

# ELECTRICAL MODELING OF MAIN INJECTOR SEXTUPOLE MAGNETS

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## 1. Introduction

The electrical models for the main injector sextupole magnet is obtained based on three terminal device impedance matrix measurement. The measurement data are analyzed and curve fitted into their equivalent circuits by using circuit simulation program Spice.

## 2. Electrical Measurement

The sextupole magnet is a three-terminal device. Fig 1 depicts the sextupole magnet three-terminal representation. Terminal 1 and 2 are the coil bus terminals and terminal 3 is the magnet case ground. The electrical characteristics of the magnet at non saturation can be described by its admittance matrix. The equations for this three-terminal device network can be written as

$$\begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix} = \begin{bmatrix} Y_{11} & Y_{12} & Y_{13} \\ Y_{21} & Y_{22} & Y_{23} \\ Y_{31} & Y_{32} & Y_{33} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix} \quad (1)$$

The 3x3 matrix on the right hand side of Eqn. (1) is called shorted circuit admittance matrix of the considered three-terminal sextupole magnet. The elements in the shorted circuit admittance matrix are frequency dependent variables. The way to measure this 3x3 matrix elements is depicts in figure 2. The excitation source used here is a high power frequency generator (Elgar Model 500) that can output current up to 5 amps. the output voltage can be adjusted from 0 to 150 Vrms, and the frequency can be varied from 10 Hz to 10KHz. A Tektronix current probe, which has the bandwidth of DC to 50 MHz, was used for current measurement. Both voltage and current as well as phase shifted between

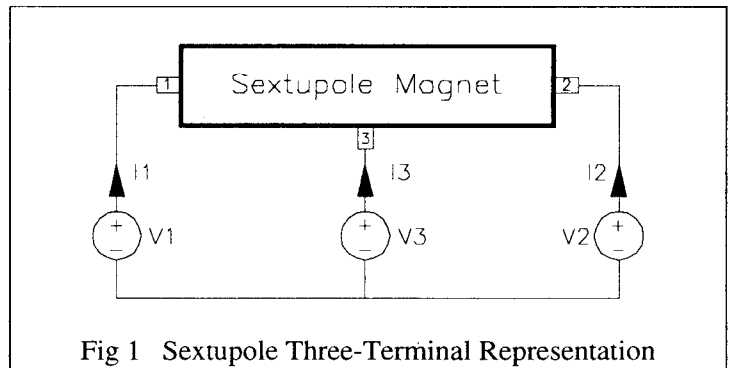


Fig 1 Sextupole Three-Terminal Representation

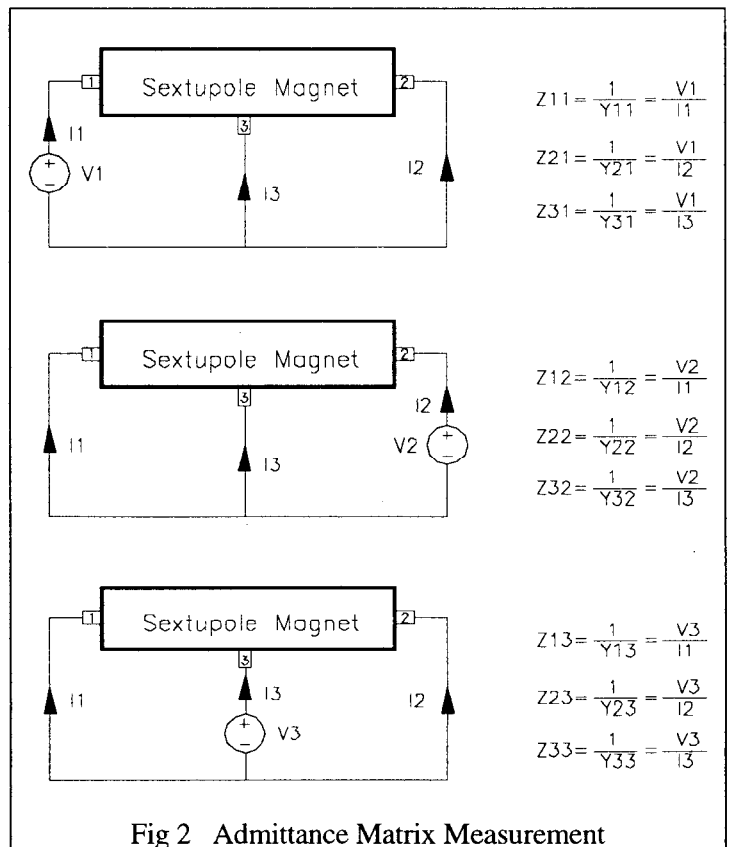


Fig 2 Admittance Matrix Measurement

$$\begin{aligned} Z_{11} &= \frac{1}{Y_{11}} = \frac{V_1}{I_1} \\ Z_{21} &= \frac{1}{Y_{21}} = \frac{V_1}{I_2} \\ Z_{31} &= \frac{1}{Y_{31}} = \frac{V_1}{I_3} \\ Z_{12} &= \frac{1}{Y_{12}} = \frac{V_2}{I_1} \\ Z_{22} &= \frac{1}{Y_{22}} = \frac{V_2}{I_2} \\ Z_{32} &= \frac{1}{Y_{32}} = \frac{V_2}{I_3} \\ Z_{13} &= \frac{1}{Y_{13}} = \frac{V_3}{I_1} \\ Z_{23} &= \frac{1}{Y_{23}} = \frac{V_3}{I_2} \\ Z_{33} &= \frac{1}{Y_{33}} = \frac{V_3}{I_3} \end{aligned}$$

voltage and current were measured by Tektronix scope. Ratio of peak to peak value of current to voltage was obtained for the shorted circuit admittance at the frequency of interest. Scope measurement for voltage and current made sure the signals being measured were not distorted.

### 3. Measurement Data Fitting

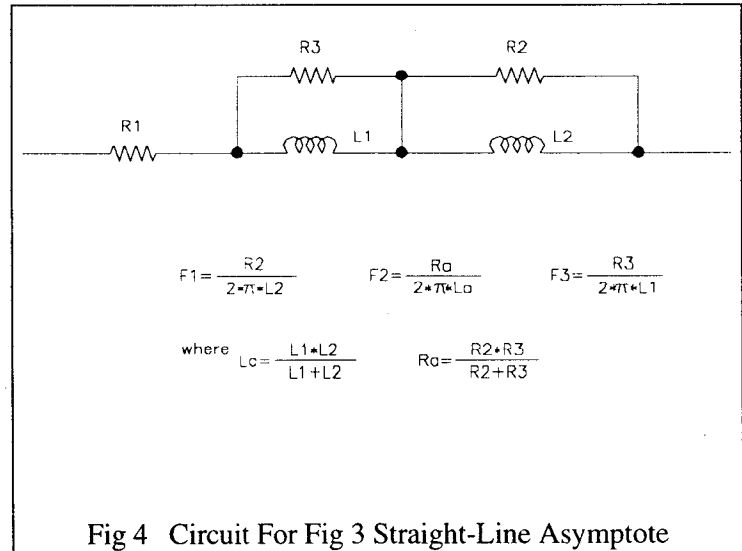
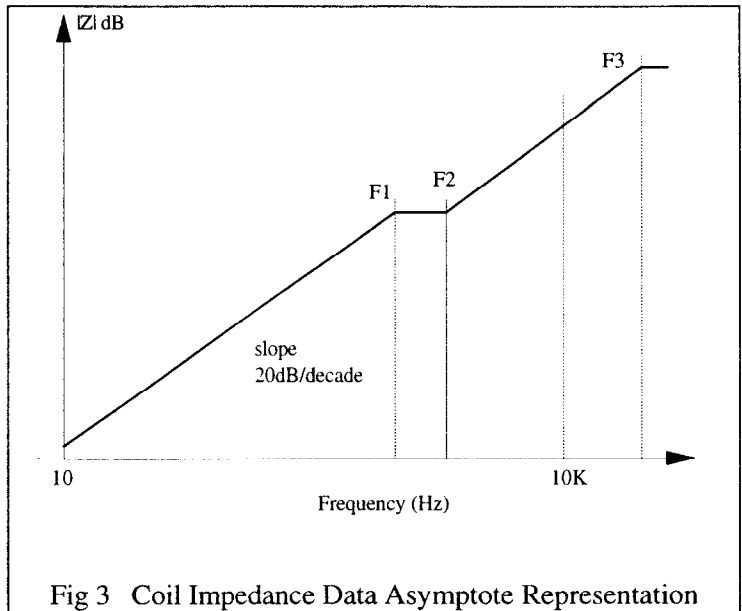
**DC Resistance** of the coil bus is measured at 18 °C. The resistance is then scaled to the resistance at 40 °C by using the formula:

$$R(40^{\circ} C) = R(18^{\circ} C) \cdot [1 + 0.004 / ^{\circ} C \cdot (40^{\circ} C - 18^{\circ} C)] \quad (2)$$

**Coil Impedance** measurement is performed by  $Z_{11}$ ,  $Z_{22}$ ,  $Z_{12}$ ,  $Z_{21}$ .  $Z_{11}$  and  $Z_{22}$  are equal both in magnitude and phase for the frequency up to 10 KHz.  $Z_{12}$  and  $Z_{21}$  are also the same both in magnitude and phase.  $Z_{11}$  and  $Z_{12}$  are the same in magnitude but 180° out of phase because the reverse direction of the current. This implies the Sextupole is symmetrical since impedance looking into both coil bus terminals is equal.

By analyzing the coil impedance measurement data  $Z_{11}$  and  $Z_{22}$ . The data can be represented by straight-line asymptotes as shown in Fig 3. The bus DC resistance has effect on coil impedance at very low frequency ( $\ll 10$  Hz), therefore it is not shown in the impedance asymptote representation here. The coil bus impedance is inductive at the frequency between 10 Hz and  $F_1$ ,  $F_2$  and  $F_3$  because the slope of the magnitude asymptote line is 20 dB/decade and the phase is 90°. The coil bus becomes small resistive at the frequency between  $F_1$  and  $F_2$ , and above  $F_3$ . In the other word, the inductance of the coil decreases as the frequency increases.

An electrical circuit shown in Fig 4 can be used to represent the straight-line asymptote characteristics in Fig 3. The corner frequency break points are approximately given by the formula in figure 4.



**Bus Capacitance** Measurement is obtained by  $Z_{13}$ ,  $Z_{31}$ ,  $Z_{23}$ ,  $Z_{32}$ , and  $Z_{33}$ .  $Z_{33}$  measures the total bus to ground capacitance.  $Z_{13}$  and  $Z_{31}$  measures the capacitance between terminal 1 and ground while terminal 2 is shorted to ground. Similarly,  $Z_{23}$  and  $Z_{32}$  measures the capacitance between terminal 2

and ground while terminal 1 is grounded. The  $Z_{13}$ ,  $Z_{31}$ ,  $Z_{23}$ ,  $Z_{32}$ , and  $Z_{33}$  are capacitance measurement because the slope of the measurement data is -20dB/decade in the magnitude plot. The capacitance is determined by the following formula

$$C = \frac{1}{2 \cdot \pi \cdot f \cdot |Z|} \quad (3)$$

where  $f$  is the excitation frequency in Hz and  $Z$  is the impedance in ohms.

#### 4. Sextupole Electrical Model

The impedance matrix measurement data for the sextupole are given in Appendix A. The DC resistance is measured at 18 °C and the value is 15.62 mΩ. The resistance at 40 °C is calculated to be 17 mΩ by using Eqn (2).  $R_1$  in Fig 4 is the DC resistance.

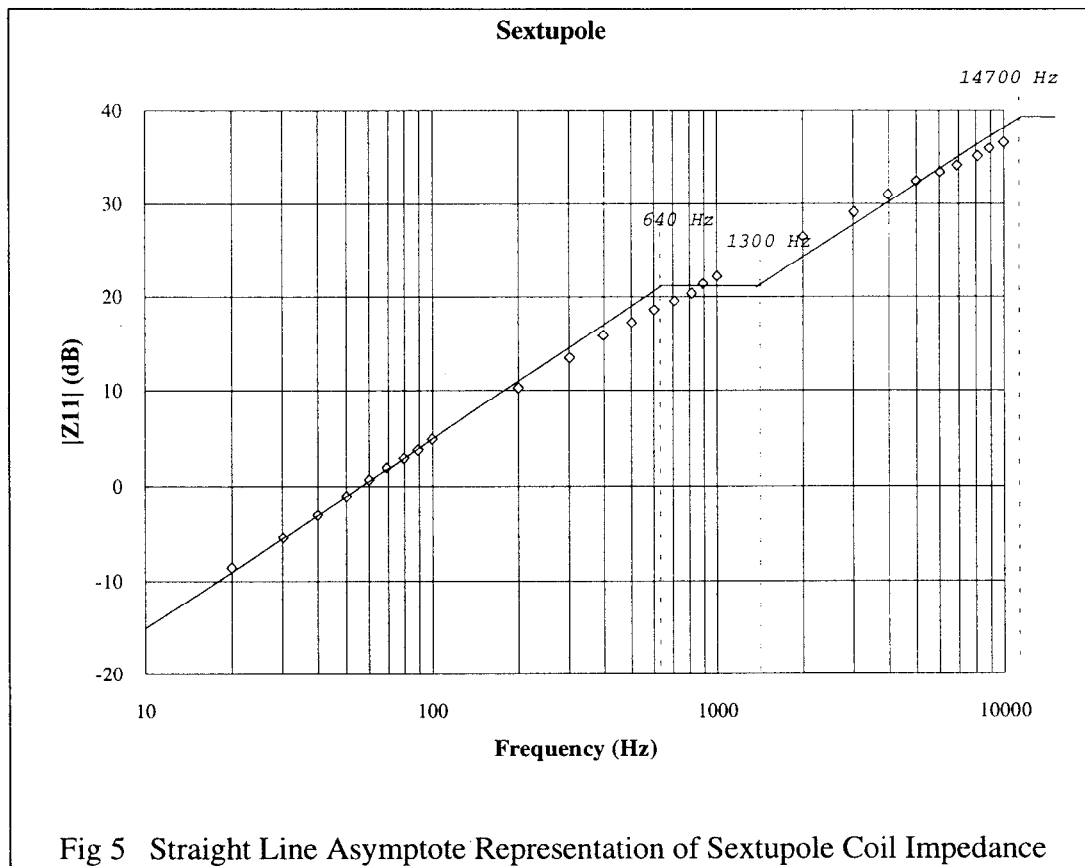


Fig 5 Straight Line Asymptote Representation of Sextupole Coil Impedance

**Coil Impedance** measurement is obtained by  $Z_{11}$ ,  $Z_{22}$ ,  $Z_{12}$ ,  $Z_{21}$ . They all have the same magnitude as function of frequency. Figure 5 shows  $Z_{11}$  measurement data where the data can be represented by straight line asymptotes. The parameters in the circuit (Fig 4) can be determined according to the data. Referring to Fig 5, the corner frequency break points, the total coil inductance at low frequency (10 Hz), the inductance at high frequency (10KHz) are obtained as:

$$F1=640 \text{ Hz} \quad F2=1300 \text{ Hz} \quad F3=14700 \text{ Hz}$$

$$\text{Total Inductance @ 10 Hz: } L_T = \frac{1}{2\pi f} \log^{-1} \left[ \frac{|Z_{11}|}{20} \right] = 2.8 \text{ mH} \quad \text{where } |Z_{11}| = -15.1 \text{ dB}$$

Inductance @ 5 KHz:  $L_1 = \frac{1}{2\pi f} \log^{-1}\left[\frac{|Z_{11}|}{20}\right] = 1.3 \text{ mH}$       where  $|Z_{11}| = 32.2 \text{ dB}$

The value of the circuit elements can be calculated since the total coil inductance, inductance at the frequency of  $F_2 < f < F_3$ , and the corner frequency break points are known.

L2 Inductance:  $L_2 = L_T - L_1 = 1.5 \text{ mH}$

R2:  $R_2 = 2 \cdot \pi \cdot F_1 \cdot L_2 = 6 \text{ } \Omega$

R3:  $R_4 = 2 \cdot \pi \cdot F_3 \cdot L_1 = 120 \text{ } \Omega$

**Bus Capacitance** is measured by  $Z_{15}$ ,  $Z_{51}$ ,  $Z_{25}$ ,  $Z_{52}$ , and  $Z_{55}$ . The total bus to magnet case ground capacitance ( $C_T$ ) is measured by  $Z_{55}$ .  $Z_{15}$  and  $Z_{51}$  measures the capacitance ( $C_1$ ) between terminal 1 and ground while terminal 2 is shorted to ground. Similarly,  $Z_{25}$  and  $Z_{52}$  measures the capacitance ( $C_2$ ) between terminal 2 and ground while terminal 1 is grounded.

Total Bus to Ground Capacitance:  $C_T = \frac{1}{2 \cdot \pi \cdot f \cdot |Z_{55}|} = 3.8 \text{ nF}$

Terminal 1 to Ground Capacitance:  $C_1 = \frac{1}{2 \cdot \pi \cdot f \cdot |Z_{15}|} = 1.9 \text{ nF}$       or

$C_1 = \frac{1}{2 \cdot \pi \cdot f \cdot |Z_{51}|} = 1.9 \text{ nF}$

Terminal 2 to Ground Capacitance:  $C_2 = \frac{1}{2 \cdot \pi \cdot f \cdot |Z_{25}|} = 1.9 \text{ nF}$       or

$C_2 = \frac{1}{2 \cdot \pi \cdot f \cdot |Z_{52}|} = 1.9 \text{ nF}$

The sextupole magnet electrical model is shown in Fig 6. The simulation results are given in Appendix A. The model matches the measurement data up to 10 KHz.

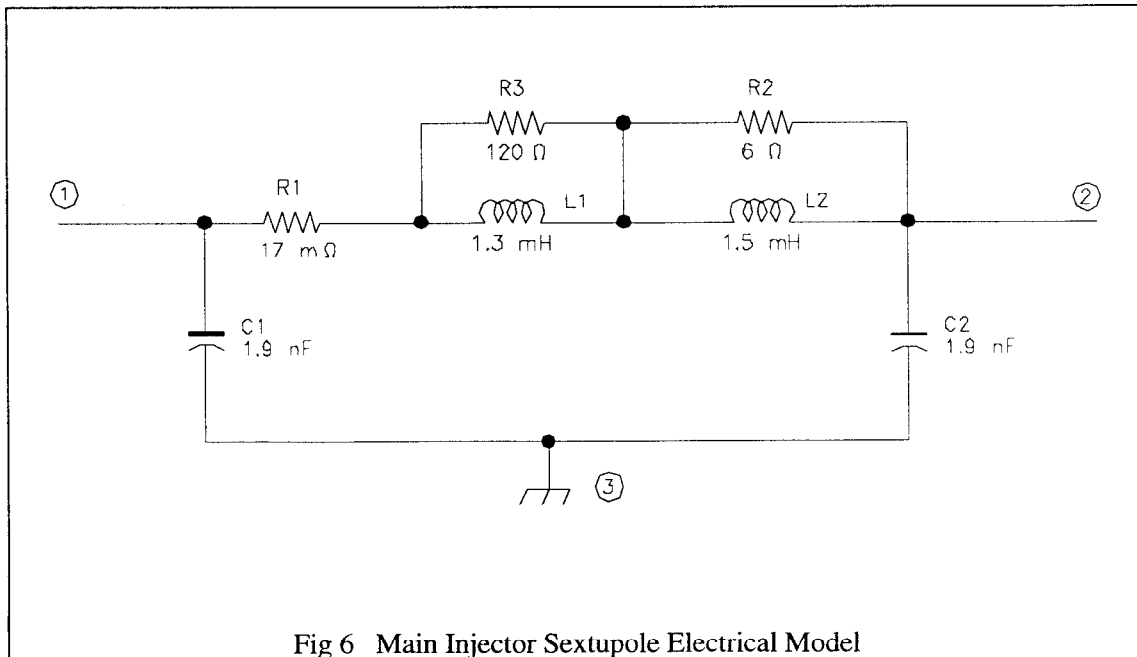


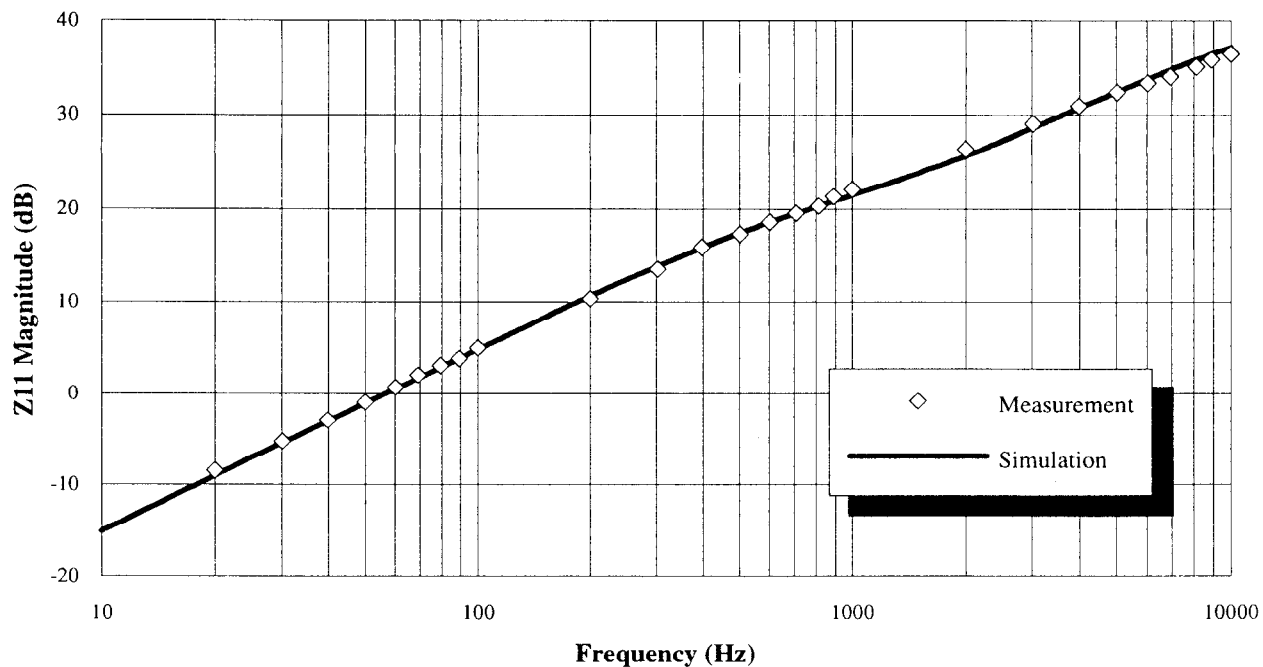
Fig 6 Main Injector Sextupole Electrical Model

## **5. Conclusion**

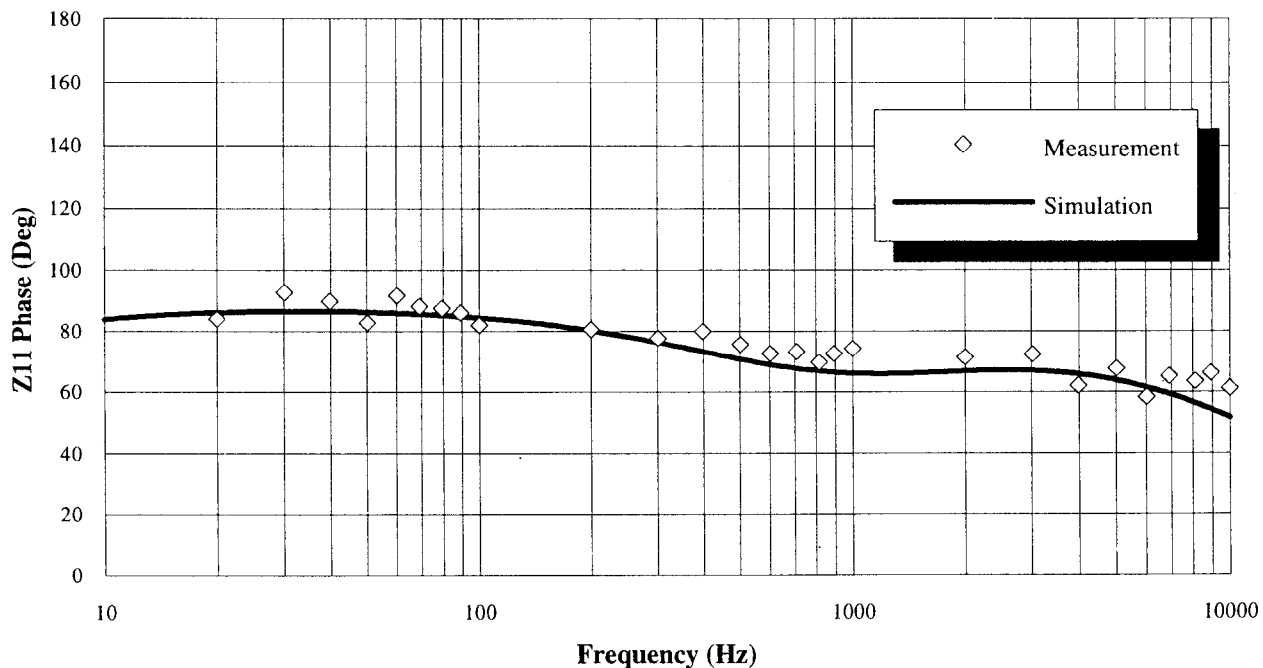
The sextupole electrical model is obtained based on the impedance matrix measurement. Spice simulation result shows the accuracy of the models. The electrical model can be used as a sub circuit to build a sextupole ring model to study the transient and frequency response of the system.

Phase: 0.000000, Amplitude: 0.000000

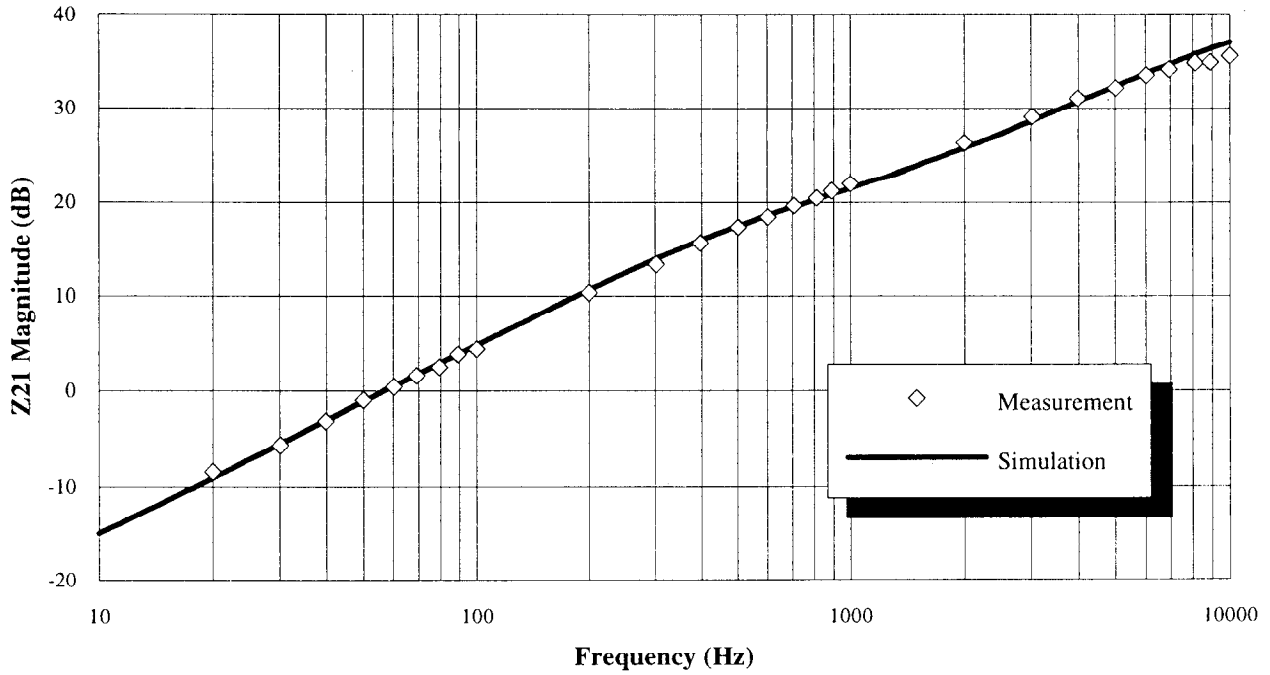
Z11 MAGNITUDE PLOT



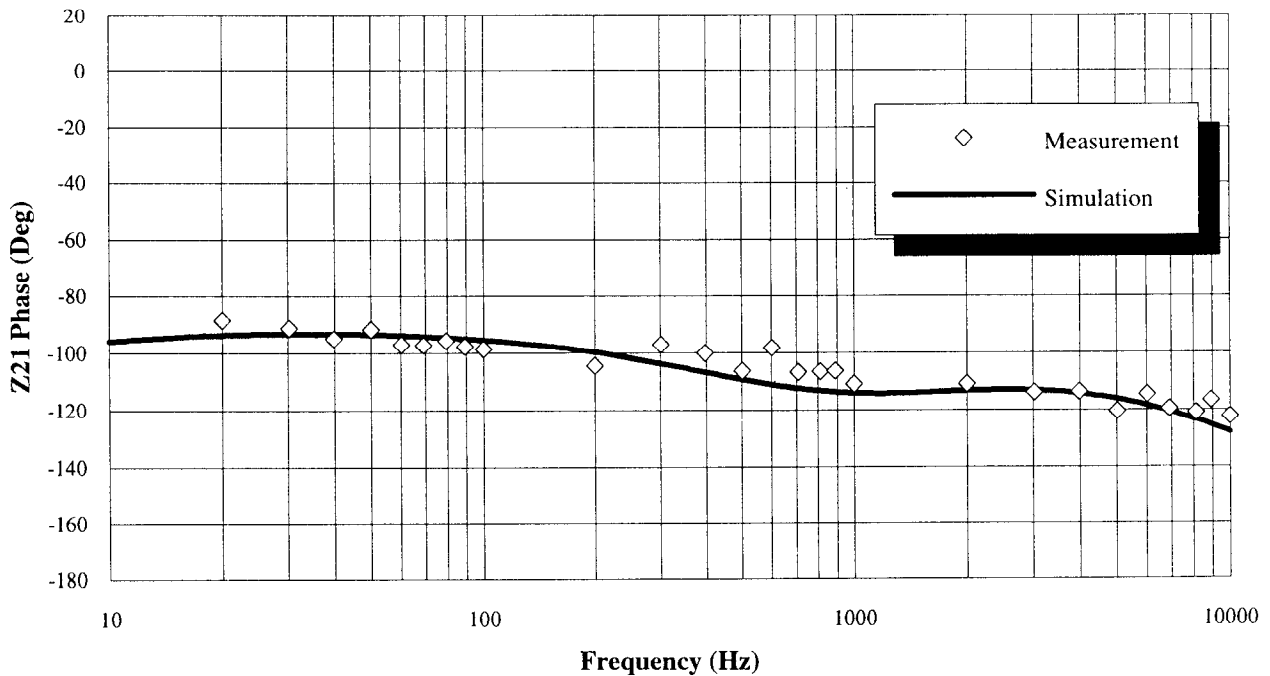
Z11 PHASE PLOT



Z21 MAGNITUDE PLOT

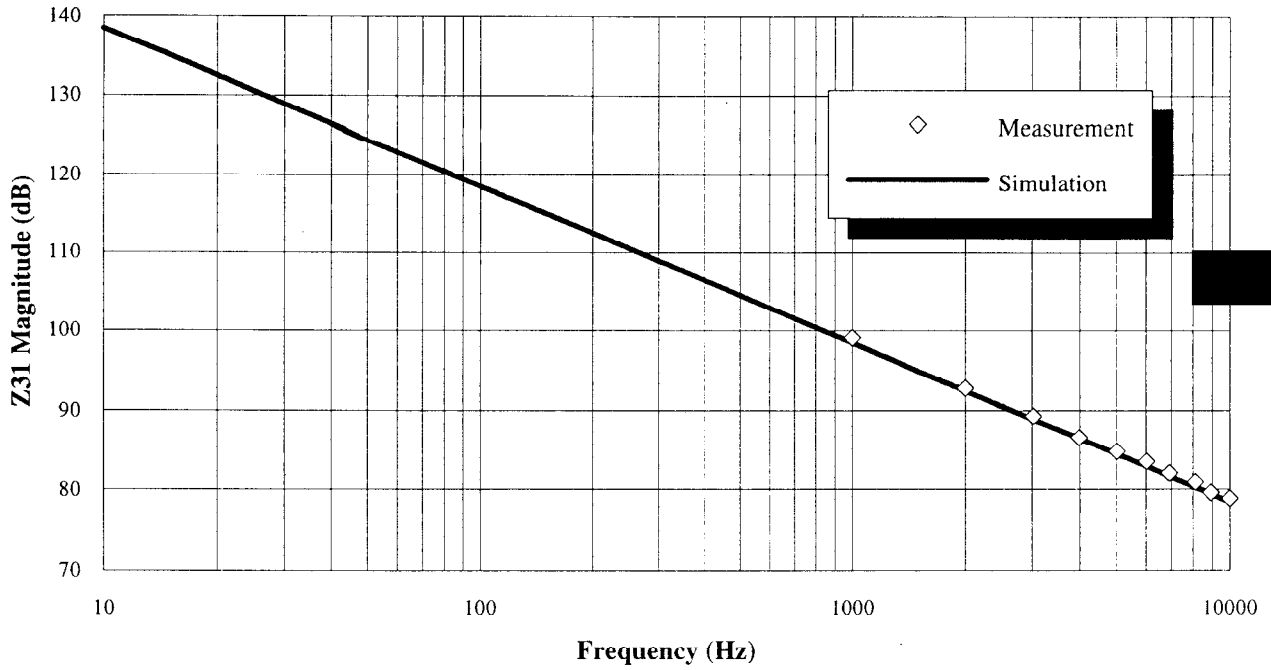


Z21 PHASE PLOT

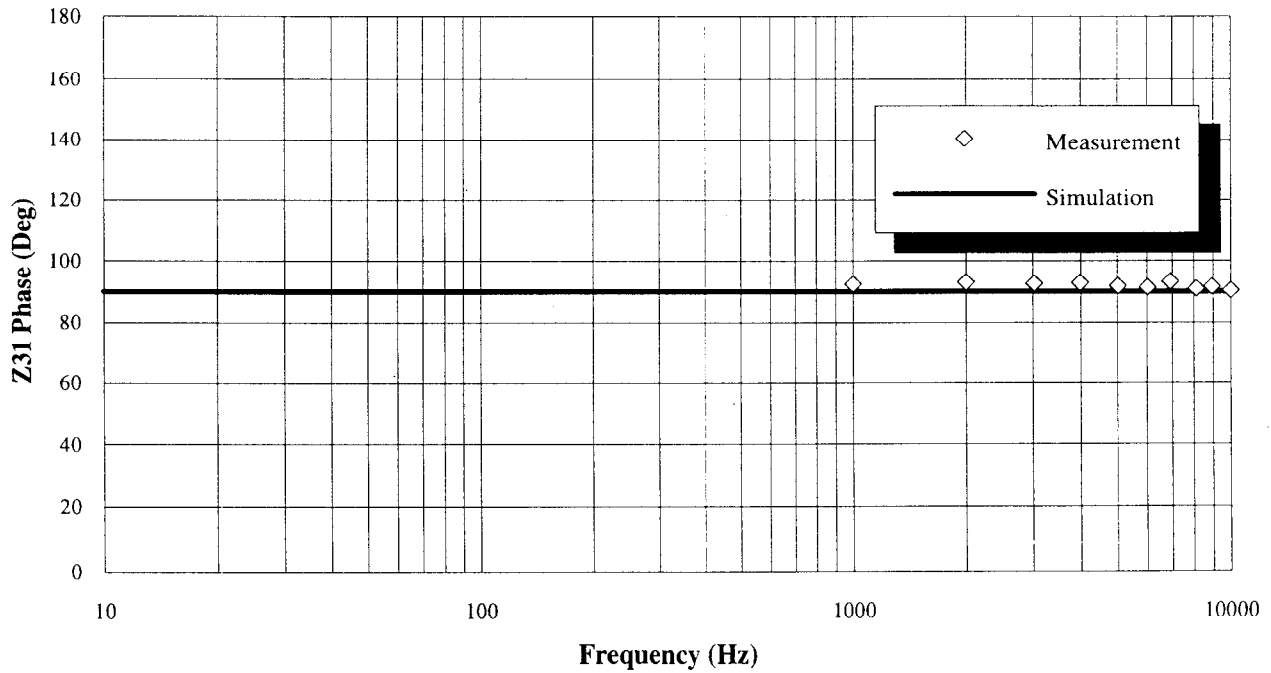


Main Injector Sextupole Magn

Z31 MAGNITUDE PLOT



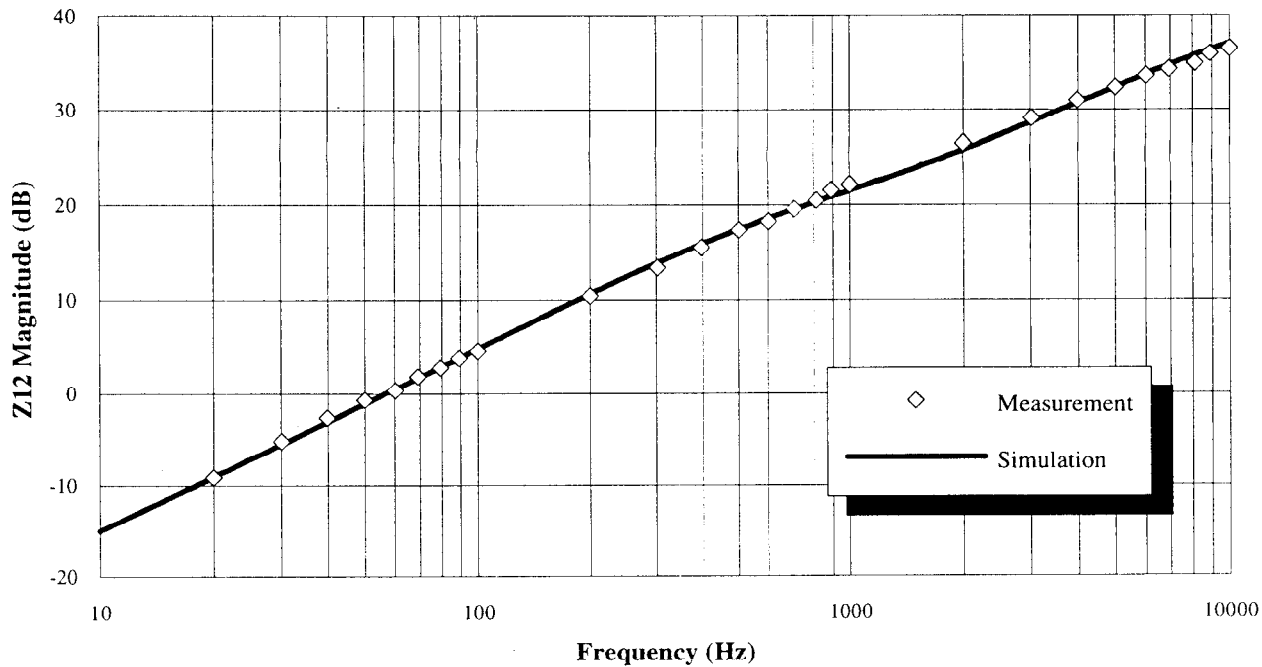
Z31 PHASE PLOT



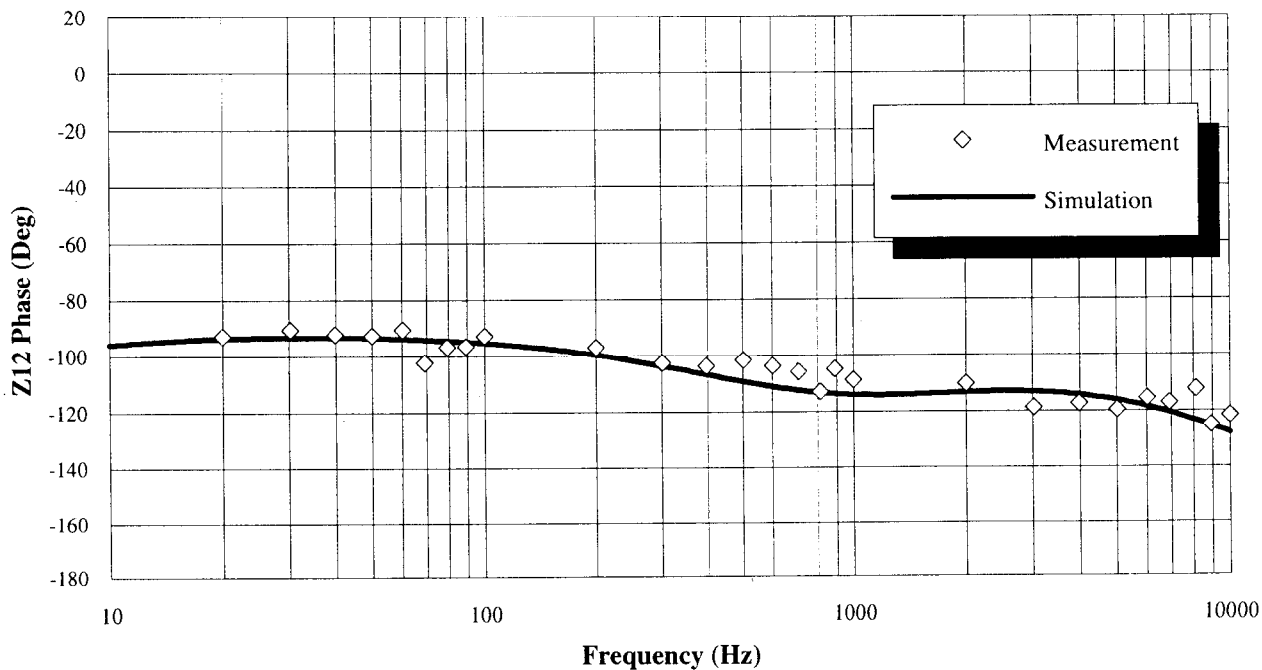


Main Injector Sextupole Magnets

Z12 MAGNITUDE PLOT

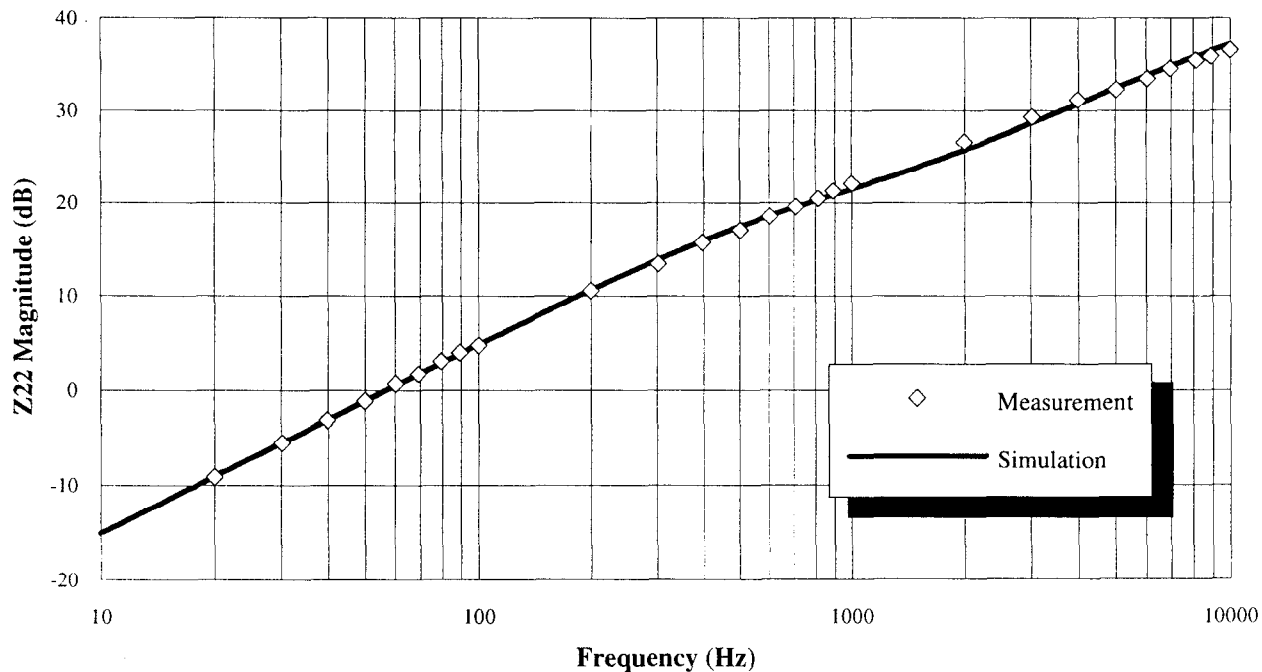


Z12 PHASE PLOT

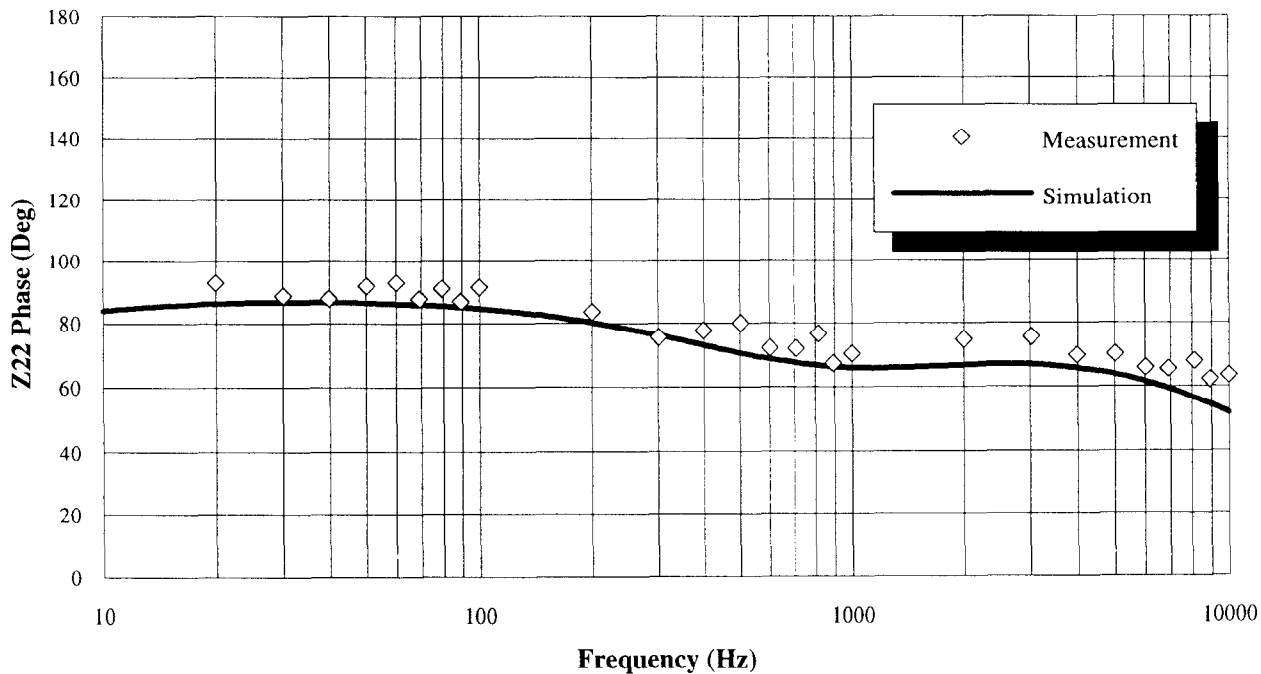


EXPERIMENTAL DATA

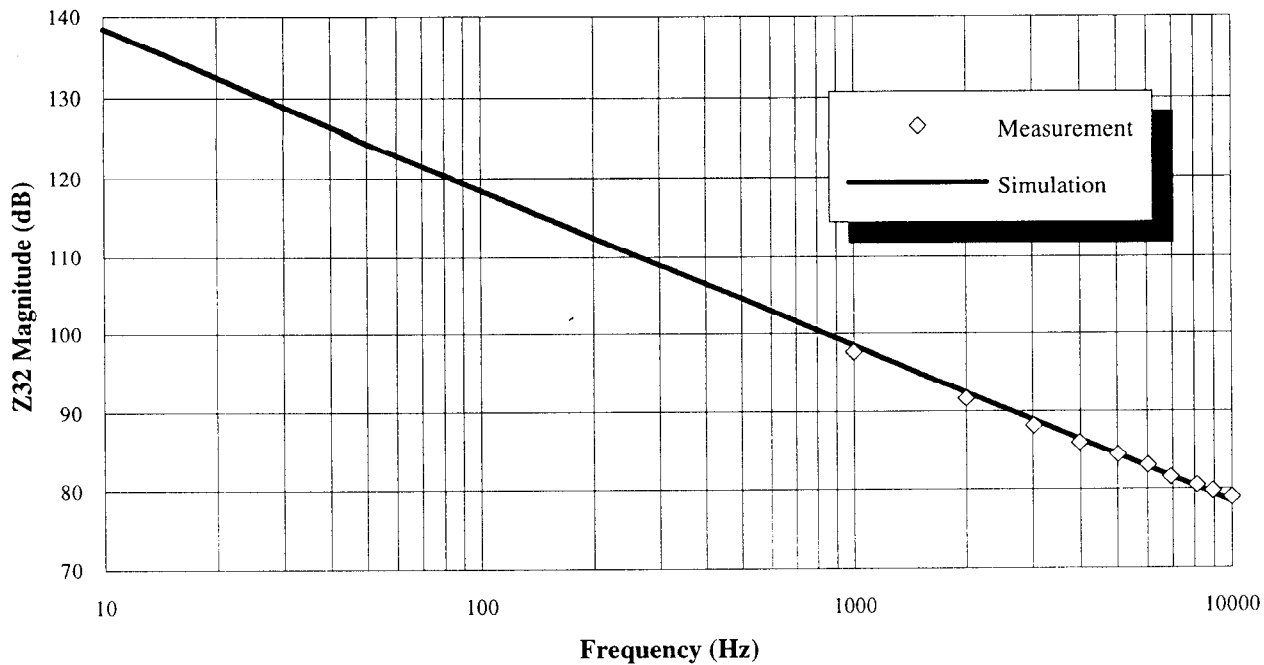
### Z22 MAGNITUDE PLOT



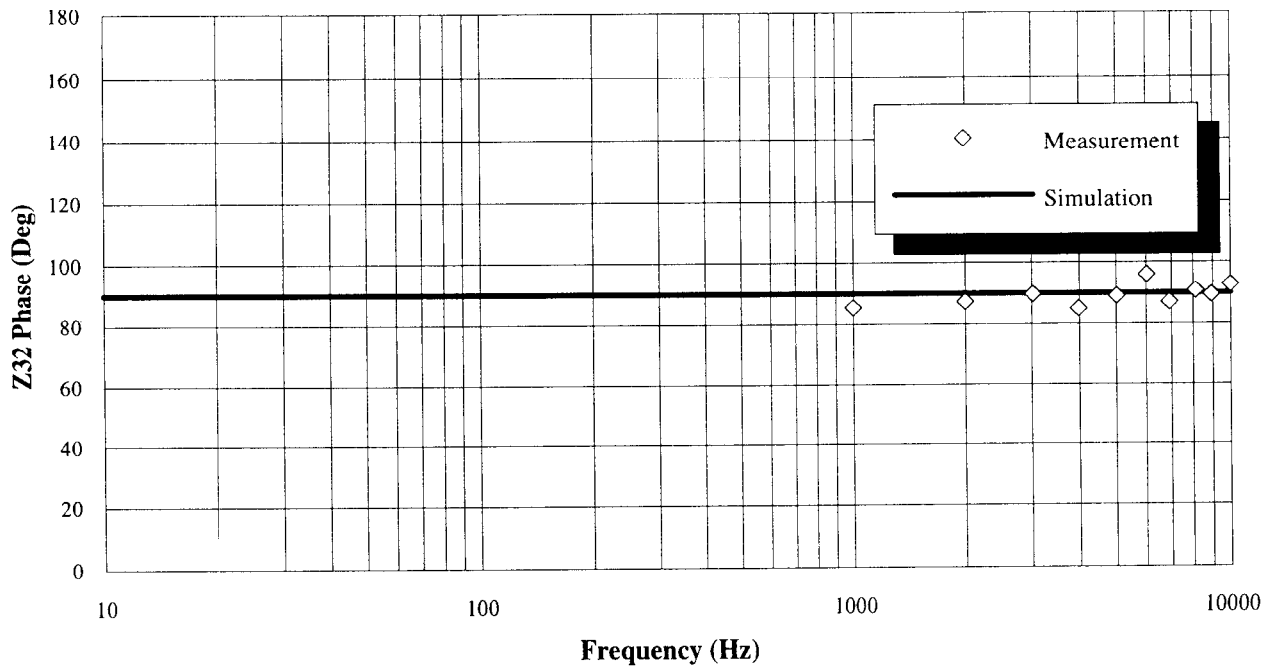
### Z22 PHASE PLOT



Z32 MAGNITUDE PLOT.

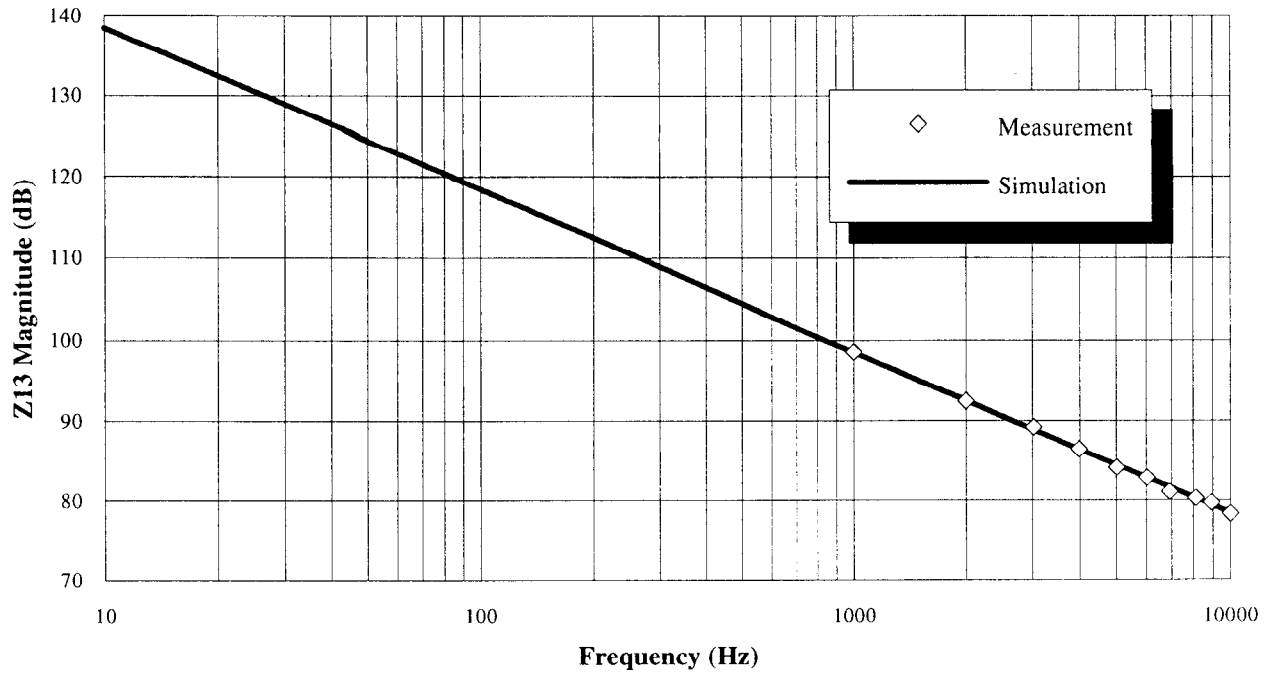


Z32 PHASE PLOT

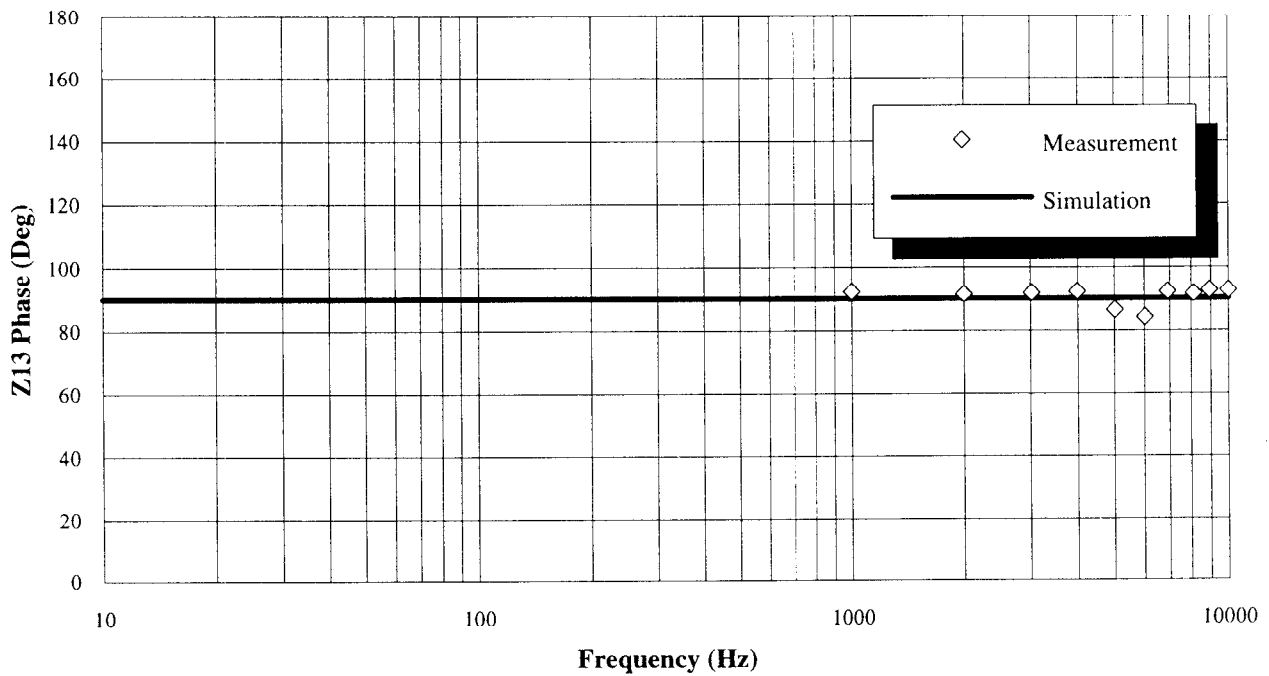


MIP Sextupole Simulation Magnitude

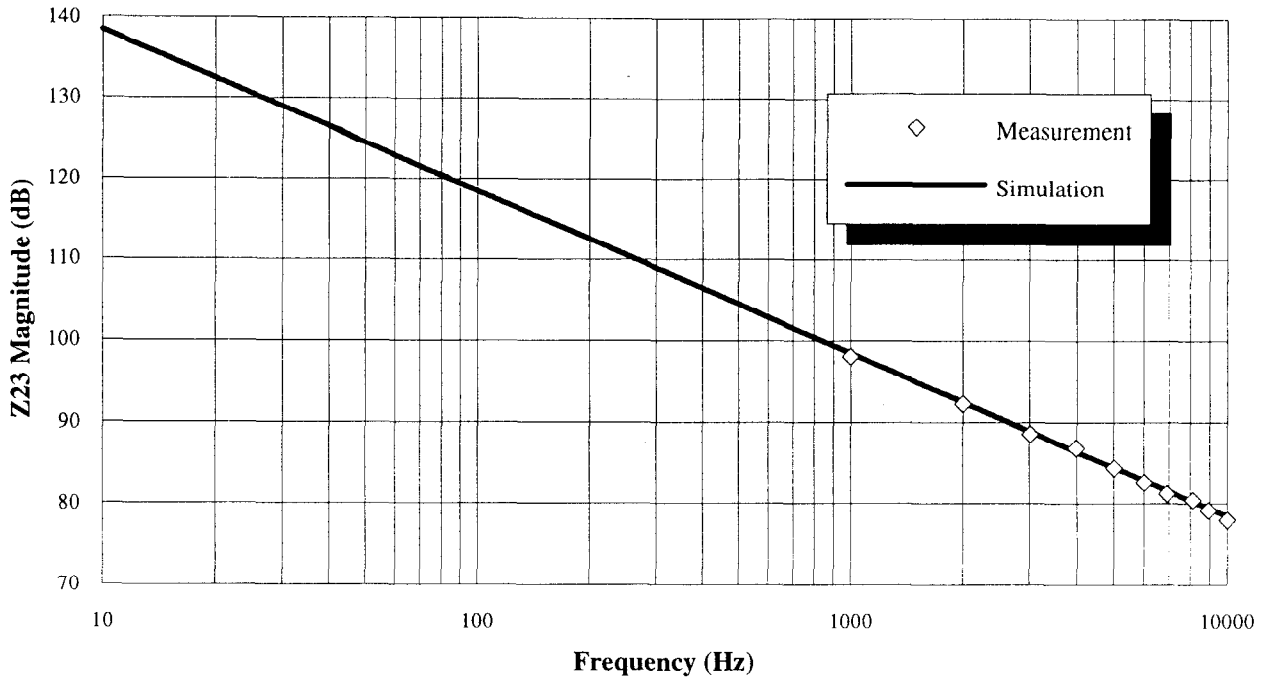
Z13 MAGNITUDE PLOT



Z13 PHASE PLOT



Z23 MAGNITUDE PLOT



Z23 PHASE PLOT

