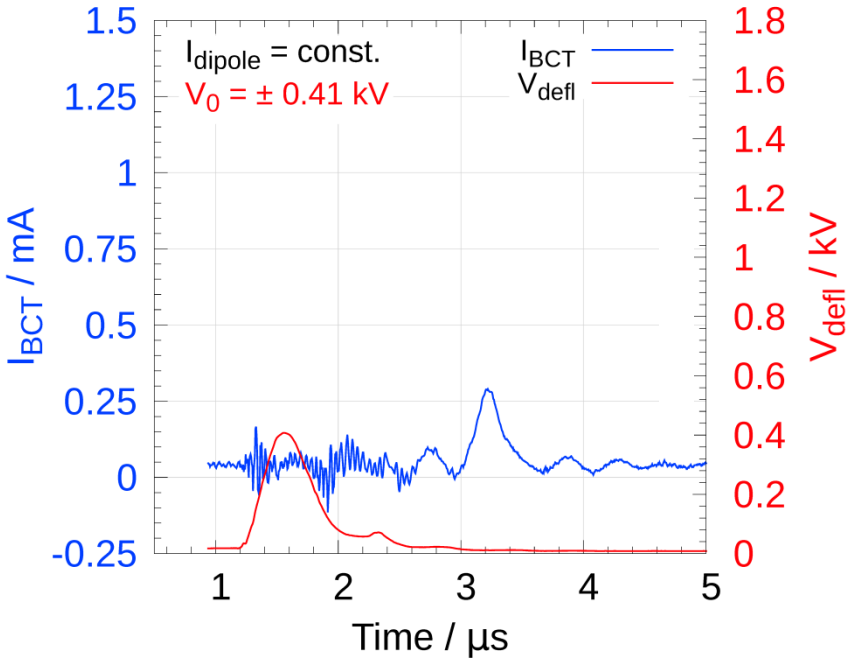


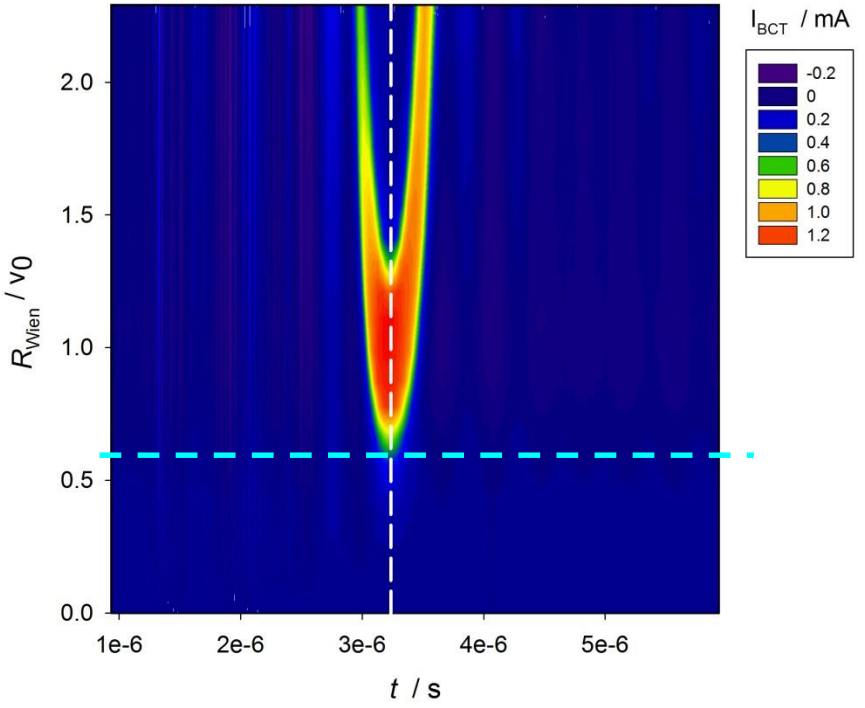
He$^+$, 14 keV
$r_{aperture}$ = 50 mm
I_{dipole} = 40.0 A

$$R_{\text{Wien}} = \frac{\int E_x \, \mathrm{d}z \cdot f_{\text{tof}}}{\int B_y \, \mathrm{d}z}$$

E_x → sweep
B_y → const.

Measurements: Variation of Wien Ratio





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sweep

const.

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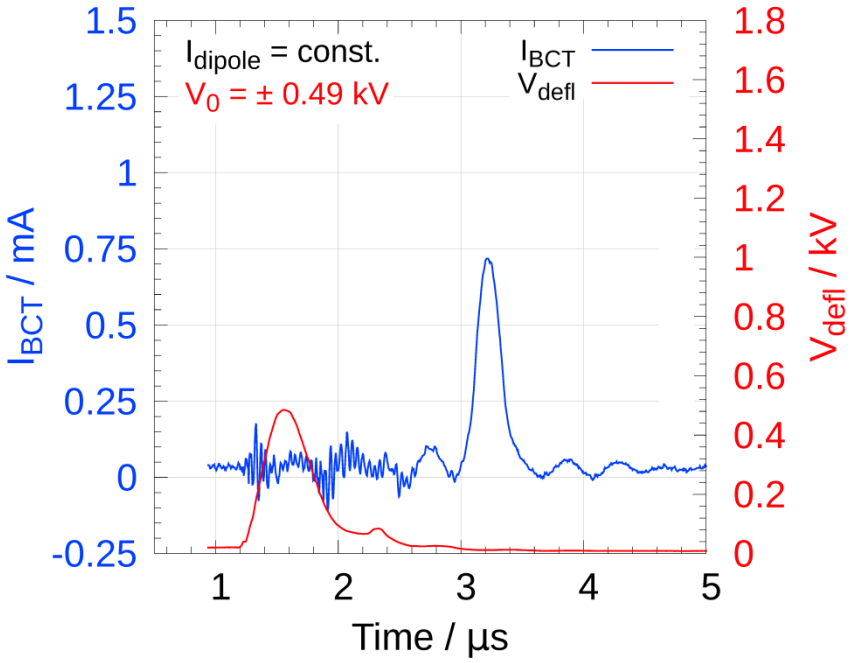

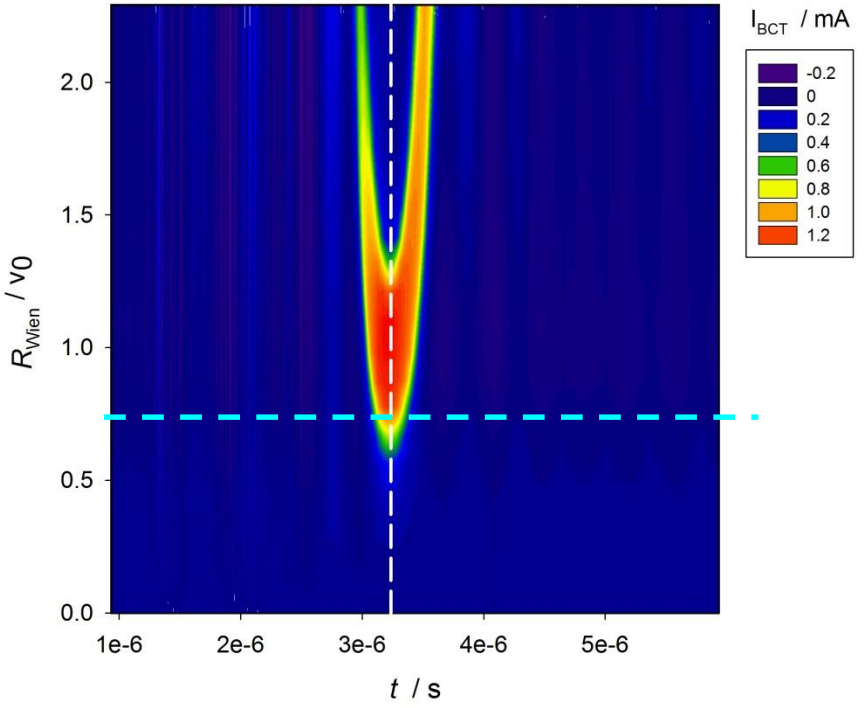

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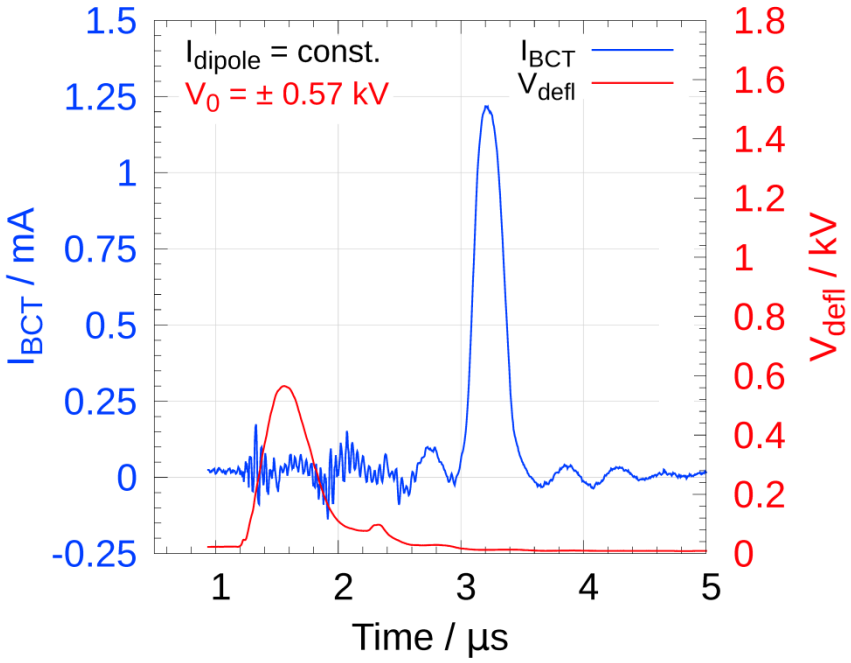

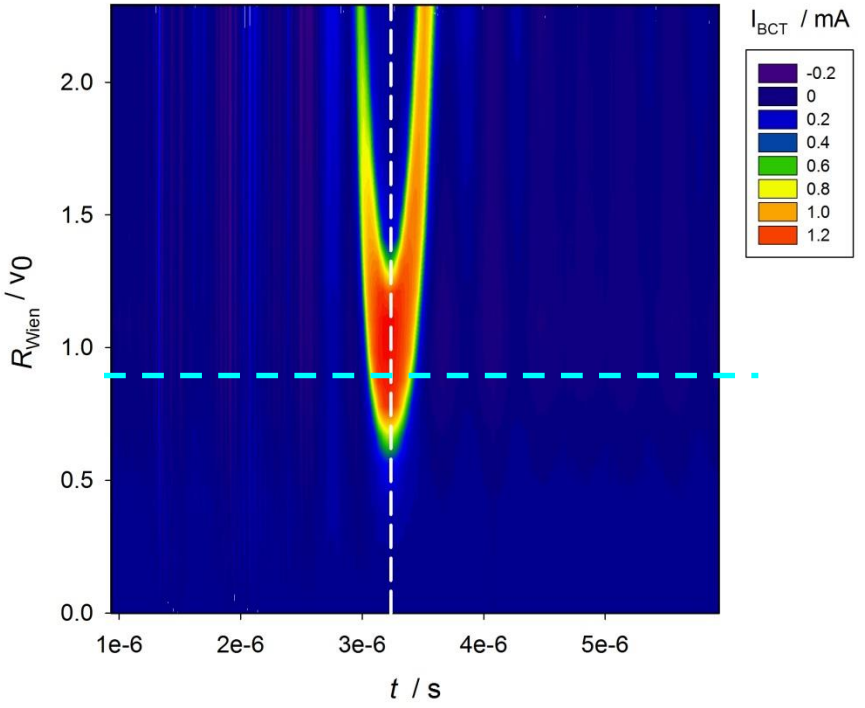

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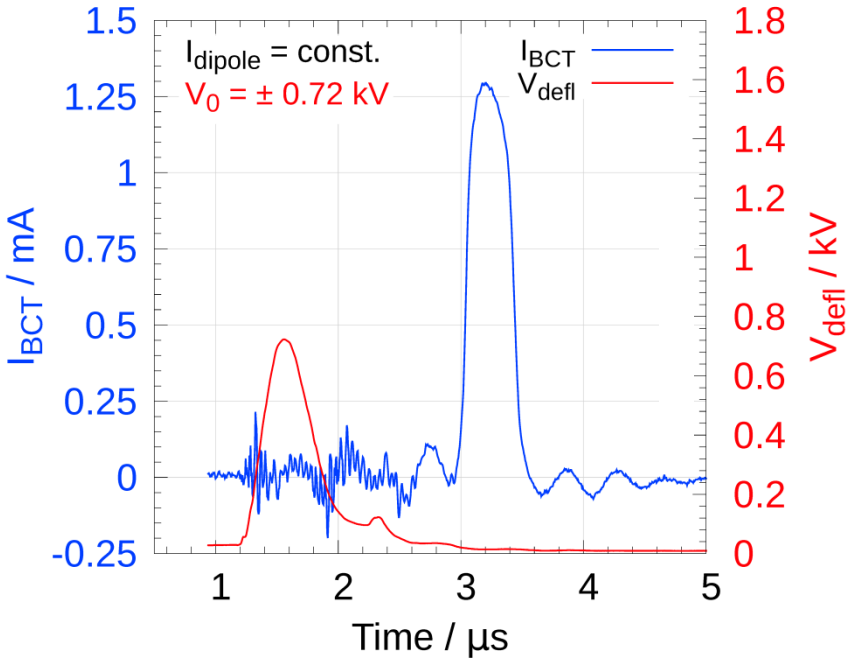

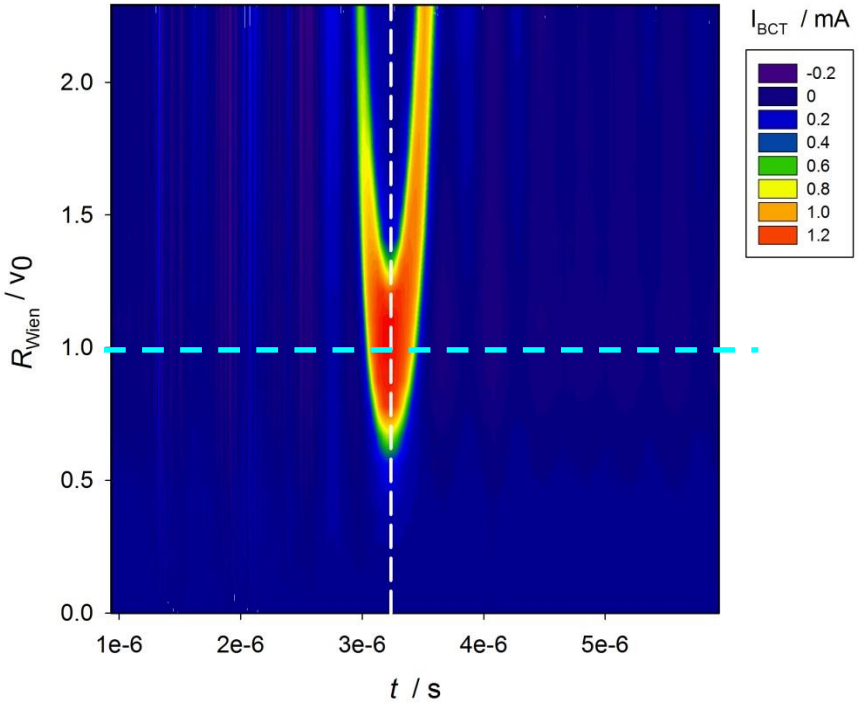

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sweep

const.

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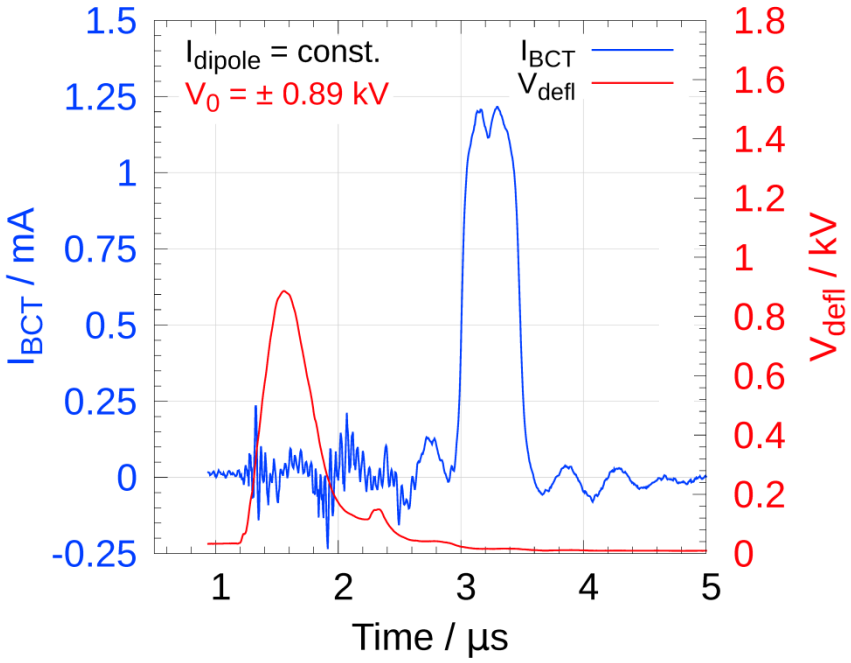

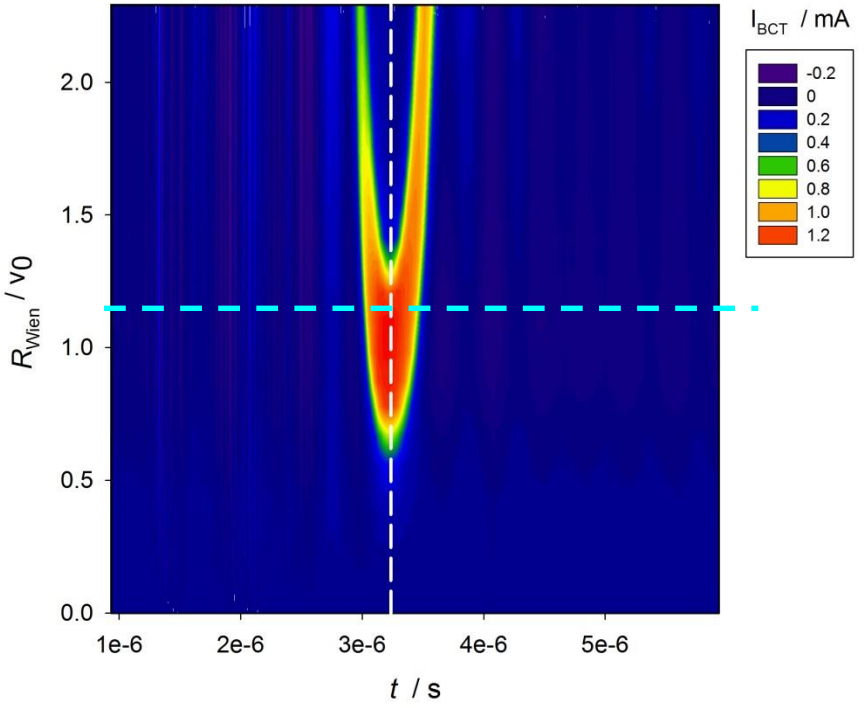

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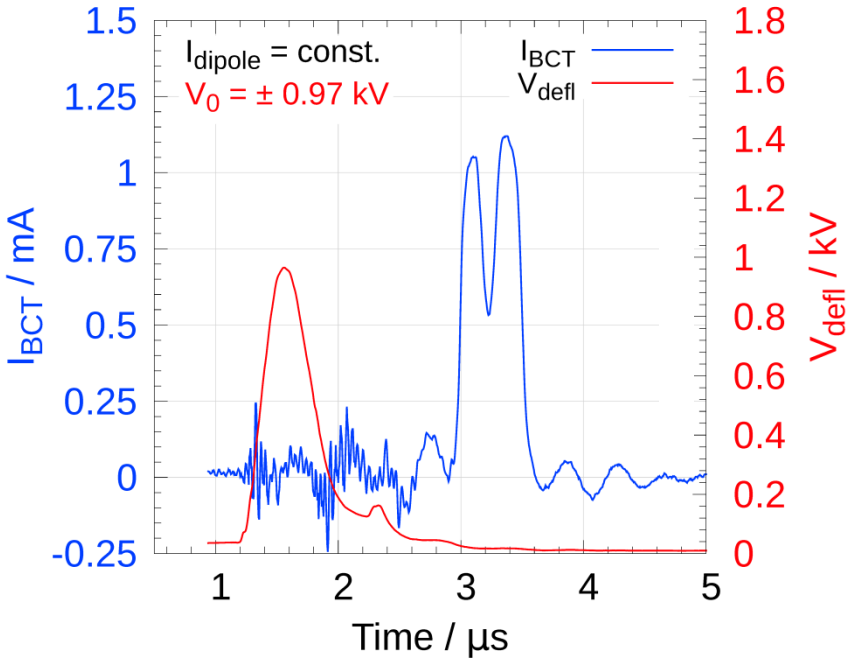
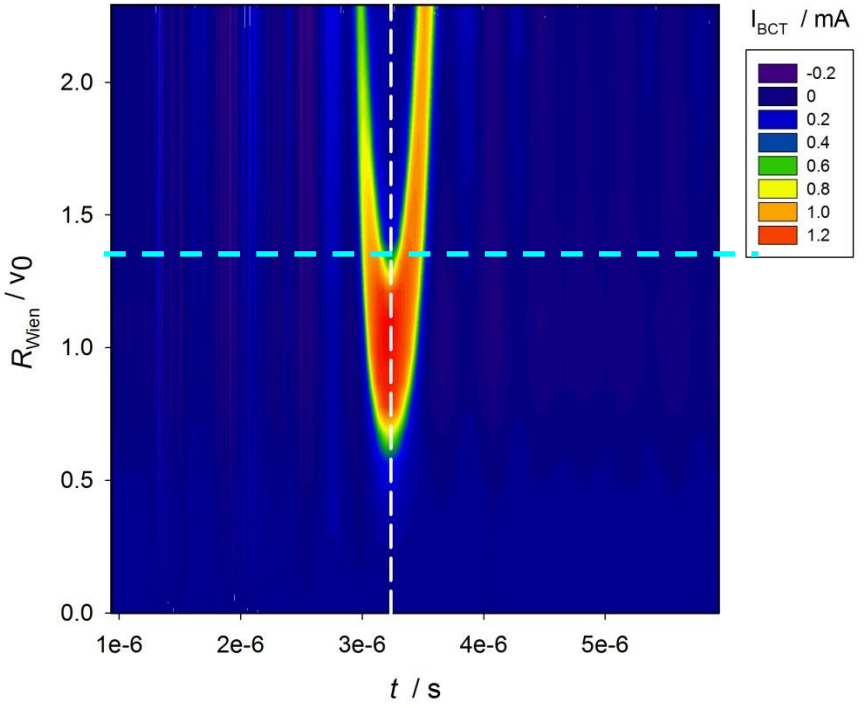
const.

Measurements: Variation of Wien Ratio





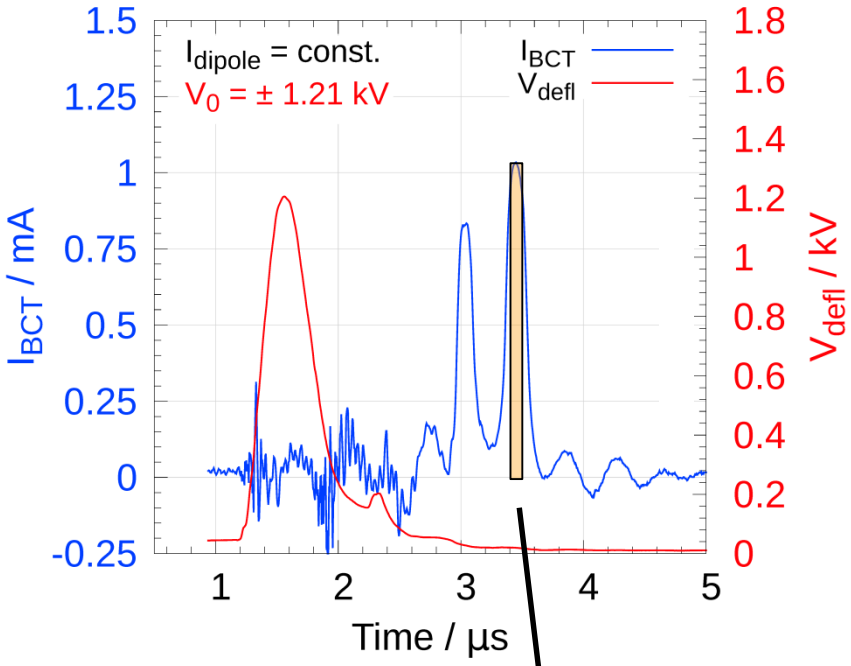
He$^+$, 14 keV
$r_{aperture}$ = 50 mm
I_{dipole} = 40.0 A

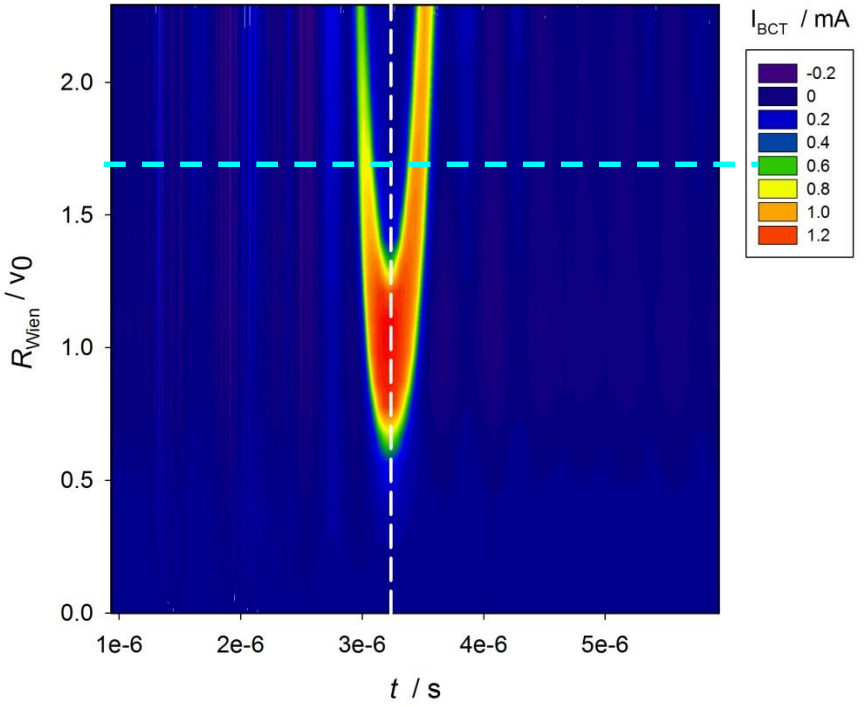
$$R_{\mathrm{Wien}} = \frac{\int E_x \,\mathrm{d}z \cdot f_{\mathrm{tof}}}{\int B_y \,\mathrm{d}z}$$

sweep

const.

Measurements: Variation of Wien Ratio





He⁺, 14 keV
$r_{aperture}$ = 50 mm
I_{dipole} = 40.0 A

$$Q_{\text{flattop}} = I_{\text{BCT}}^{\max} \cdot t_{\text{flattop}}$$

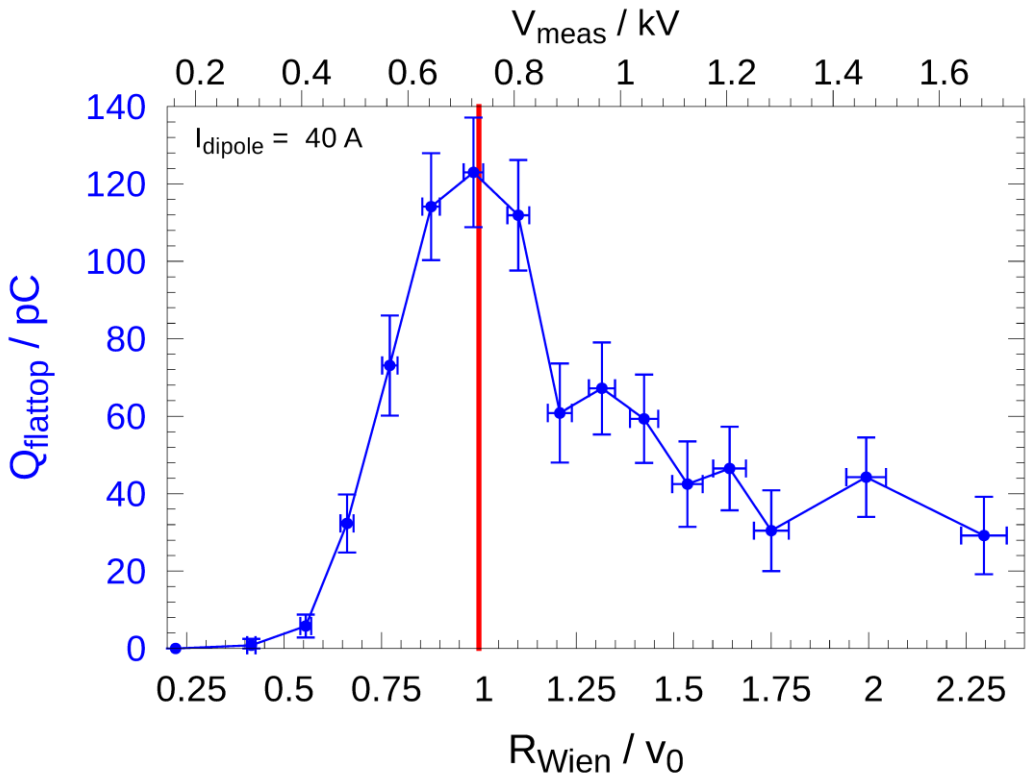
$$R_{\text{Wien}} = \frac{\int E_x \, \mathrm{d}z \cdot f_{\text{tof}}}{\int B_y \, \mathrm{d}z}$$

sweep

const.

Measurements: Variation of Wien Ratio

- Highest flat-top charge achieved for the theoretically derived Wien condition.
- Adequate matching of electric and magnetic deflection forces.



He$^+$, 14 keV
$r_{aperture}$ = 50 mm
I_{dipole} = 40.0 A

$$Q_{\text{flattop}} = I_{\text{BCT}}^{\max} \cdot t_{\text{flattop}}$$

$$R_{\text{Wien}} = \frac{\int E_x \, \mathrm{d}z \cdot f_{\text{tof}}}{\int B_y \, \mathrm{d}z}$$

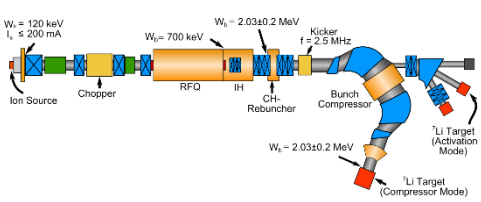
E_x: sweep
B_y: const.

LEBT: PXIE and FRANZ

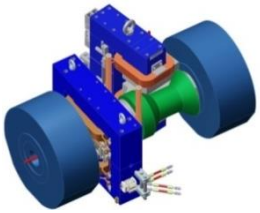
	PXIE	FRANZ – Commissioning	FRANZ - II
	H^-	He^+	p
Beam Energy	30 keV	14 keV	120 keV
Beam Current	5 (10) mA	< 3.5 mA	50 (200) mA
Beta	0.8%	0.27%	1.6%
Gen. Perveance	6.25E-04	2.74E-03	7.81E-04
Chopping in (center of) LEBT	yes	yes	yes
Pulse Length	> µs	100 ns to µs	100 ns to µs
Rep. Rate	1 to 60 Hz	103 to 257 kHz	103 to 257 kHz
Numbers of Solenoids	3	4	4

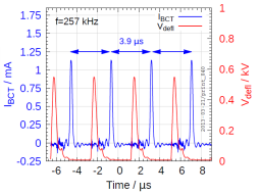
Conclusion

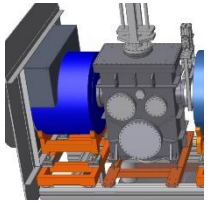
- Accelerator-driven neutron source FRANZ currently under construction.



- E×B chopper and LEBT section have been commissioned with beam: ready for pulsed & dc operation.

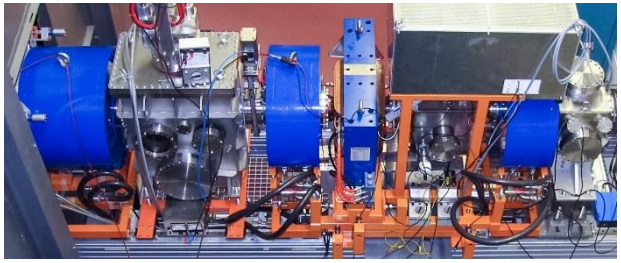


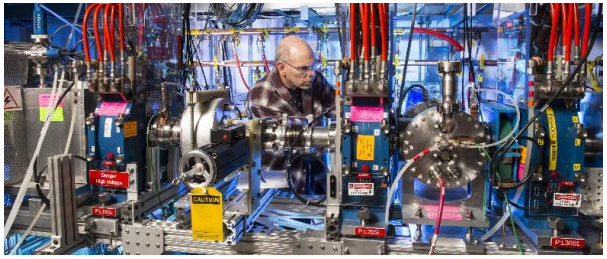




- *The LEBTs for FRANZ and PXIE allow…*
  - investigation of high-perveance beams…
  - …with positive (FRANZ) and negative (PXIE) ions…
  - …in dc or in pulsed mode…
  - …using different neutralization schemes,…

  which is a promising basis for further cooperation.



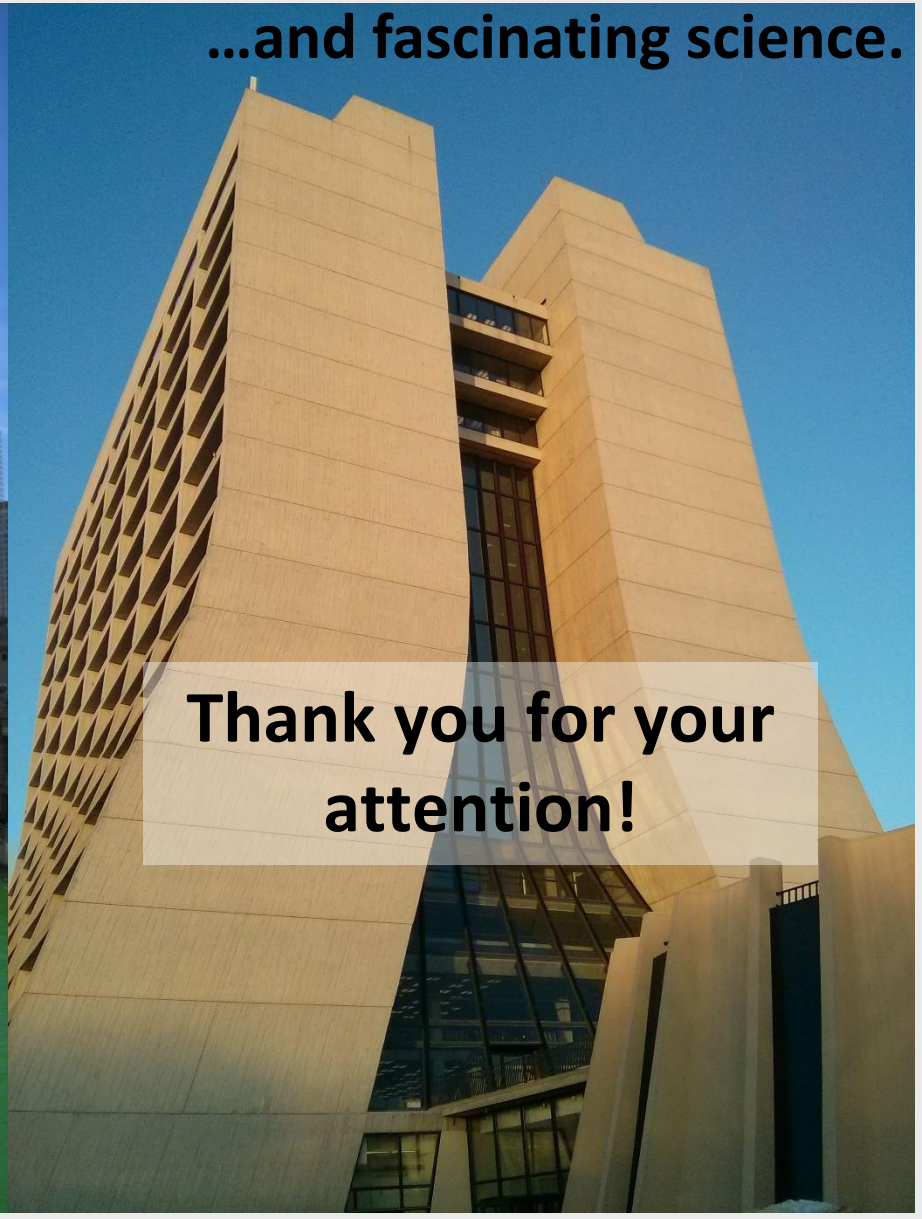


Thanks to…

- FRANZ team: M. Heilmann, B. Klump, O. Meusel, H. Podlech, U. Ratzinger, A. Schempp, P. Schneider, M. Schwarz, W. Schweizer, K. Volk.

- NNP group: A. Ates, M. Droba, S. Klaproth, O. Meusel, D. Noll, O. Payir, P. Schneider, H. Niebuhr, B. Scheible, K. Schulte, J. Wagner, K. Zerbe.

Blue skies,…
…green rivers…


…and fascinating science.
Thank you for your attention!

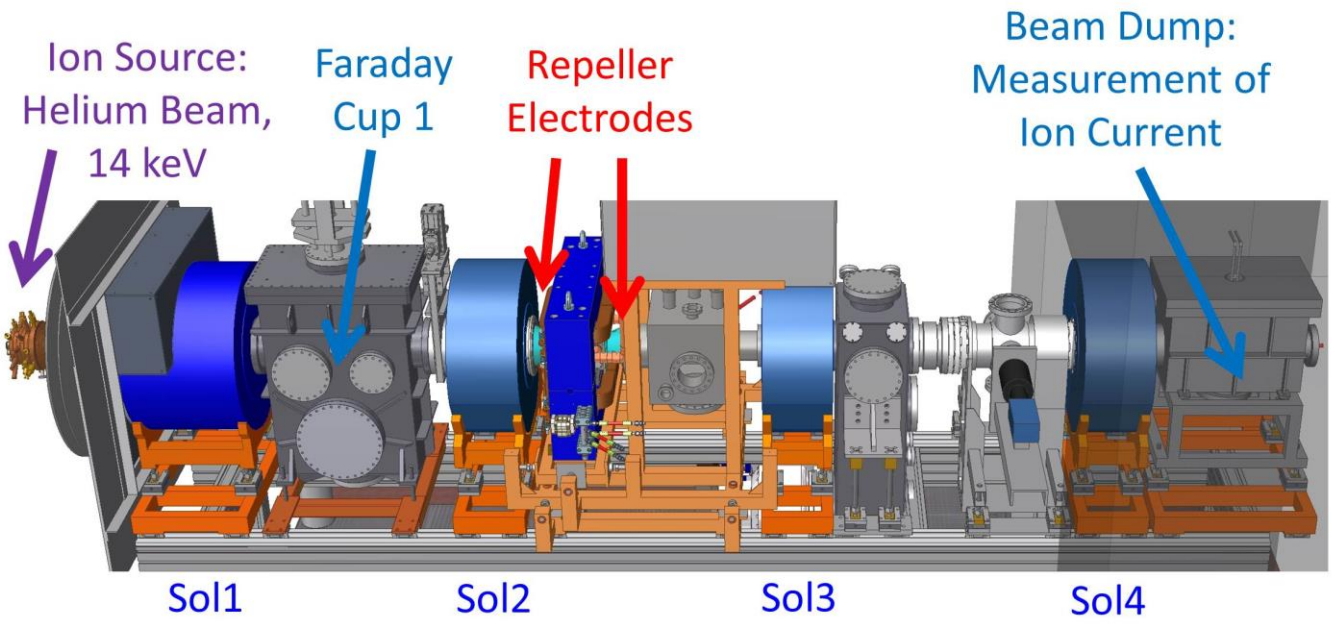
Backup

Beam Measurements

Measurements: DC Transmission

Helium Beam
E_b = 14 keV
I_{sol1} = 147 A
I_{sol2} = 70 A
I_{sol3} = 140 A
I_{sol4} = 183 A
V_{repell} = -200V

$$T_{\mathrm{lebt}} = \frac{(1.86 \pm 0.01)\,\mathrm{mA}}{(2.25 \pm 0.01)\,\mathrm{mA}} = (82.7 \pm 0.8)\,\%$$

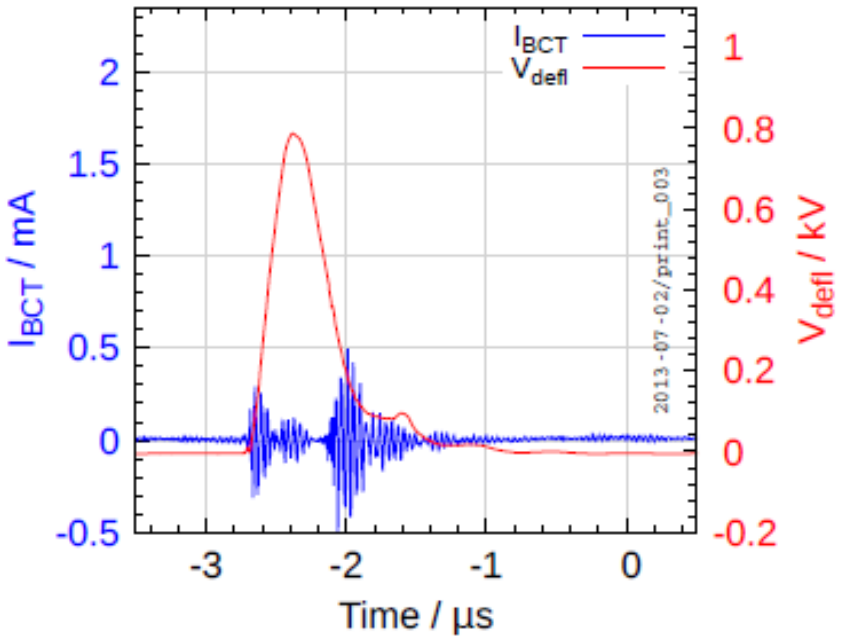


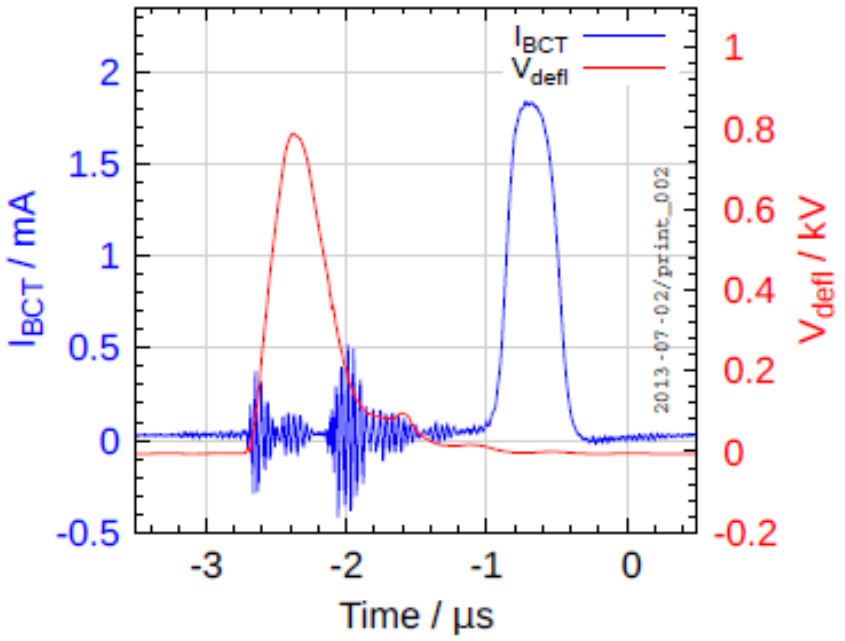
- Length: 3.5 m
- Perveance K = 1.76 · 10 −3 (equiv. 113 mA, p, 120keV)
- Test Ion Source

Measurements: Transmission of Chopped Beam

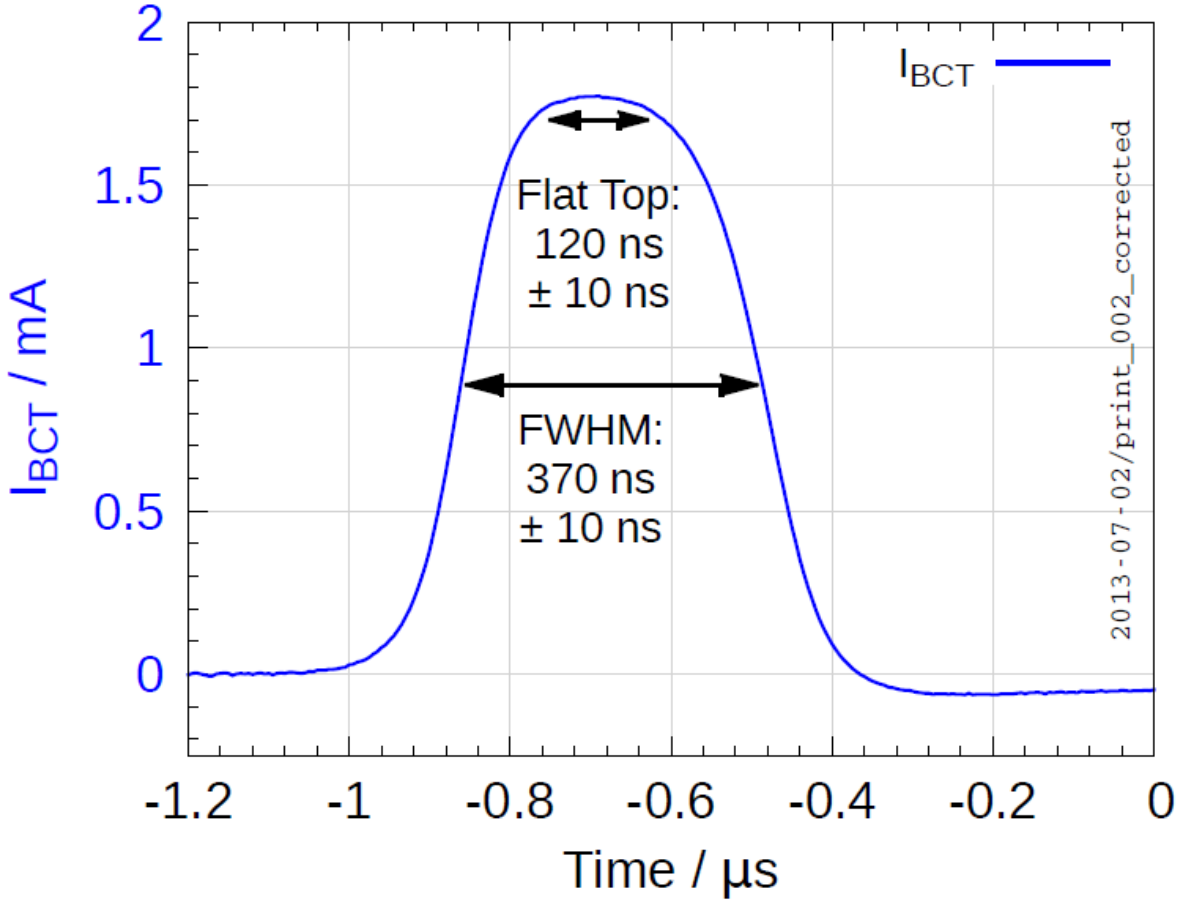
	DC Beam	*Chopped Beam*
Ion Species	He^+	He^+
Beam Energy W_b / keV	14	14
Max. Beam Current I_b / mA	**1.86 ± 0.02**	**1.77 ± 0.01**
Current I_{Sol1} / A	147	147
Current I_{Sol2} / A	70	70
Current I_{Sol3} / A	**140**	**169**
Current I_{Sol4} / A	190	190
Measurement Device	FC, Beam Dump	BCT
Repetition Rate	DC	257 kHz
Ratio of Chopped to DC Current	**(95.2 ± 1.6) %**	

Measurements: Noise Correction

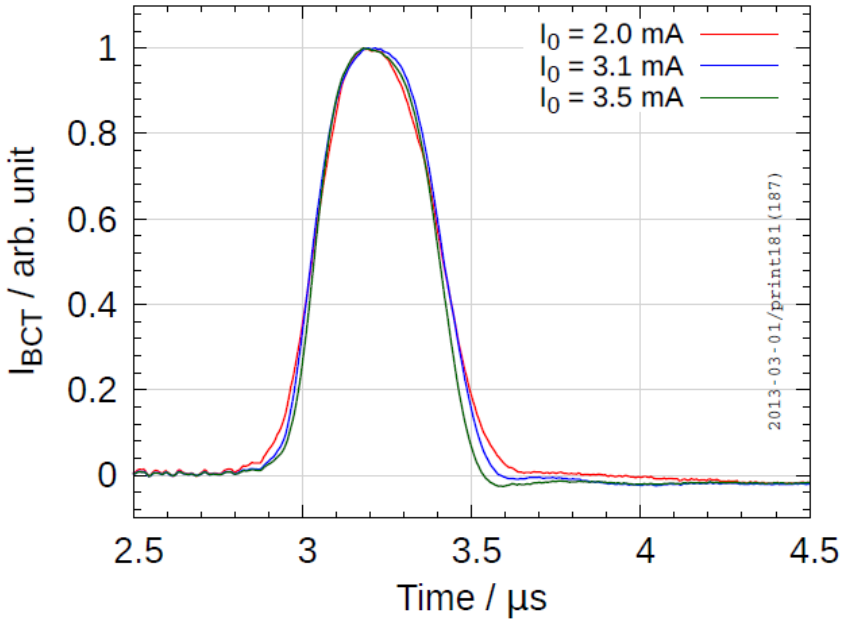


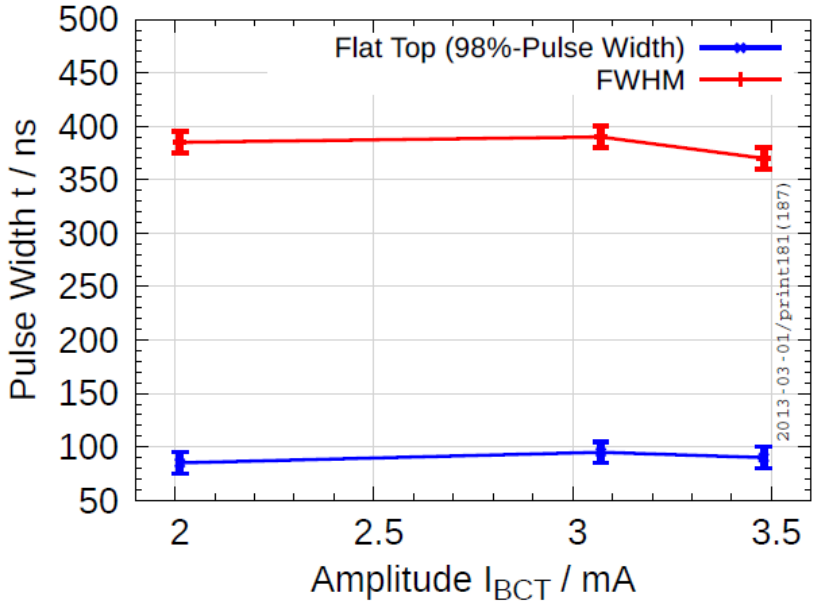


Measurements: Noise Correction

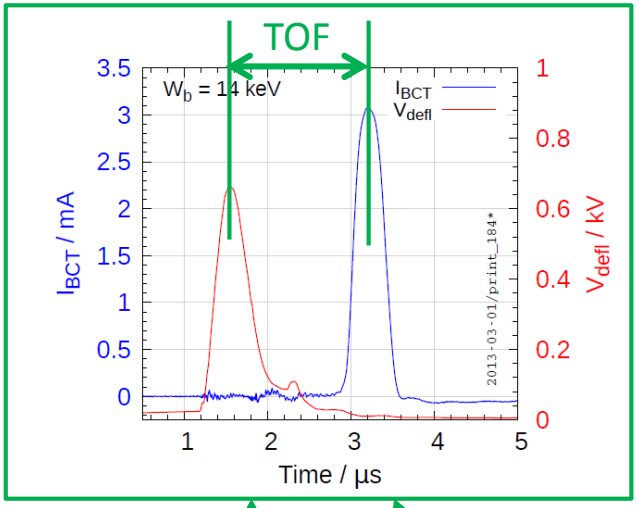


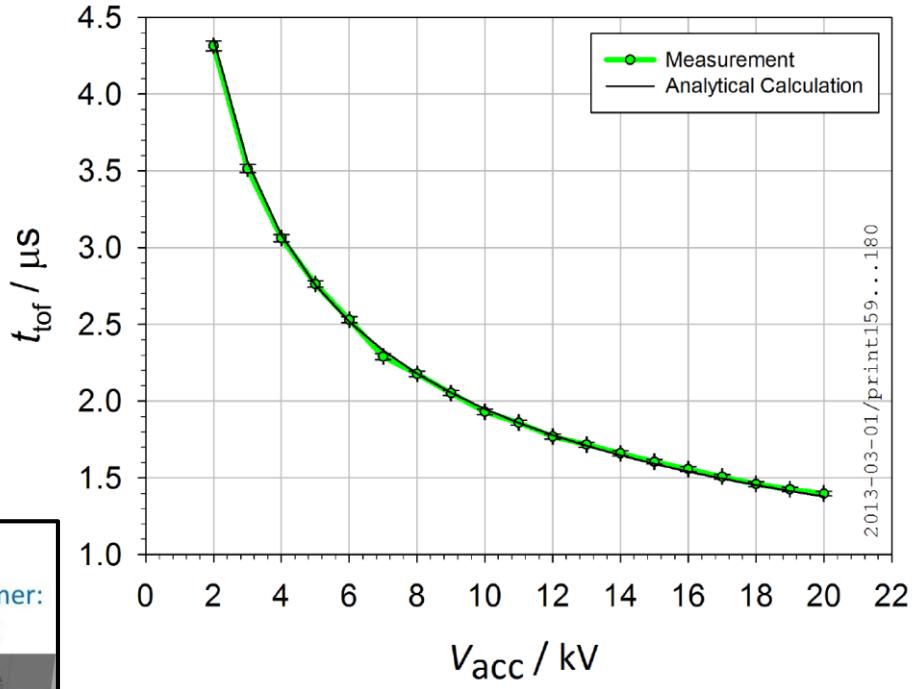
High-Perveance Beams

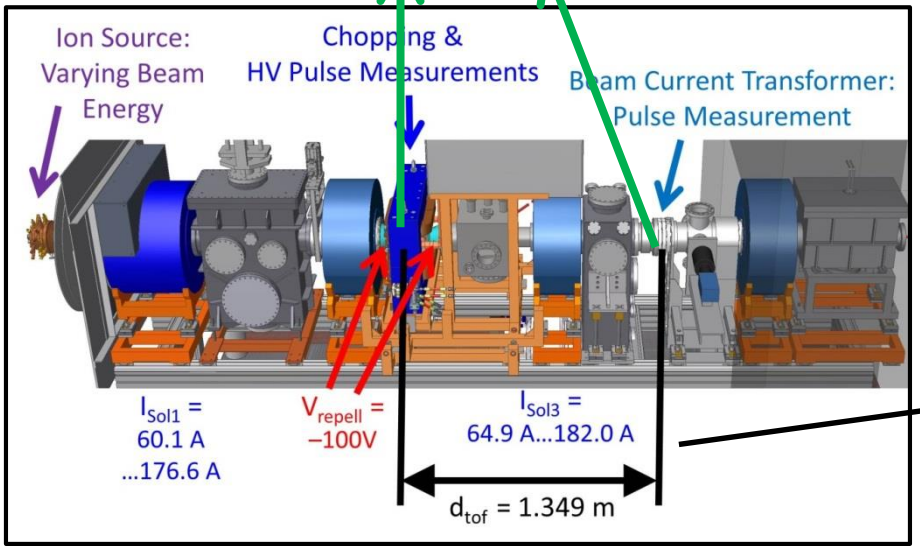




Measurements: Beam Energy Variation & TOF

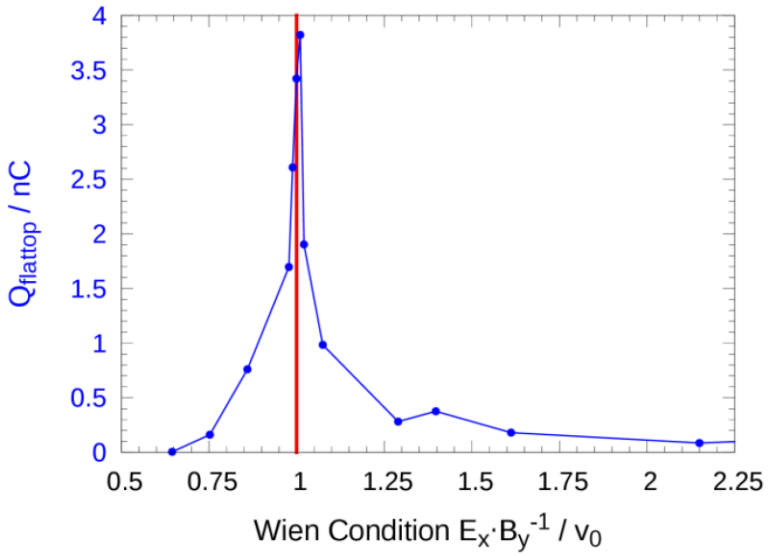






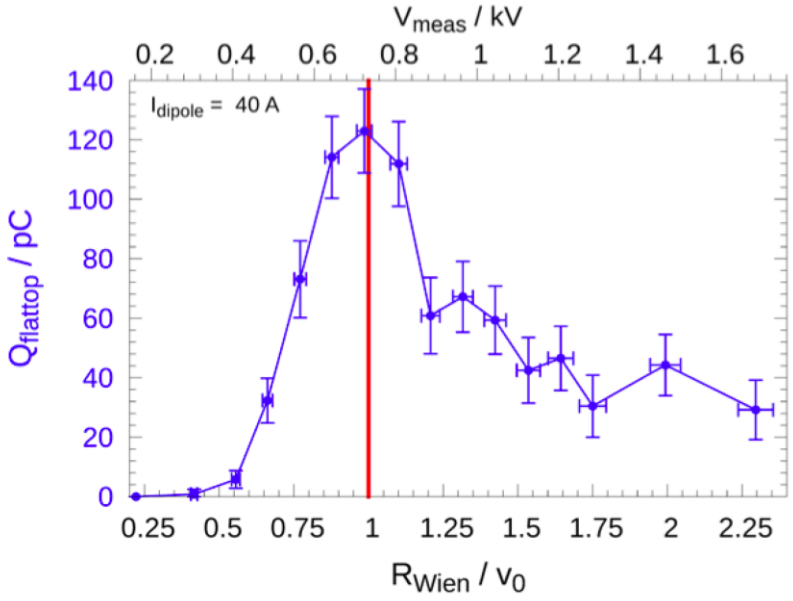
$$t_{\mathrm{tof}} = \frac{v_{\mathrm{p}}}{d_{\mathrm{tof}}}$$

Simulation



p+, 120 keV, 20 mm aperture

Measurement

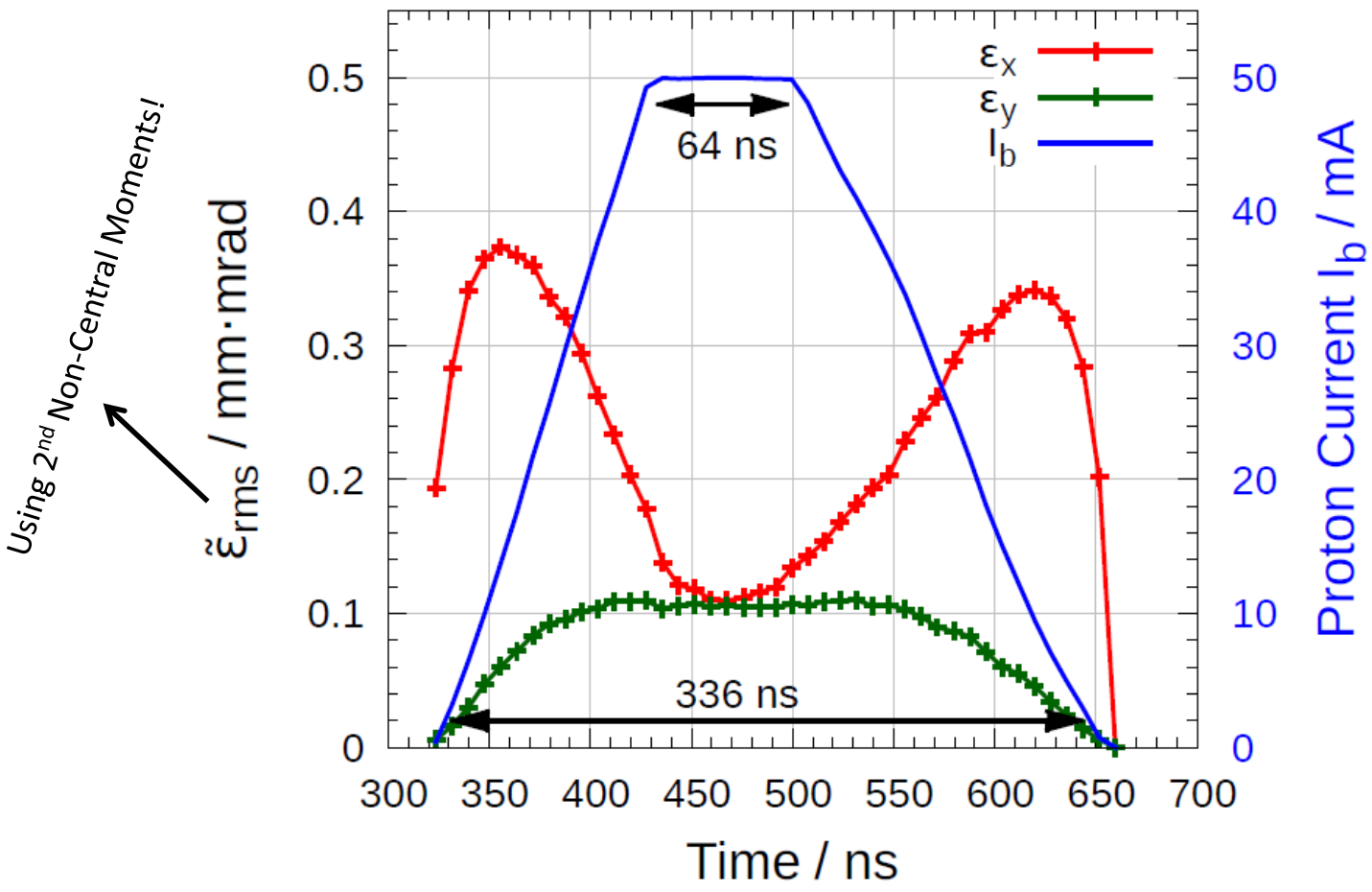


He⁺, 14 keV, 50 mm aperture

Simulations

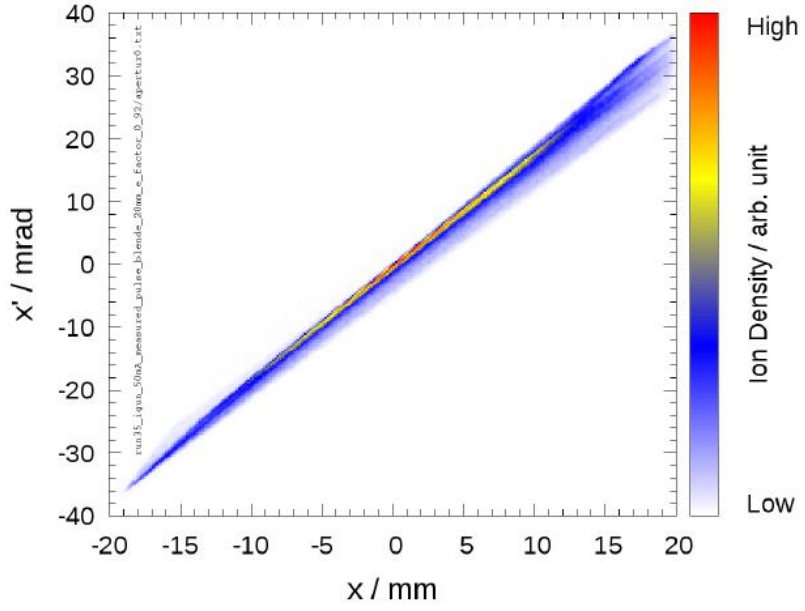
Pulsed Beam Dynamics: Beam Shaping

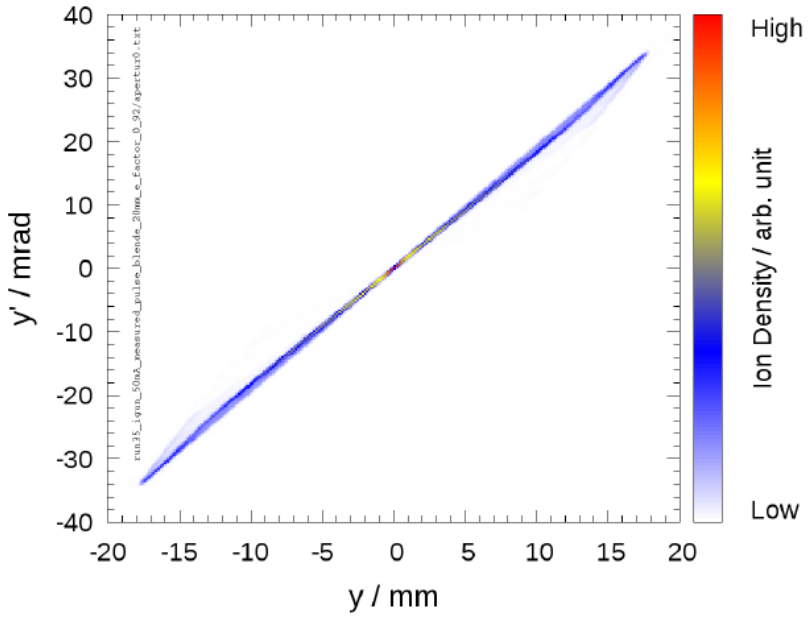
Simulated Beam Pulse Behind Chopper



Pulsed Beam Dynamics: Beam Shaping

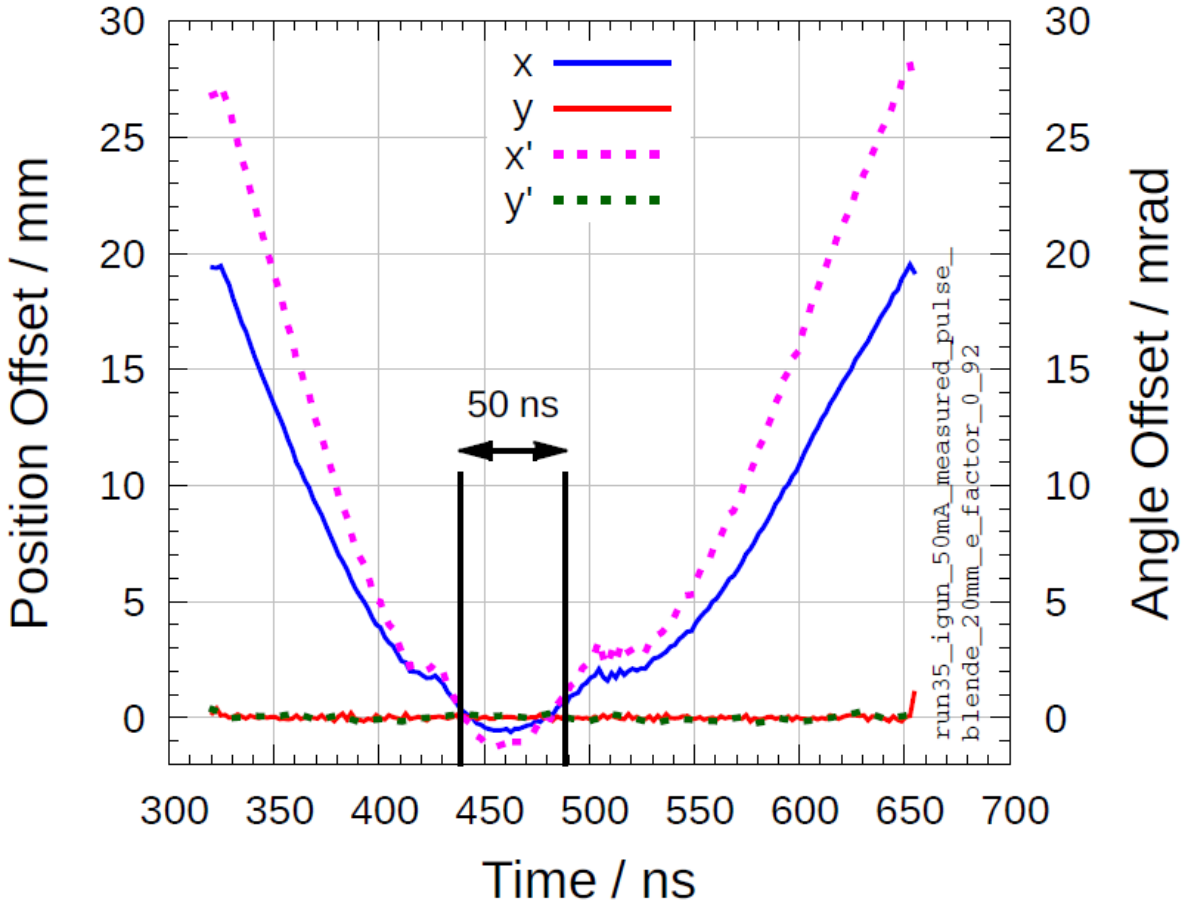
Simulated Beam Pulse Behind Chopper



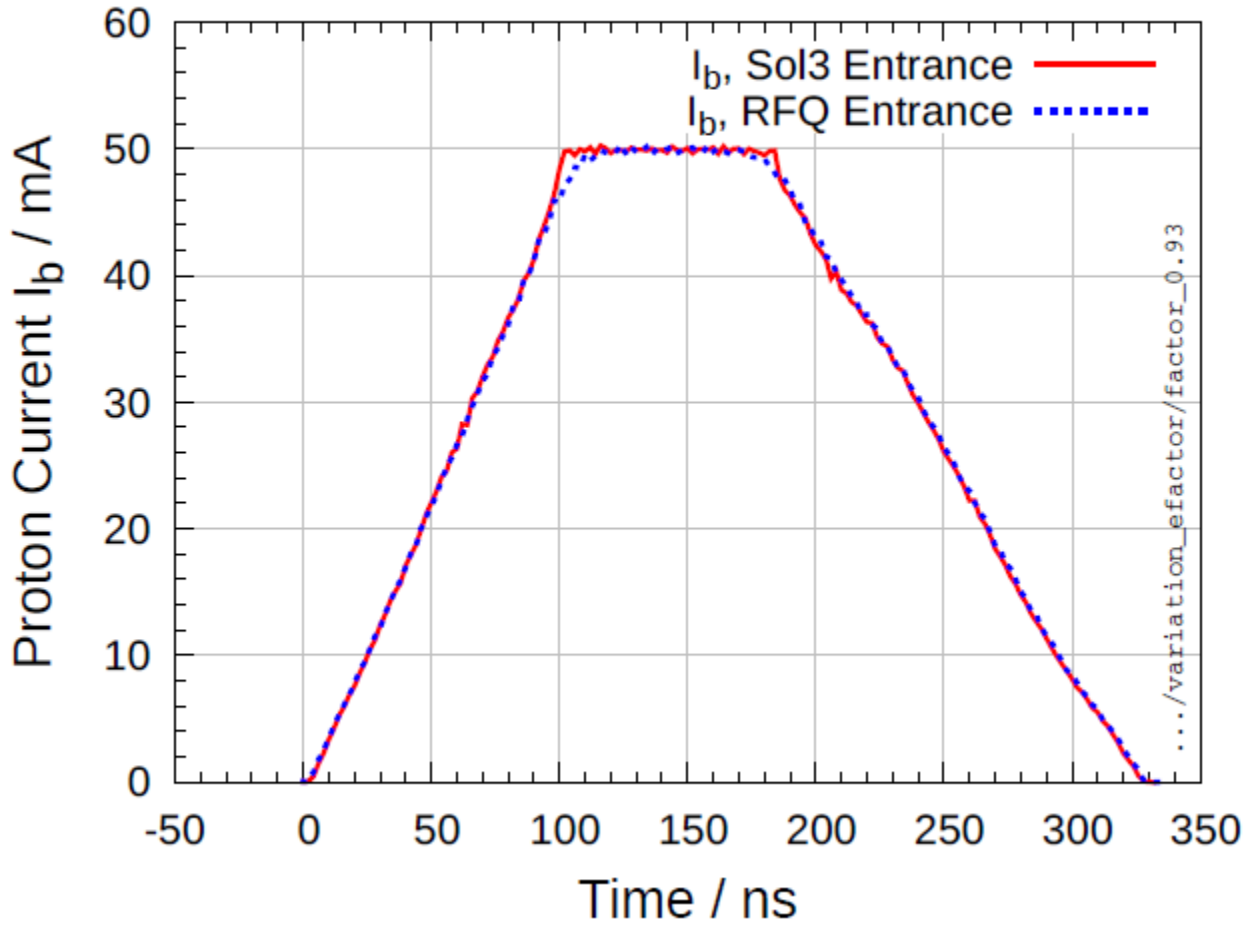


Pulsed Beam Dynamics: Beam Shaping

Offsets Behind Chopper (no solenoids)

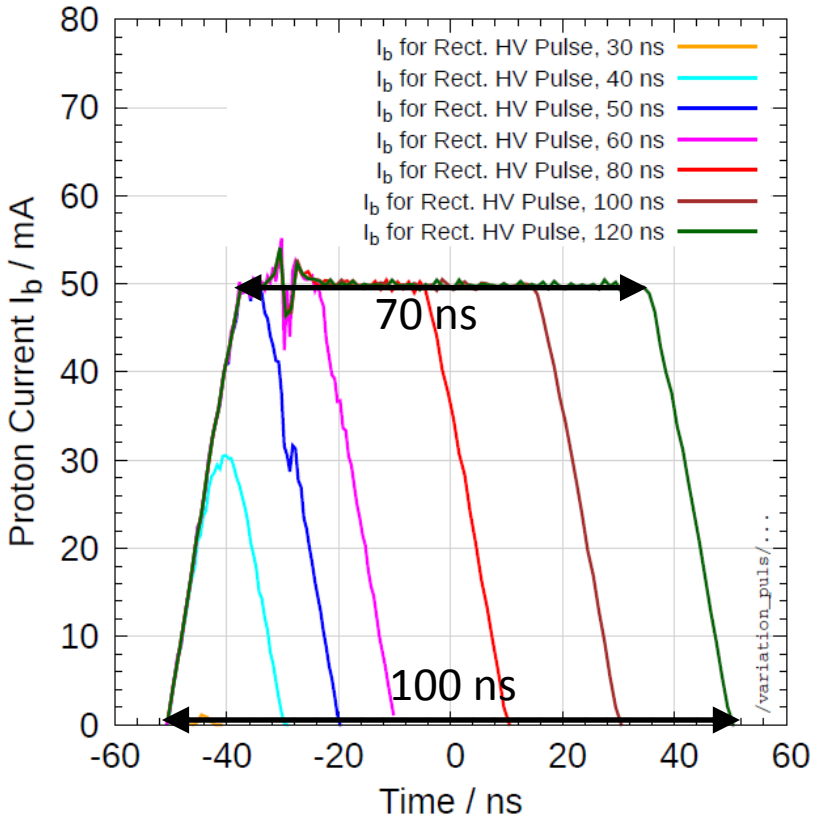


Pulsed Beam Dynamics: Beam Shaping

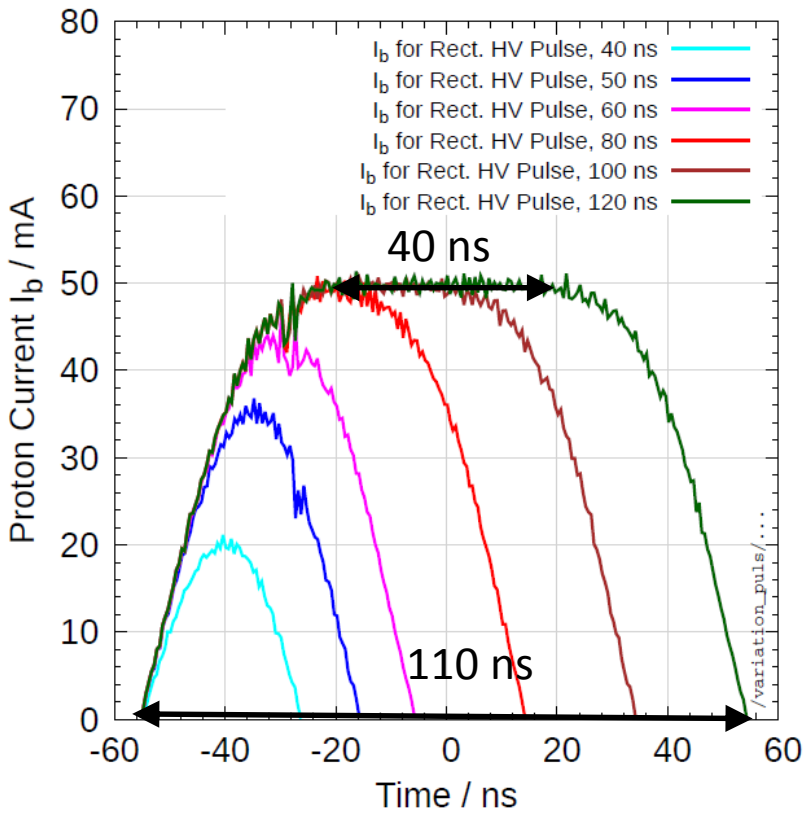


Pulsed Beam Dynamics: Beam Shaping

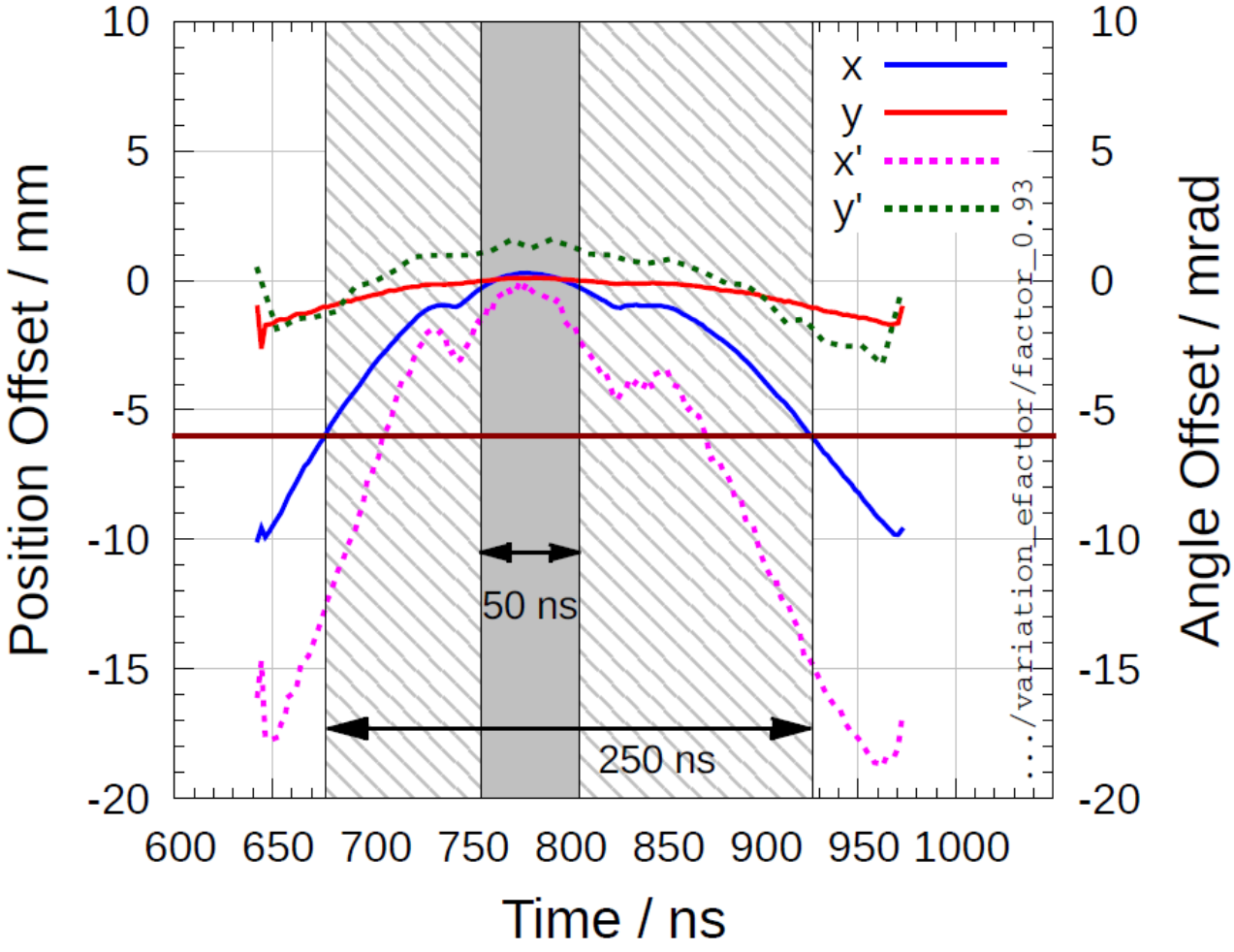
Sim. Beam Pulse Behind Chopper



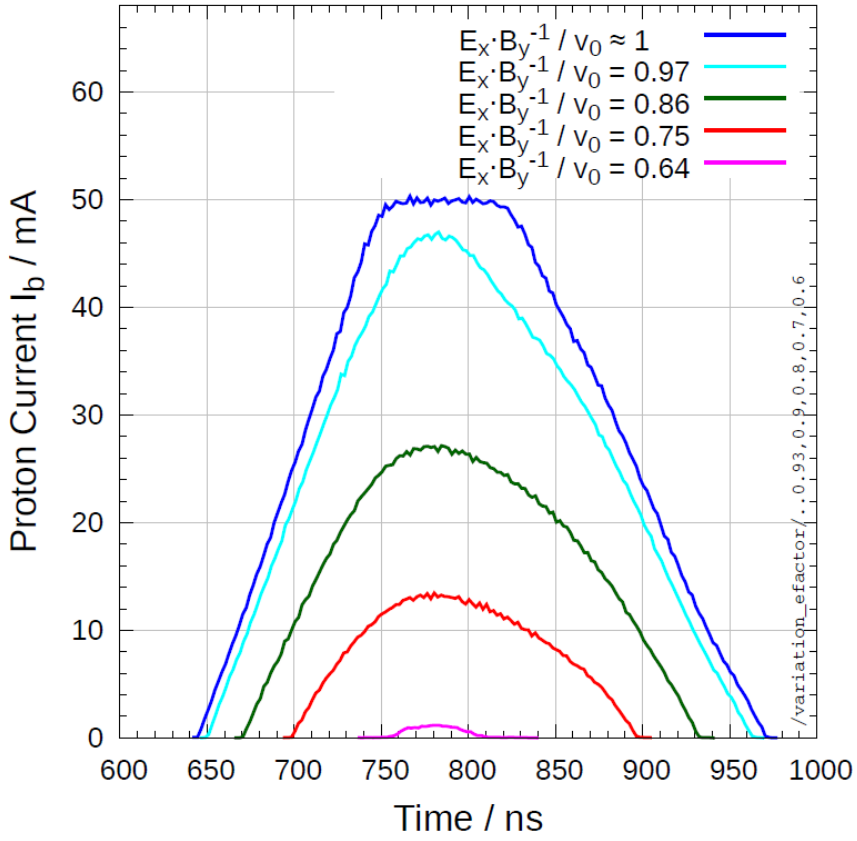
Sim. Beam Pulse at RFQ Entrance

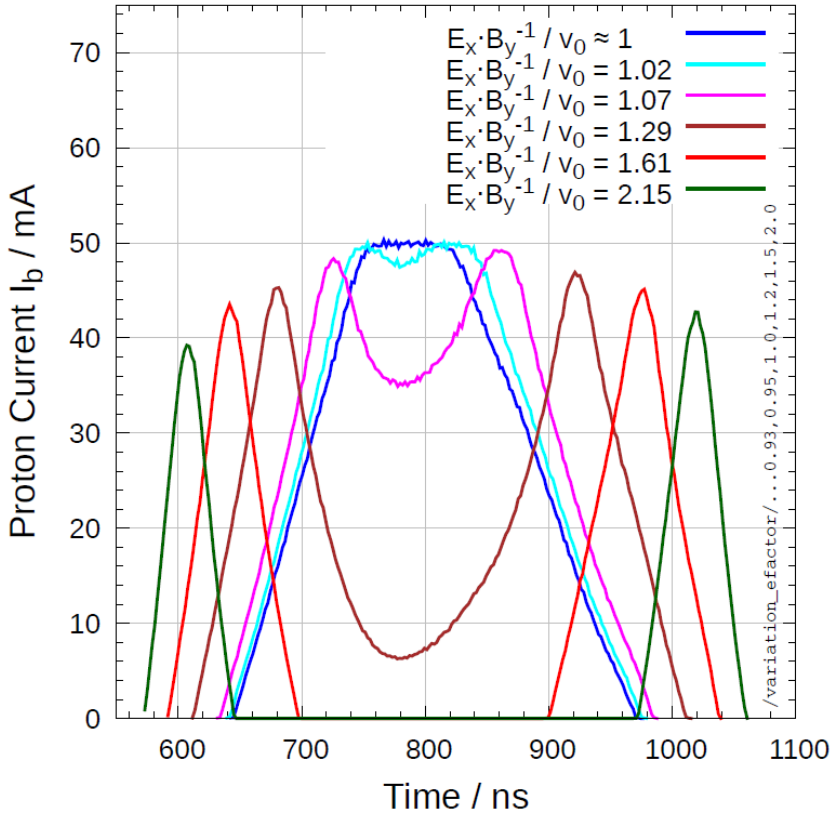


Pulsed Beam Dynamics: Beam Shaping

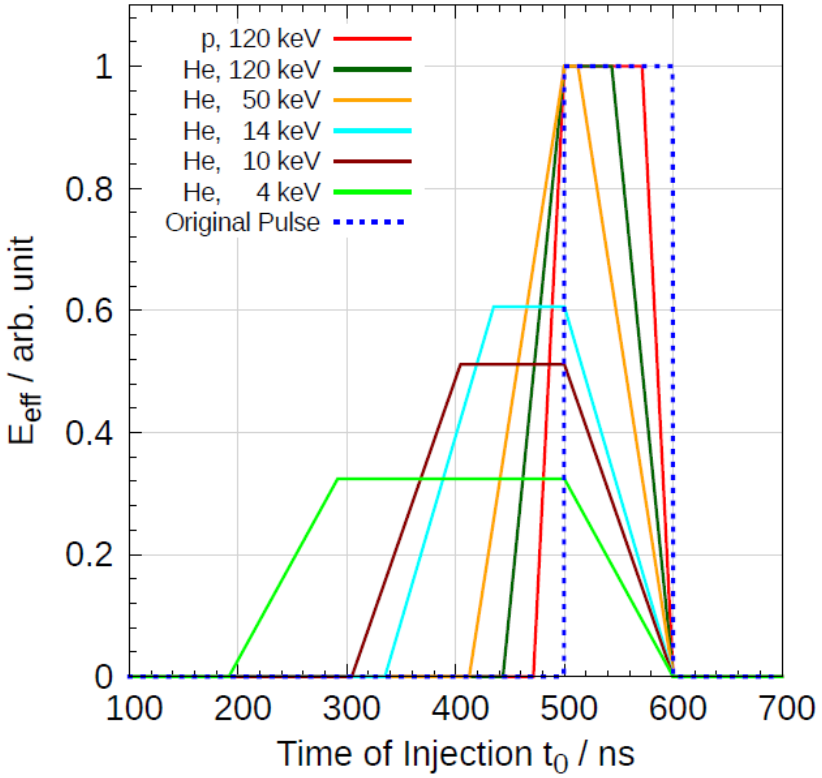


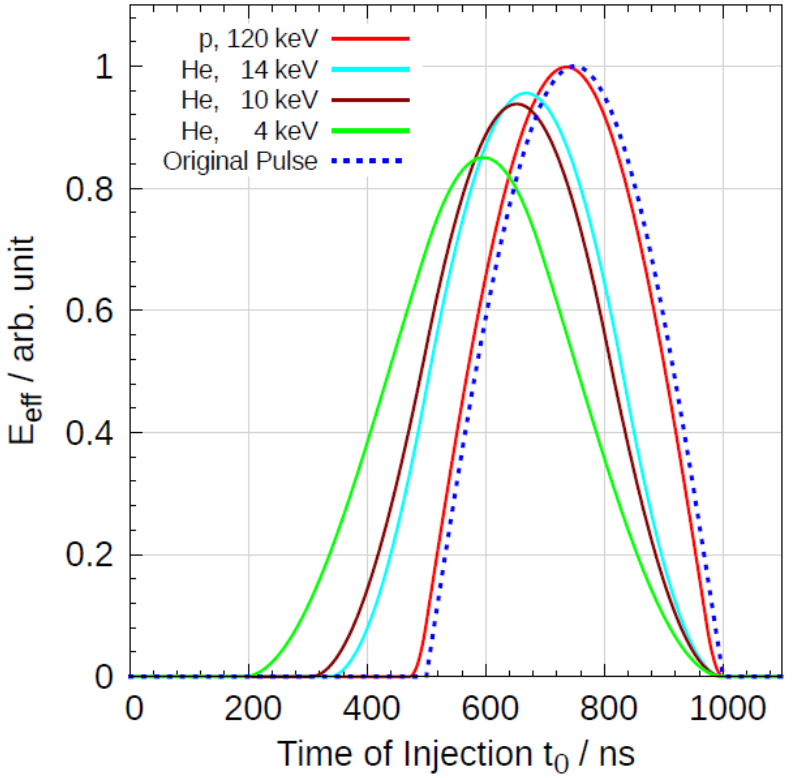
Simulations: Variation of Wien Ratio





Effective Fields

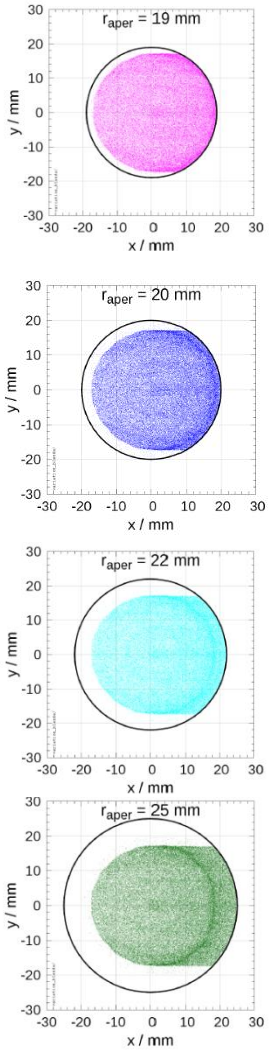




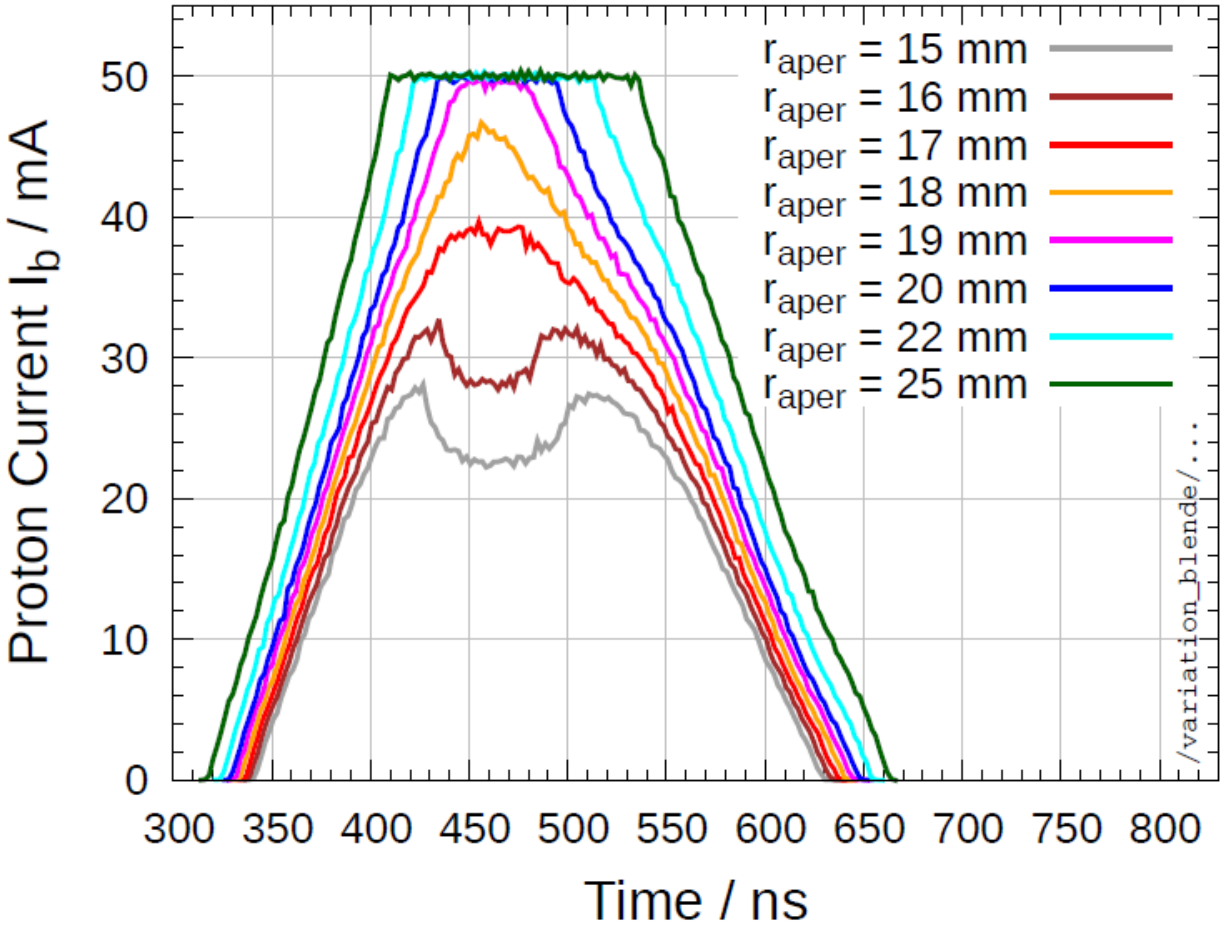
$$f_{\mathrm{tof}} = \frac{E_{\mathrm{eff}}^{\max}}{E^{\max}}$$

$$E_{\mathrm{eff}}(t_0) = \frac{1}{t_{\mathrm{tof}}} \int_{t_0}^{t_{\mathrm{exit}}} E(t)\,\mathrm{d}t$$

Pulsed Beam Dynamics: Beam Shaping

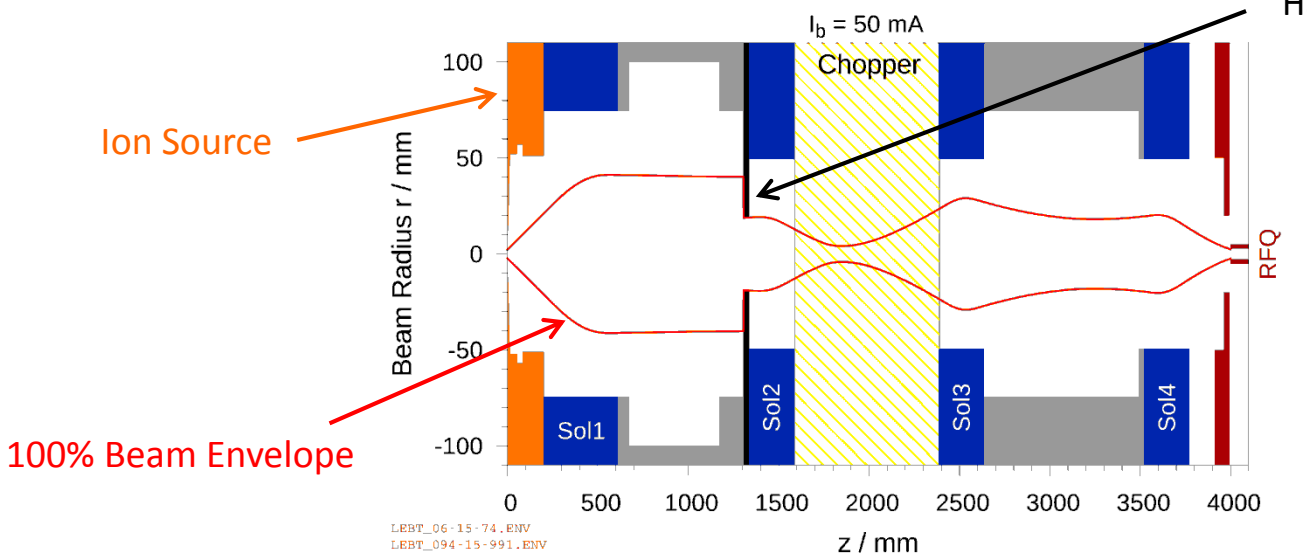


Variation of Aperture Radius



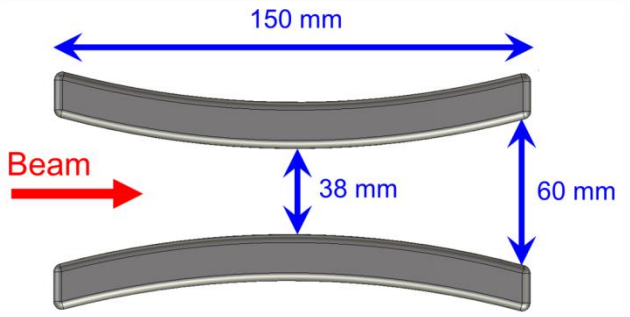
DC Beam Transport

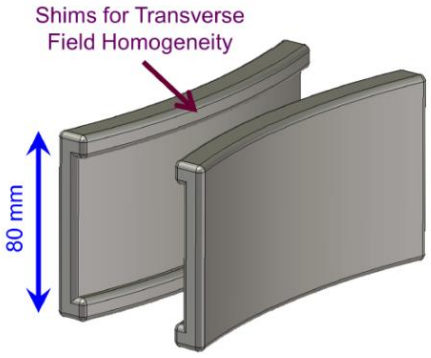
Beam Matching in LEBT Section



p, 120 keV:
Transmission: 98%

Electric Deflection Plates





Matching of Defl. Forces

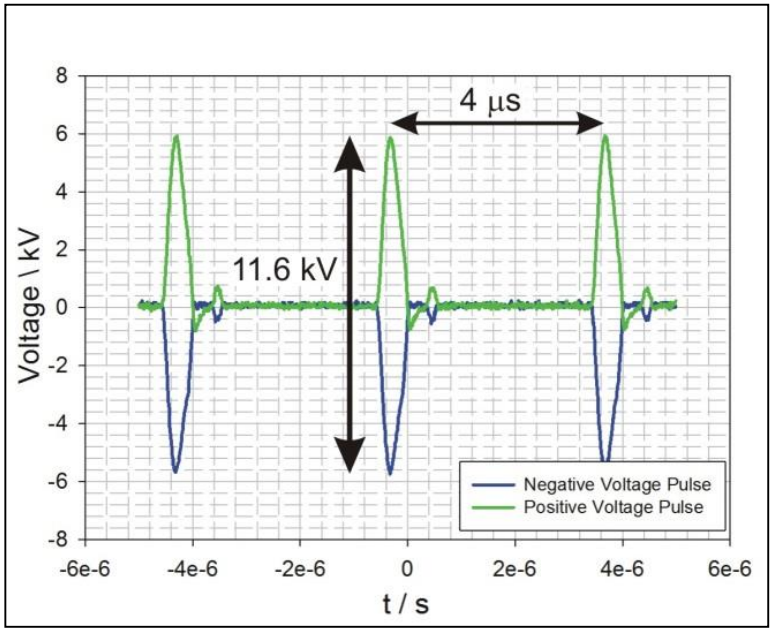
$$\int (\vec{F}_{\mathrm{elec}} + \vec{F}_{\mathrm{mag}})\ \mathrm{d}z \stackrel{!}{=} 0$$

$$\int q \cdot (\vec{E} + \vec{v}_{\mathrm{p}} \times \vec{B})\ \mathrm{d}z \stackrel{!}{=} 0$$

HV Pulse Generator

HV Pulse Generator

Requirements:
f_{rep} =250 kHz ✓
V_0 = ± 5 kV ✓

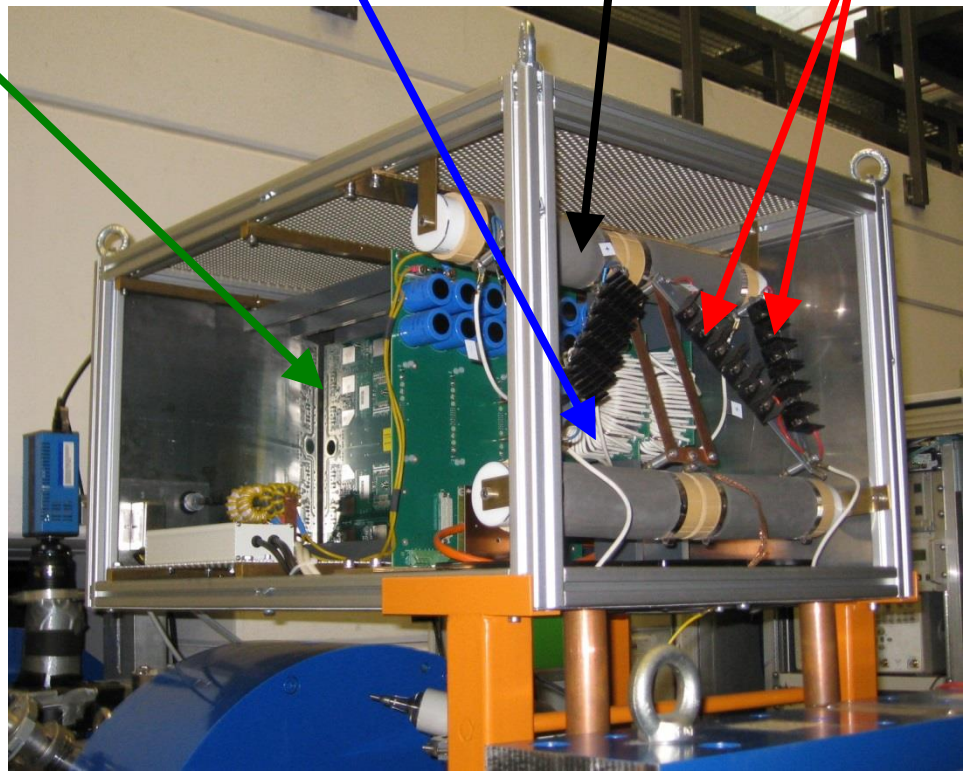


MOSFETs (*Thomson*-Board)

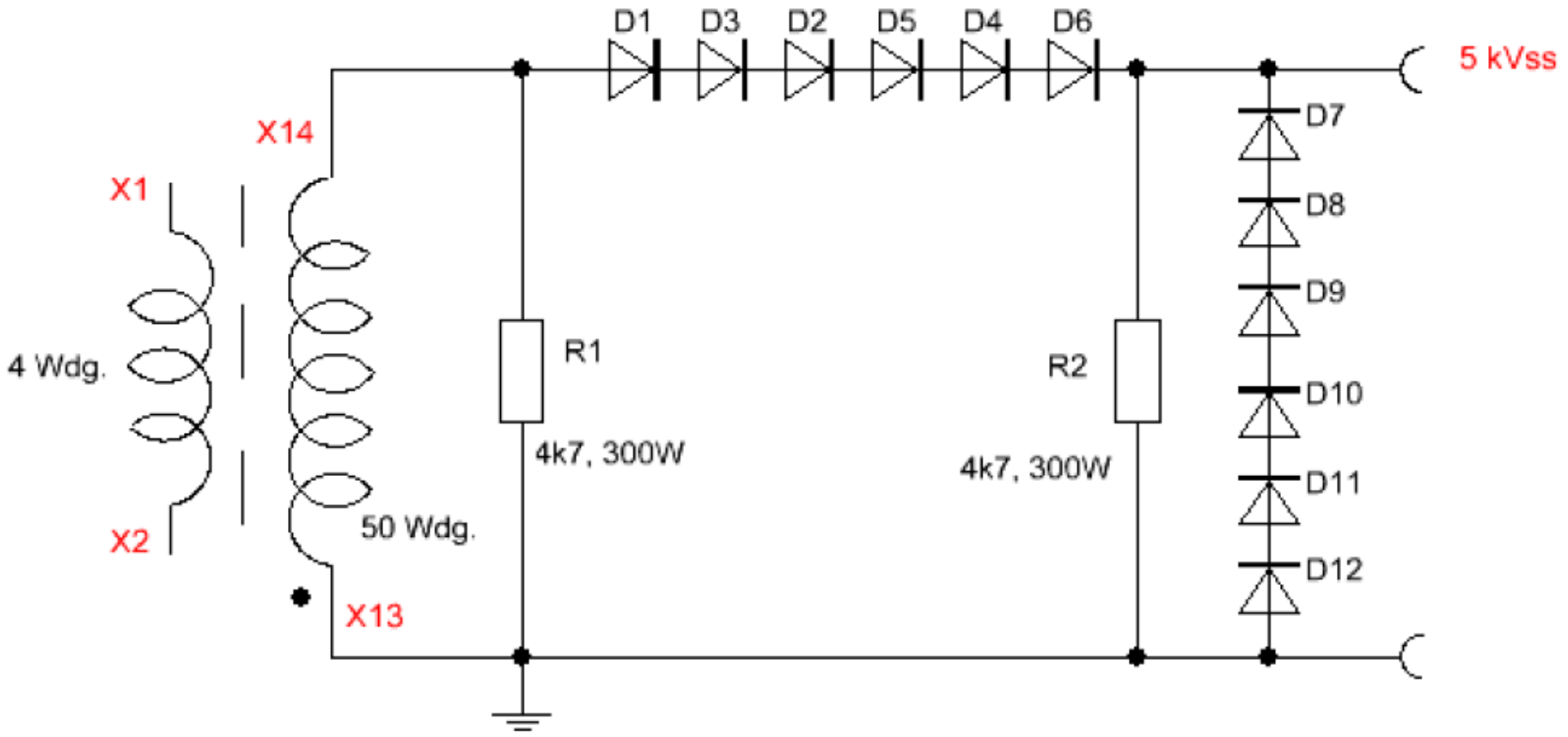
Ferrite Cores

R = 47 kΩ

Diodes



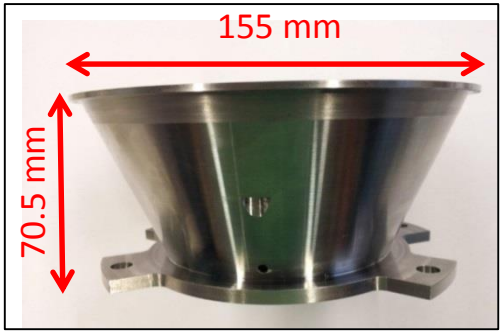
HV Pulse Generator



Repeller Electrodes/ Shortening Tubes

Electric Deflection Field:
→ Electron Flux on Deflector Plates
→ Decompensation of Proton Beam
→ Installation of Repeller Electrodes

In situ HV tests:
V = - 5 kV ✓
Requirements: V = -0.5 kV ✓

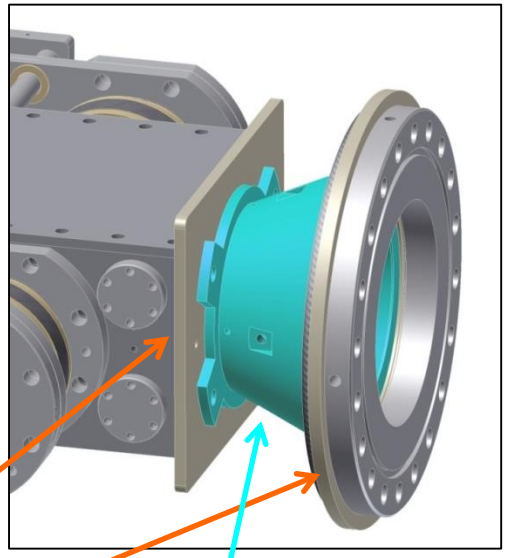


Beam Potential:

$$\Phi(r) = \frac{I_b}{4\pi \cdot \varepsilon_0 \cdot v_p}\left[1 + 2\ln\left(\frac{r_D}{r_b}\right) - \frac{r^2}{r_b^2}\right]$$

Homogenous Beam,
I_b = 50 mA, r_b = 10 mm
→ **Φ_b = 400 V**

→ 500 V_{repell} required.

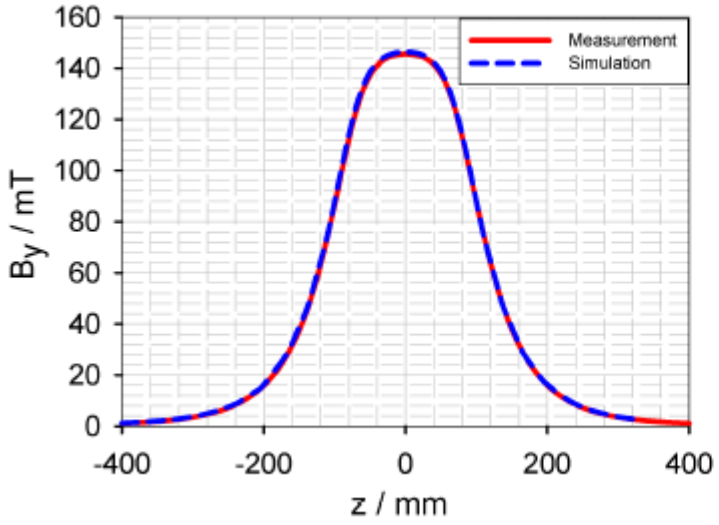


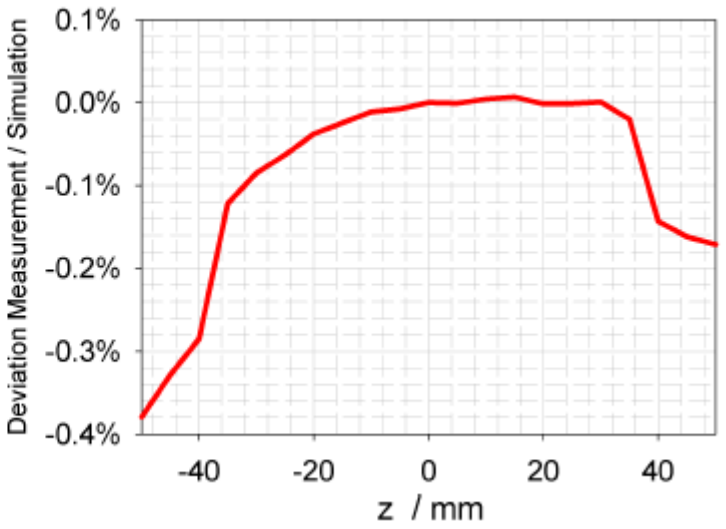
Insulating Flanges & Sleeves

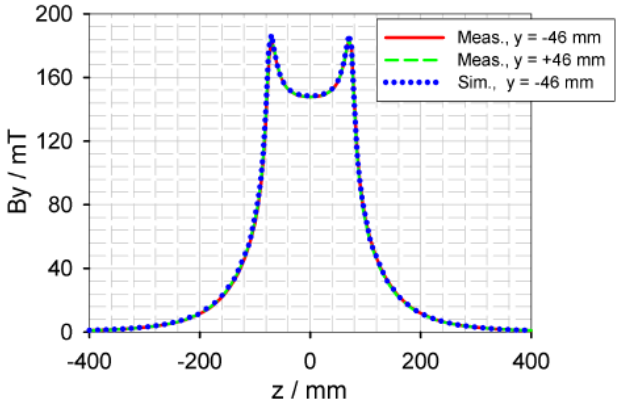
Material: Magnetic Steel

Technical Design

Chopper Dipole: Field Measurements

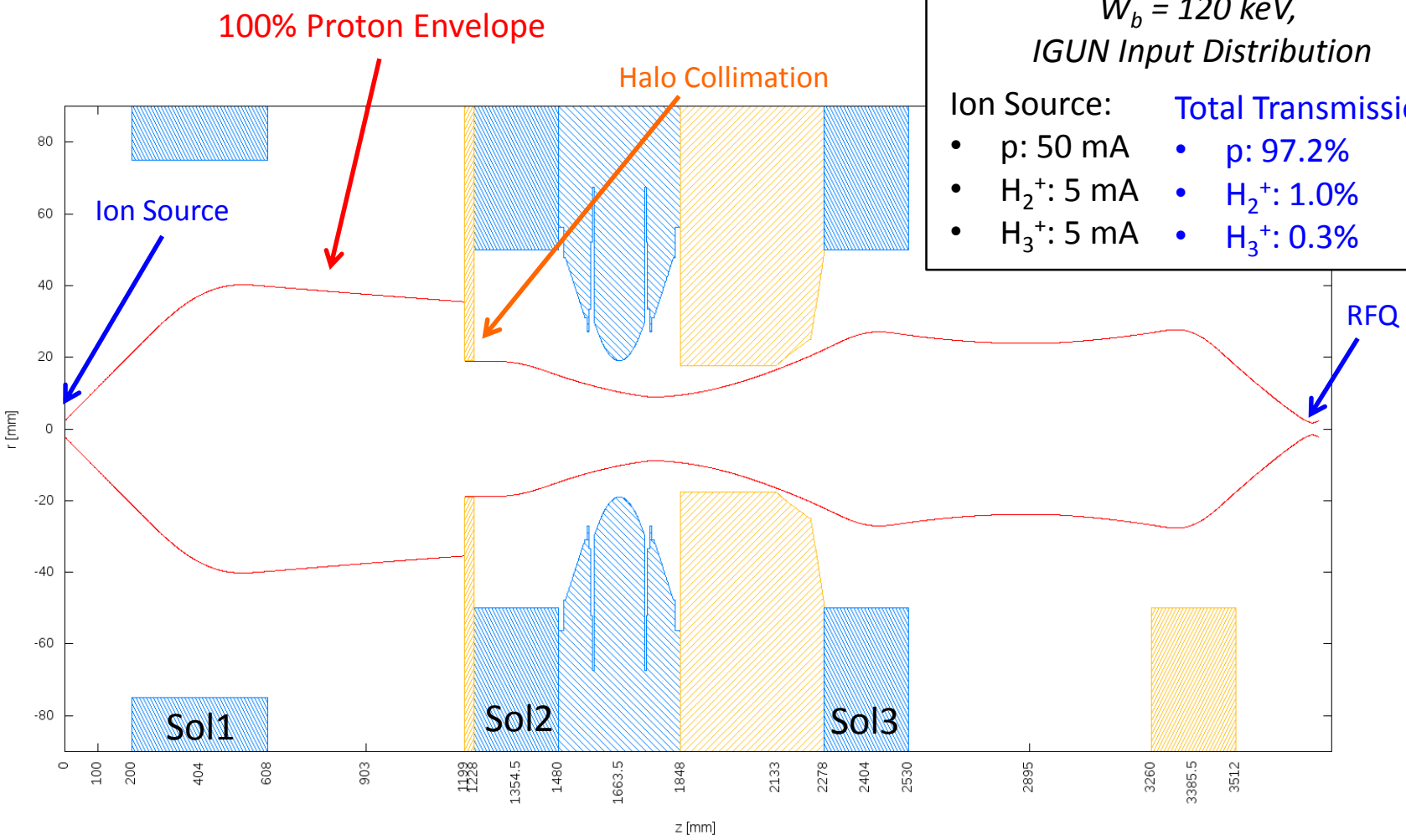






LEBT Simulations

DC Beam Transport



W_b = 120 keV,
IGUN Input Distribution

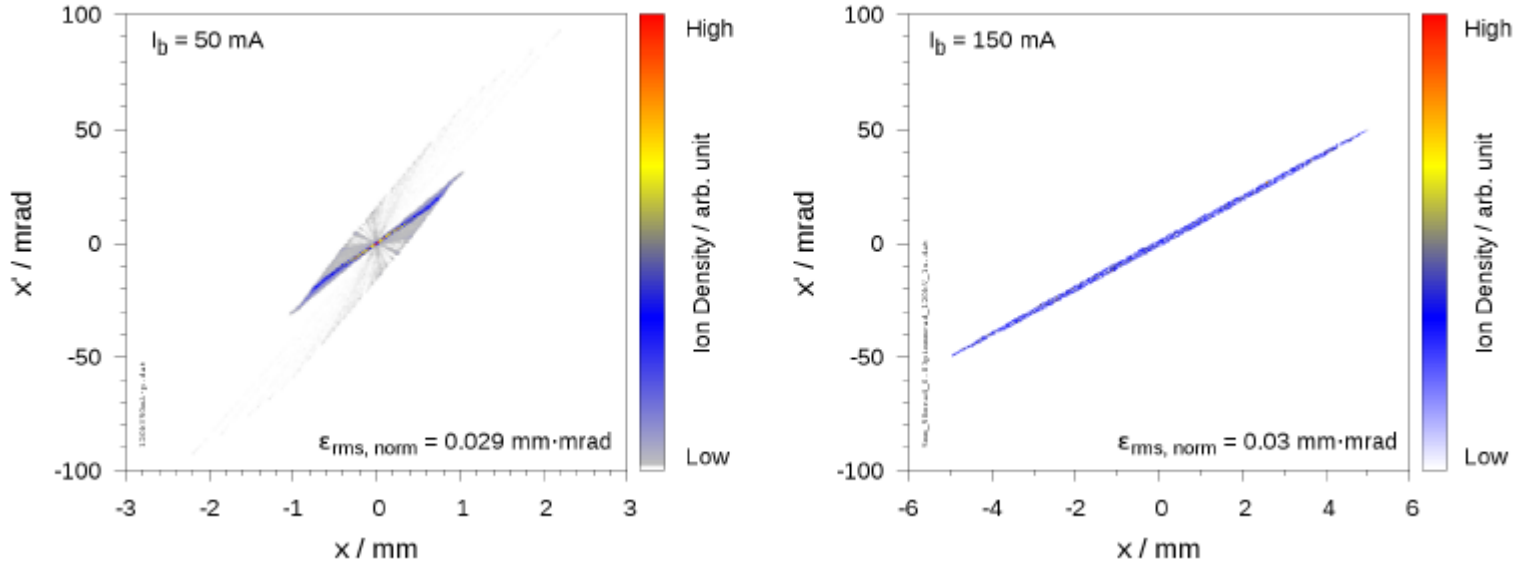
Ion Source:
- p: 50 mA
- H_2^+: 5 mA
- H_3^+: 5 mA

Total Transmission
- p: 97.2%
- H_2^+: 1.0%
- H_3^+: 0.3%

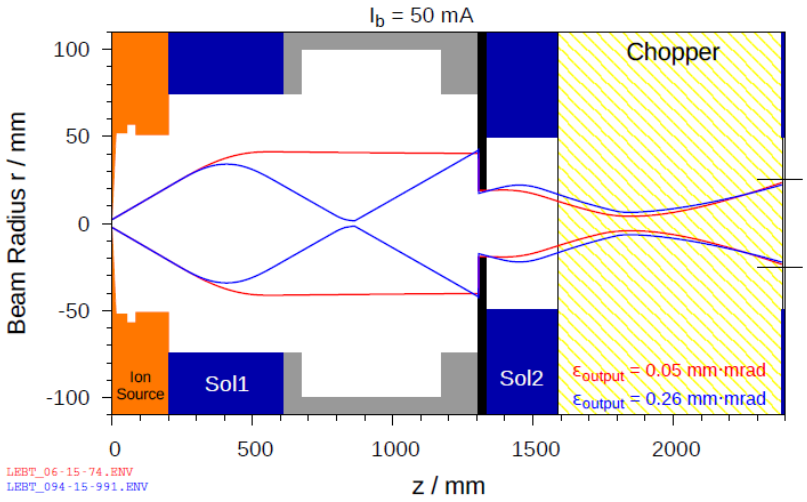
Transport Simulation (Lintra)

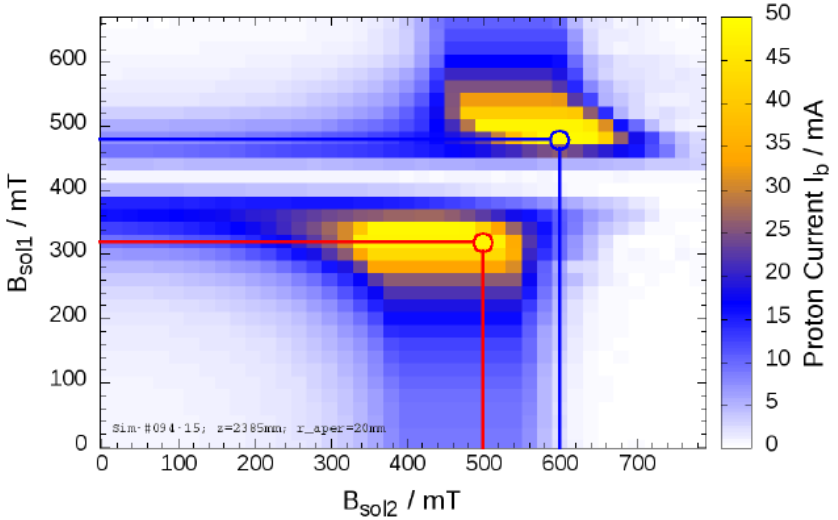
DC Beam Transport

Ion Source Distributions

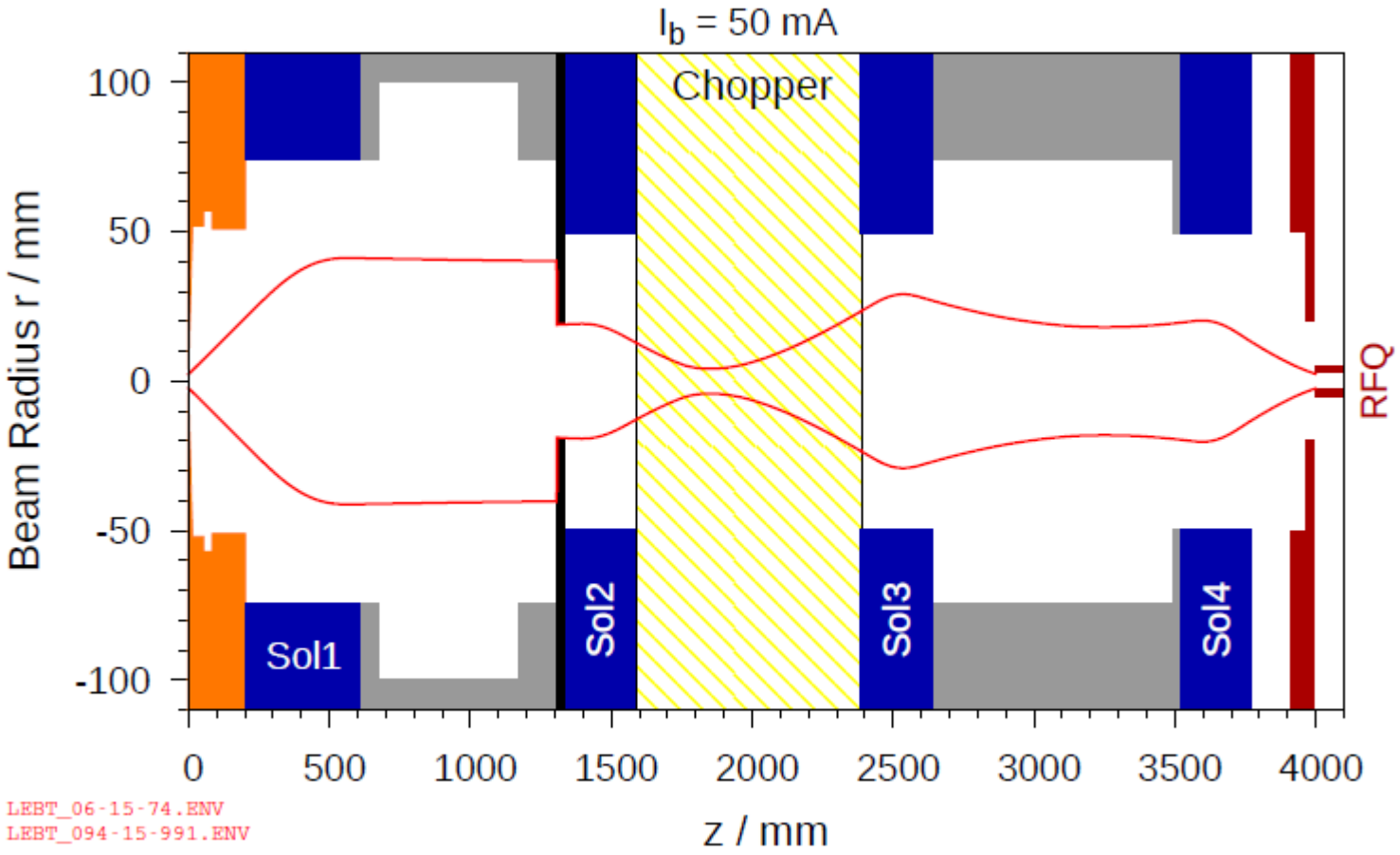


DC Beam Transport

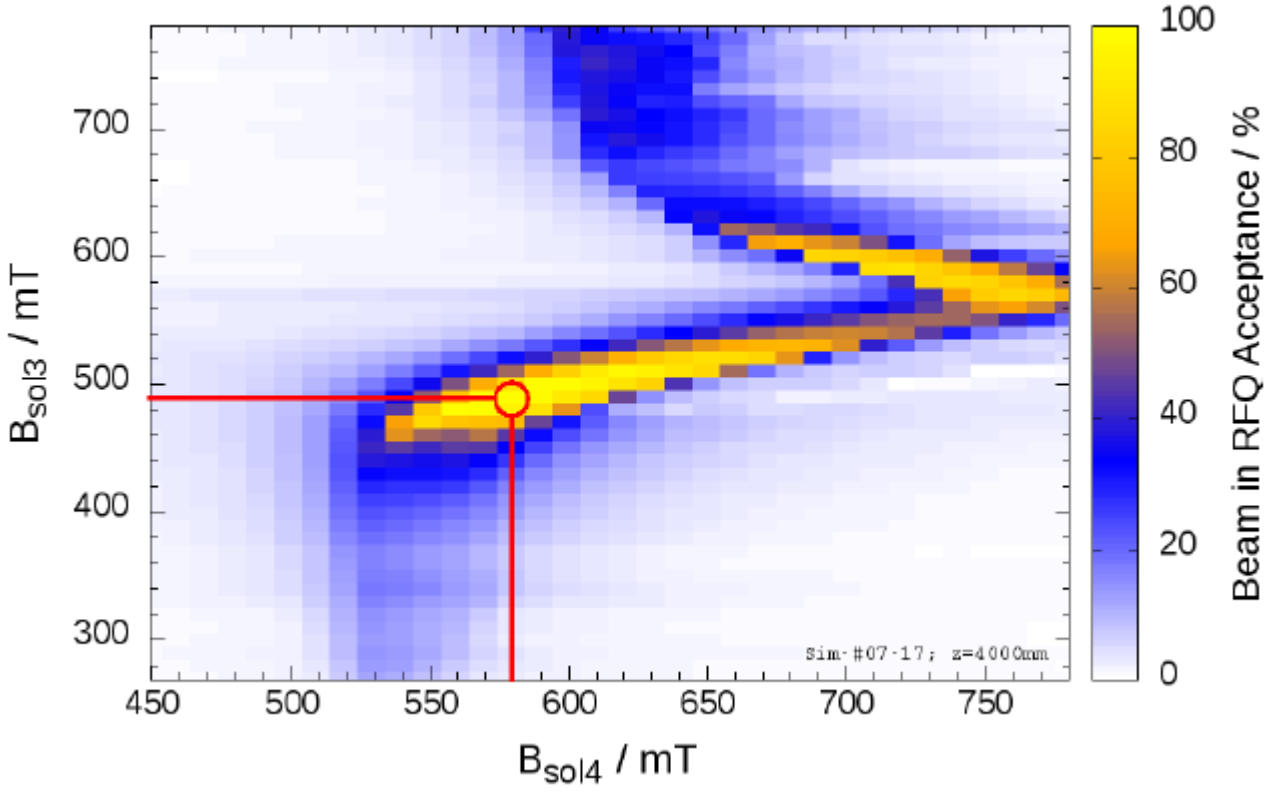




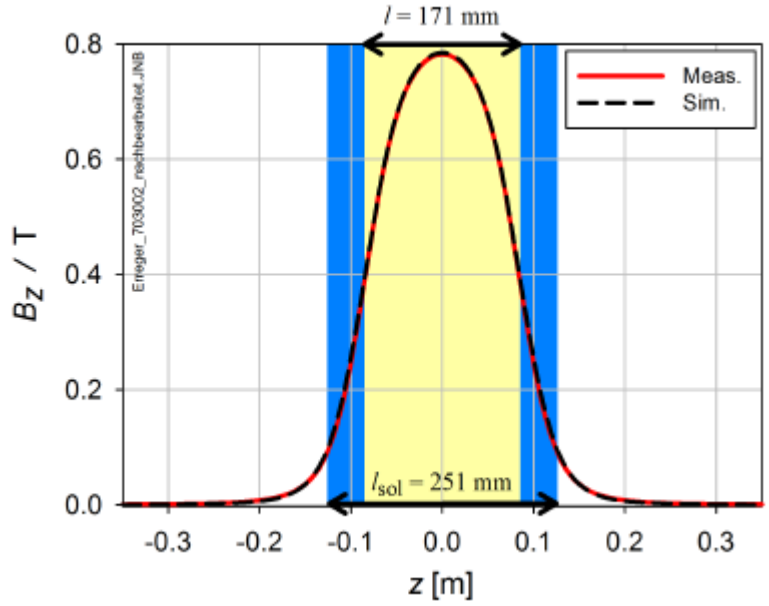
DC Beam Transport

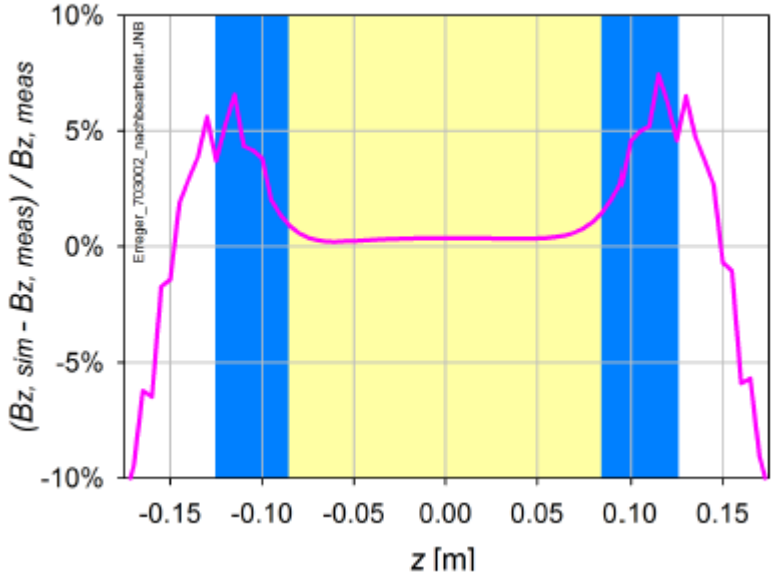


DC Beam Transport: RFQ Matching



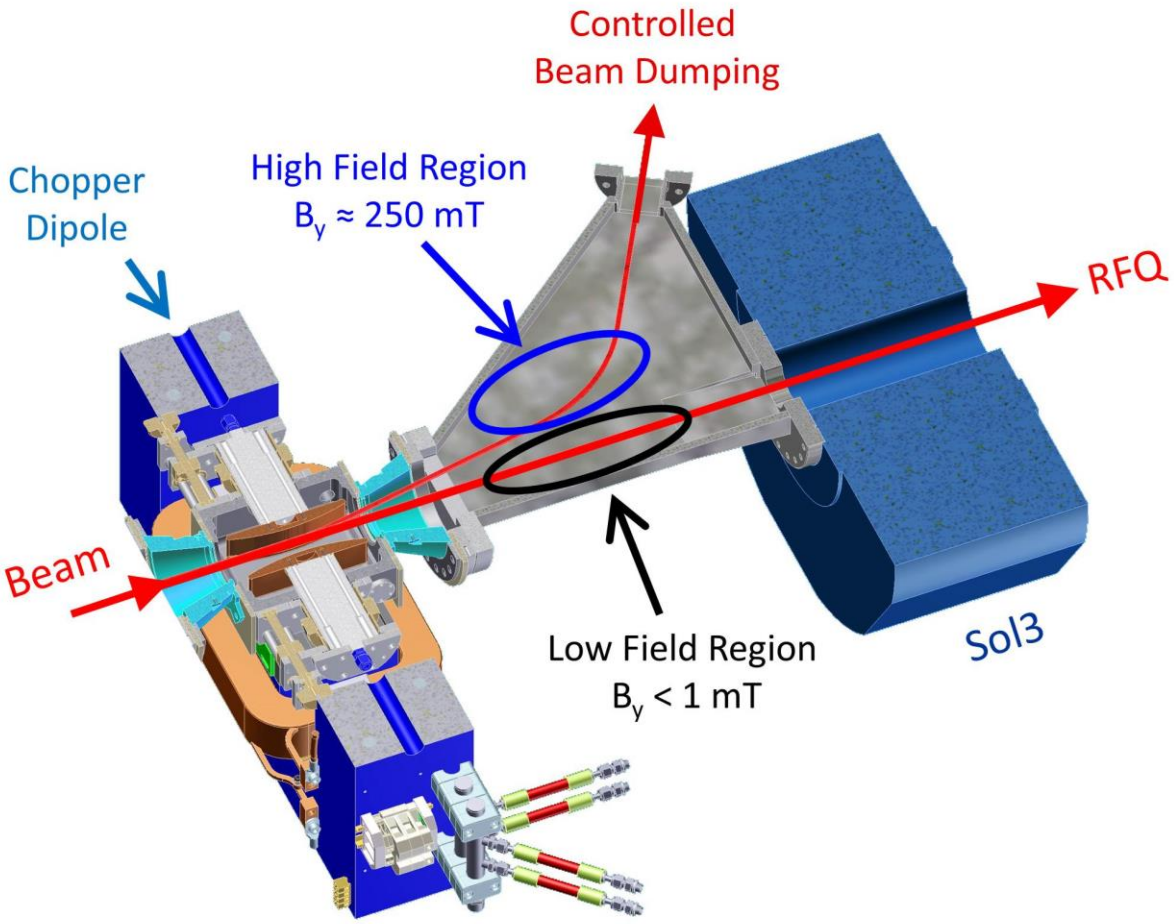
DC Beam Transport





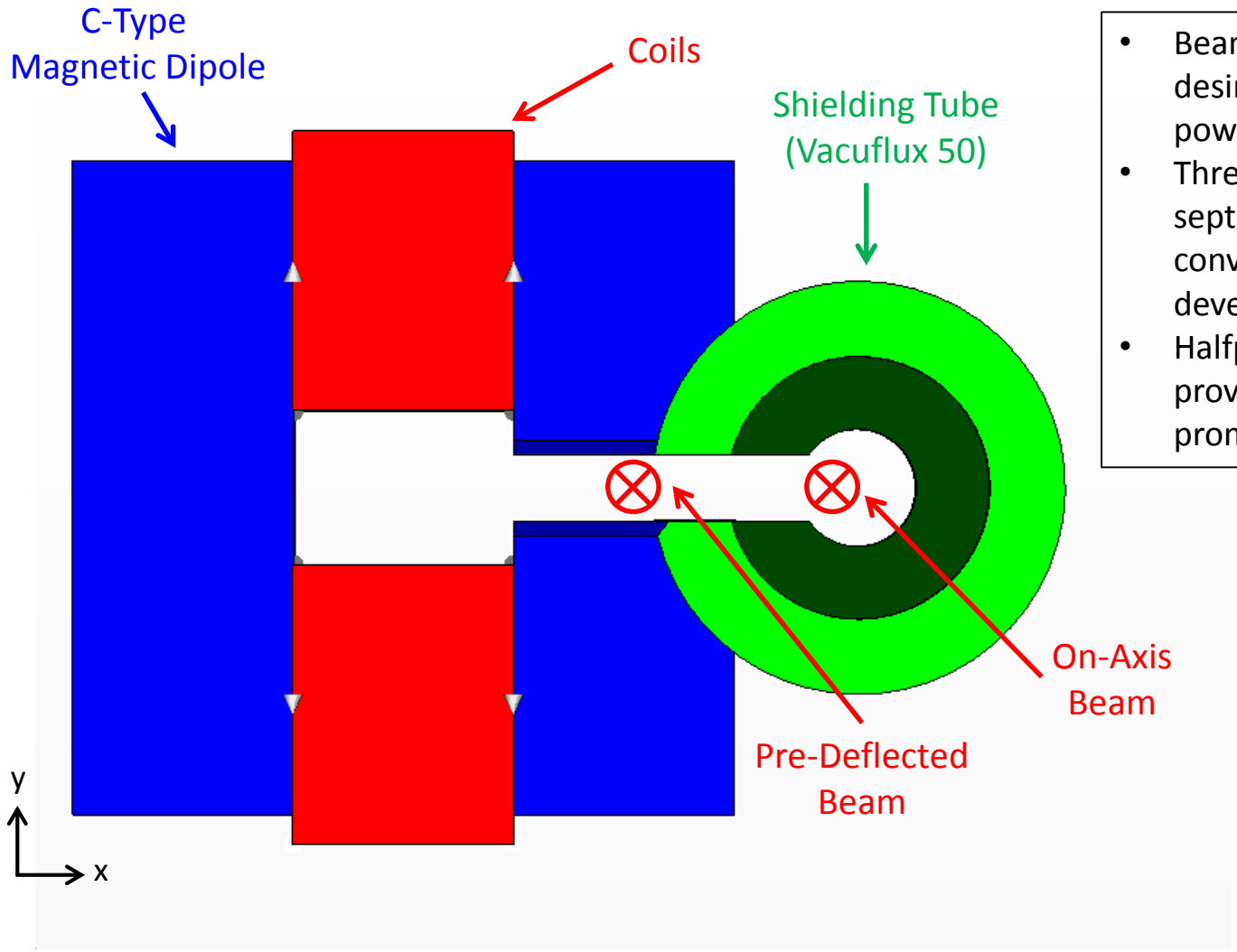
Beam Separation System

Beam Separation: Concept



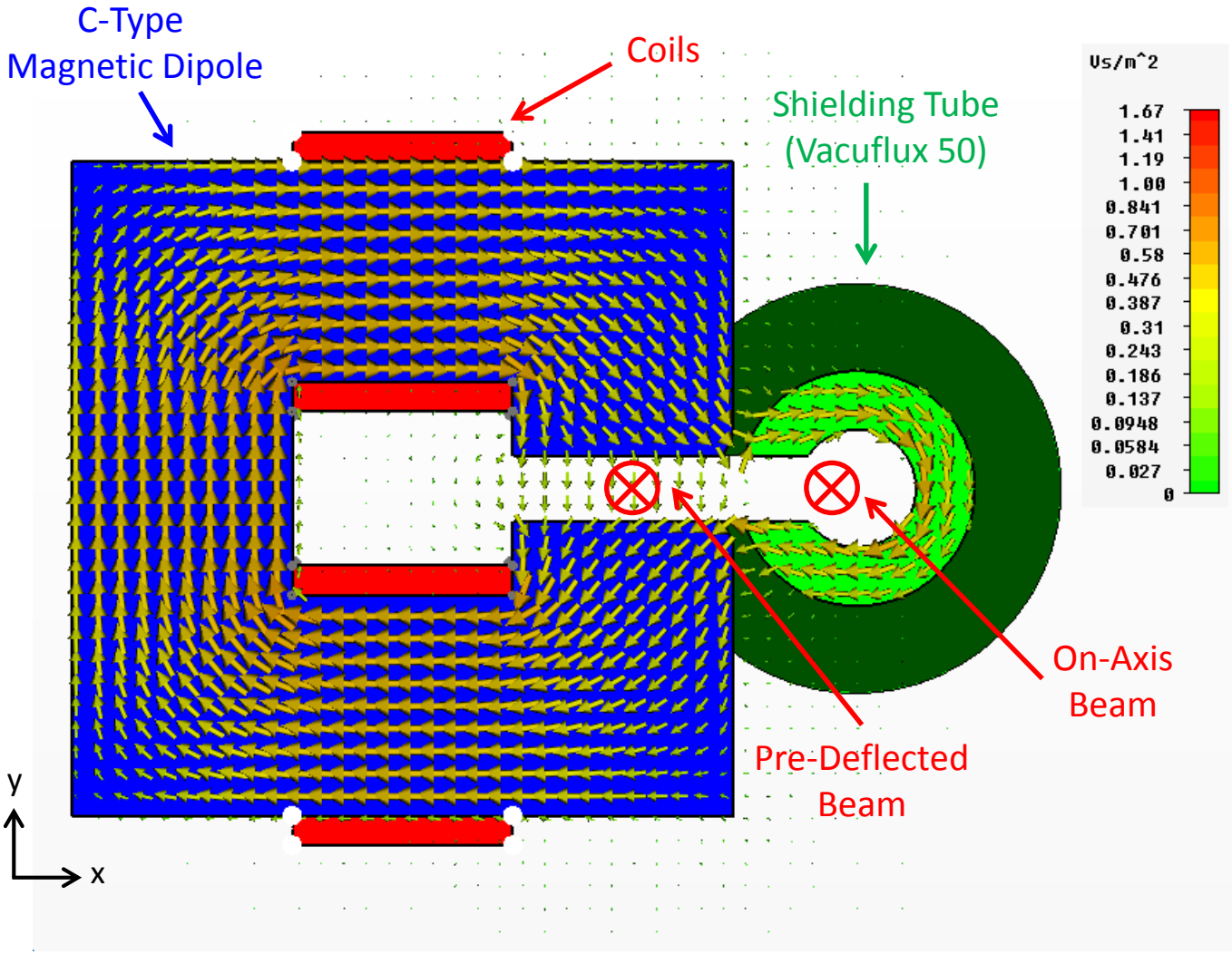
- Beam separation desirable for high beam power.
- Three different „massless“ septa systems and one conventional system were developed and optimized.

Beam Separation: Halfpipe Septum

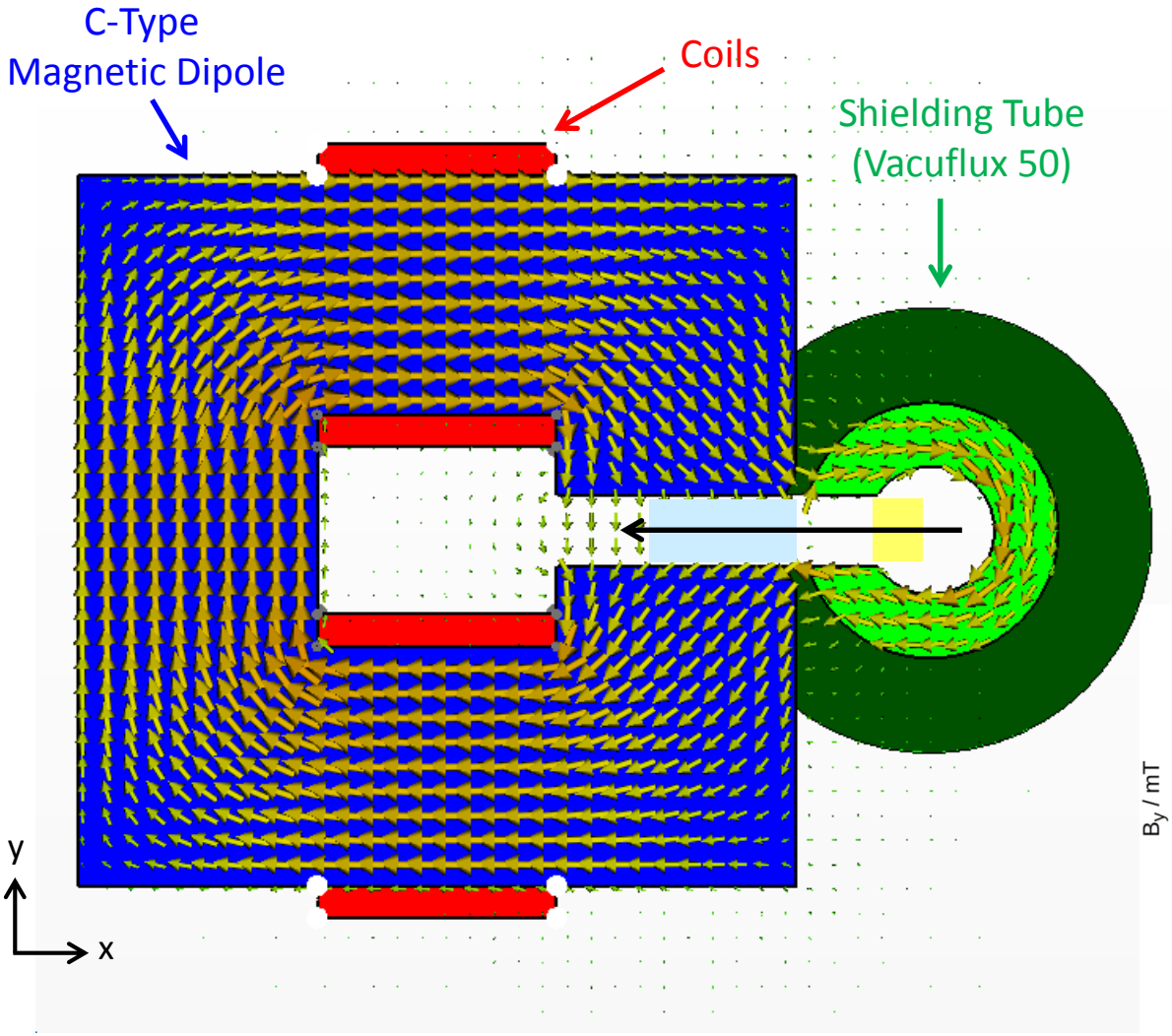


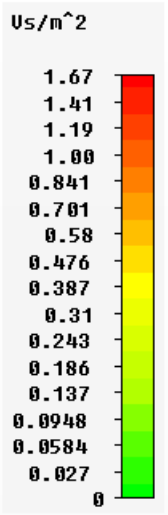
- Beam separation desirable for high beam power.
- Three different „massless“ septa systems and one conventional system were developed and optimized.
- Halfpipe Massless Septum proved to be the most promising.

Beam Separation: Halfpipe Septum

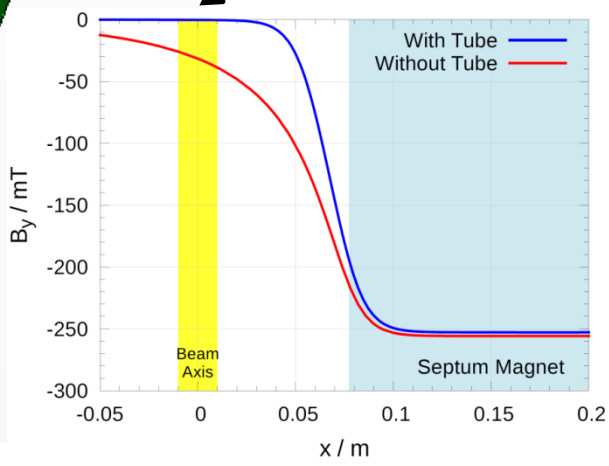


Beam Separation: Halfpipe Septum





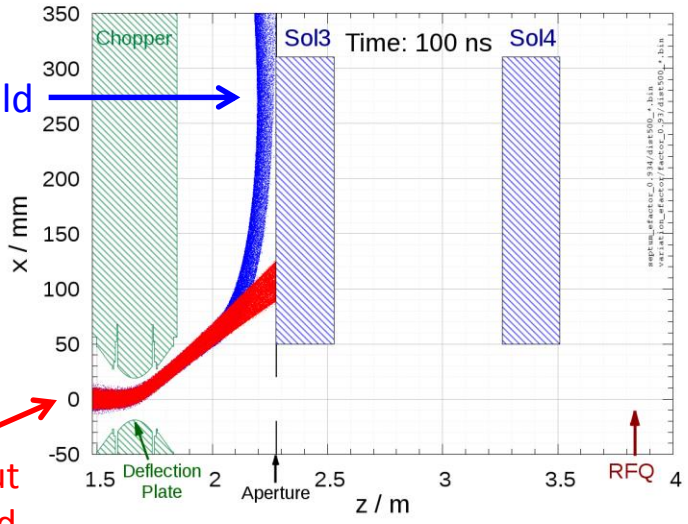
B field on axis reduced from B_y = -31.6 mT to B_y = -0.3 mT.

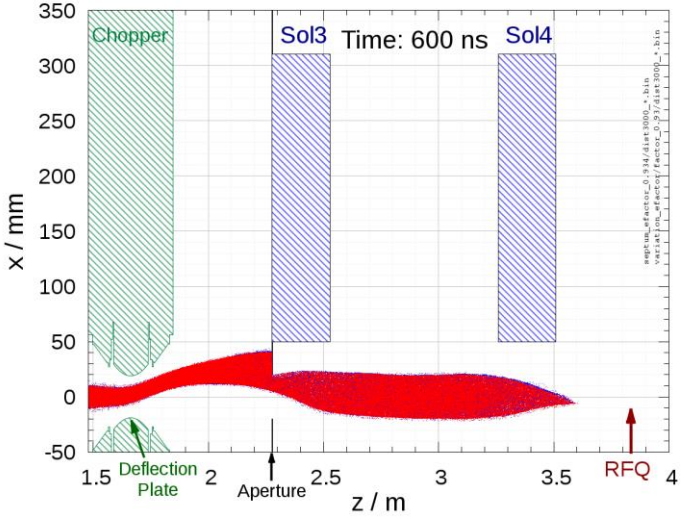


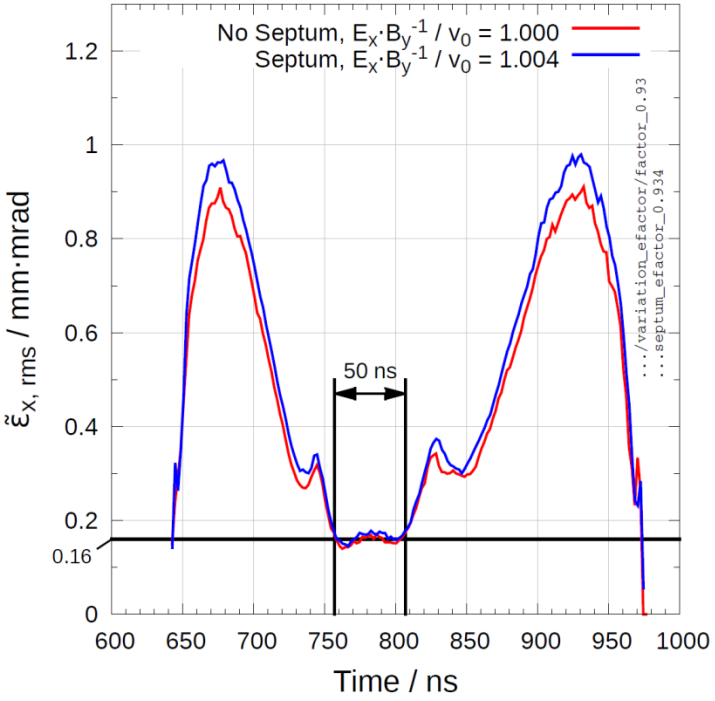
Beam Separation: Beam Simulation

Sim. with septum field

Sim. without septum field







Emittance of 50 ns Flat Top

No Septum:

$\varepsilon_{rms,\,norm} = 0.156$ mm·mrad

With Septum:

$\varepsilon_{rms,\,norm} = 0.162$ mm·mrad