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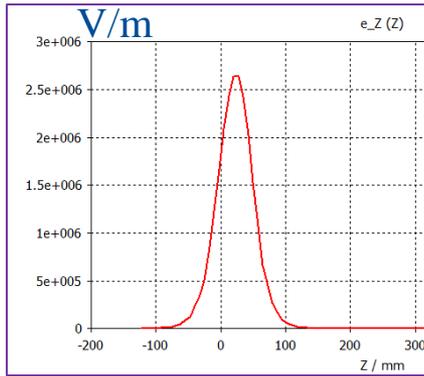
# **Cavity parameters used in CST, preliminary results with blocking capacitor and more thermal analyses**

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2<sup>nd</sup> Harmonic cavity Meeting

1/VII-2015

# Definitions in CST



$$P_{rms} = V_{rms}^2/R \Rightarrow R_s = V_{rms}^2/P_{rms} = V_{peak}^2/2P_{rms} = V_{eff}^2/2P_{thermal} = R_{gennady}/2$$

## What are $V_{eff}$ , $P$ , $R_{sh}$ in CST?

**Voltage  $V_{eff}$ :** CST integrates the electric field along the given voltage integration path (cavity axes typically). By definition  $V_{eff}$  takes into account time flight factor, but currently  $\beta = 1$  is assumed ( $\beta$  - particle relative velocity).

## Thermal losses P:

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Result: Thermal Losses
Loss calculation settings:
Default conductivity for PEC surfaces: 5.800000e+007 S/m
Consider surface losses on boundaries: *** none ***

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Computed 2 thermal loss distributions.

1: Filename : loss (#0001)_1(1)
   Solver   : Frequency Domain: S-Parameter [1(1)]
   Frequency: 76.55 MHz
   Grid     : Tet
   Field Type: Dynamic Loss density
   Loss Type: Electric Volume Loss
   Total Loss: 3.870068e-001 W

2: Filename : surface loss int (#0001)_1(1)
   Solver   : Frequency Domain: S-Parameter [1(1)]
   Frequency: 76.55 MHz
   Grid     : Tet
   Field Type: Surface Loss Density
   Loss Type: Surface Loss
   Total Loss: 1.048295e-001 W
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FD solver -> Thermal solver

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Result: Heat Flow Values

Heat Flow [temperaturesource1]: -1.949943e-001 W
Heat Flow [temperaturesource2]: 2.881760e+000 W
Heat Flow [temperaturesource3]: 0.000000e+000 W
Heat Flow [thermalloss0: El. Volume Loss Distribution]: 3.870204e-001 W (rms) (imported:
Heat Flow [thermalloss0: Surface Loss Distribution]: 1.025462e-001 W (rms) (imported:

Total Heat Flow: 3.176333e+000 W (rms) = 6.352665e+000 W (peak)

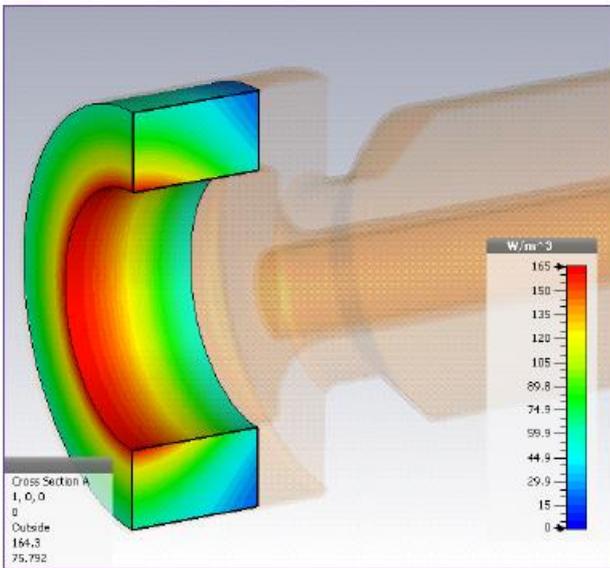
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External power scaling factors:
- thermalloss0: 1.000000e+000
External power sum considered: 4.895666e-001 W (rms) = 9.791332e-001 W (peak)

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External power scaling factors:
- thermalloss2: 6.504000e+003
External power sum considered: 3.184784e+003 W (rms) = 6.369569e+003 W (peak)
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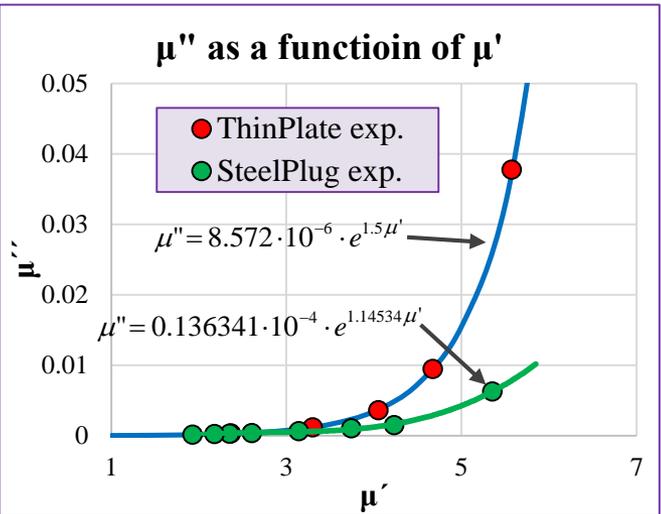
**Shunt impedance:**  $R_{sh} = V_{eff}^2/P$

# FD, EM and trans. model with garnet with averaged $\mu'$ & $\mu''$

Garnet with fixed parameters  $\mu' = 3.5$ ,  $\tan\delta_e = 0.0001$  and  $\tan\delta_m = 0.000467$ . Equivalent to transmission model



Tianhuan Luo, ThinPlate data  
 $F = 75.503 \text{ MHz}$   
 For  $V_{\text{peak}} = 100 \text{ KV}$ :  
 $P_{\text{ferrite}_e} = 8.11 \text{ kW}$   
 $P_{\text{ferrite}_m} = 63.25 \text{ kW}$   
 $P_{\text{ferrite}} = 71.36 \text{ kW}$   
 $P_{\text{copper}} = 9.14 \text{ kW}$   
 $P_{\text{total}} = 80.5 \text{ kW}$   
 The Omega3P EM simulation agrees well with Gennady's results.



For garnet with fixed parameters FD solver and EM solver (CST and Omega3P) deliver close results.

For  $f=76 \text{ MHz}$   $\mu' = 3.5 \Rightarrow$  SteelPlug  $\tan\delta = 0.000206$  (or  $\tan\delta = 0.0002145$  from Tan's approximation)

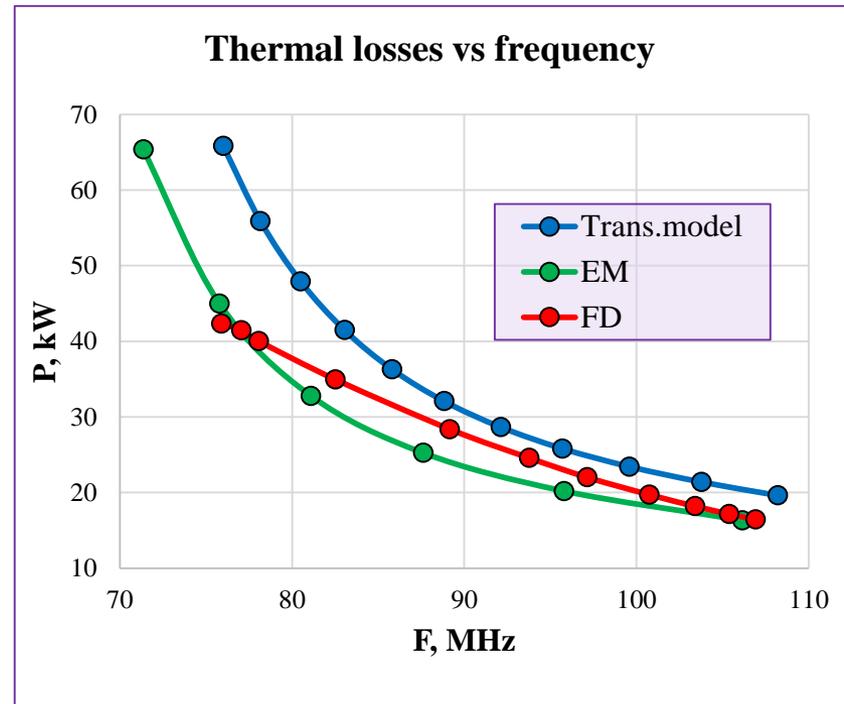
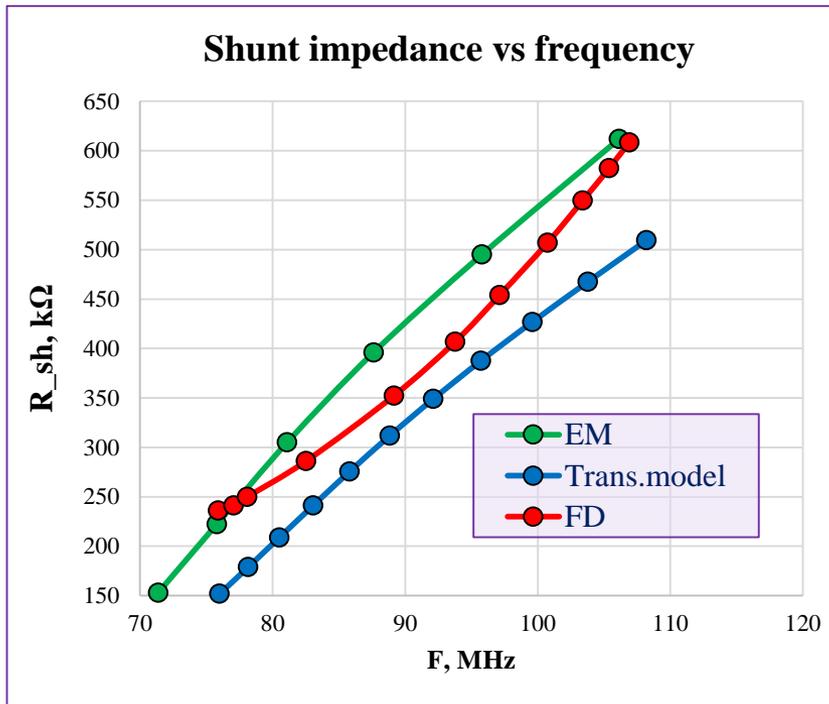
Recalculating Tianhuan Luo results with SteelPlug  $\tan\delta = 0.000206$   
 $P_{\text{total}} = 8.11 + 9.14 + 71.36 * 206 / 467 = 48.72 \text{ kW}$   
 $R_{\text{sh}} = 100^2 / 48.72 = 205 \text{ k}\Omega$

$\tan\delta_m$	4.67e-4	2.06e-4	
$R_{\text{sh}}$ , k $\Omega$	128	230	CST EM
P, kW	78	43.5	
$R_{\text{sh}}$ , k $\Omega$	124	205	Omega3P
P, kW	80.5	48.7	
$R_{\text{sh}}$ , k $\Omega$	78.5	152	Transmit. model
P, kW	127.4	65.8	

# Uniform garnet vs non-linear garnet

Uniform garnet – transition model and CST eigenmode solver

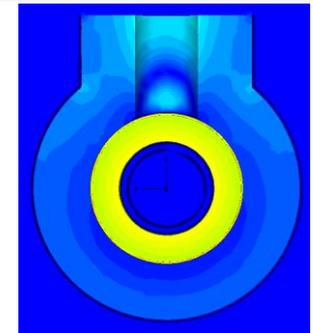
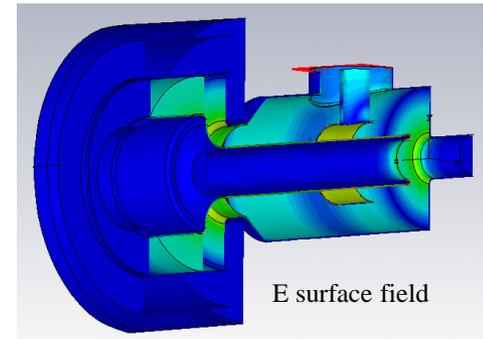
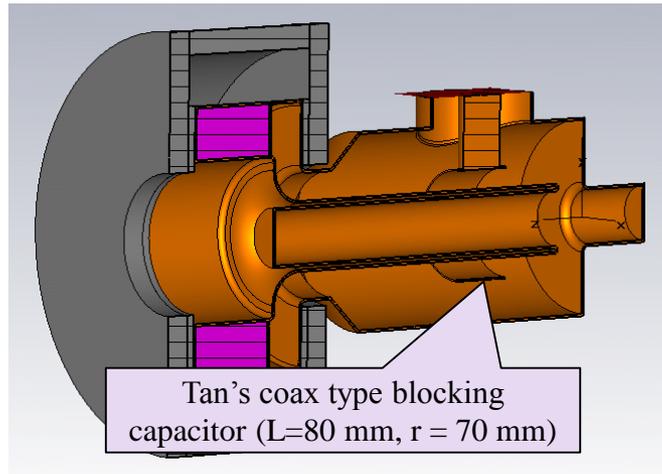
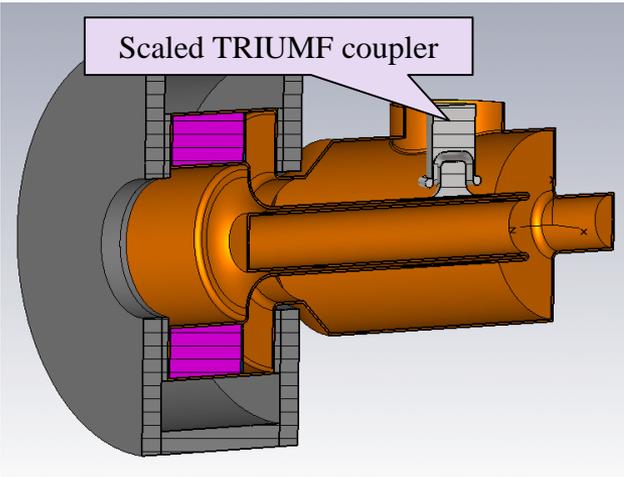
Non-linear garnet – CST frequency domain with external bias



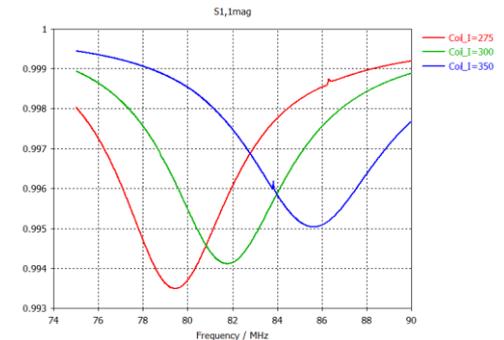
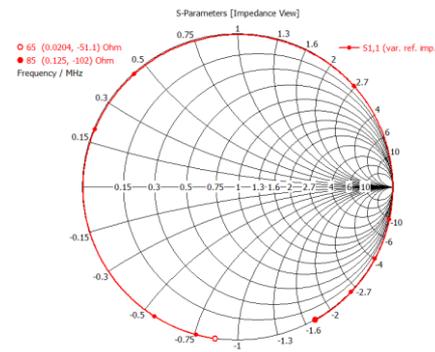
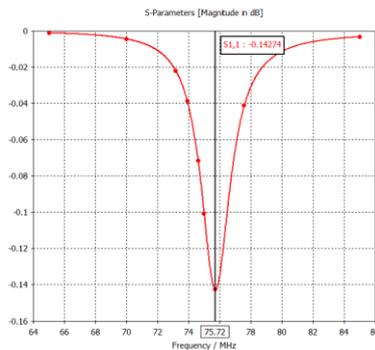
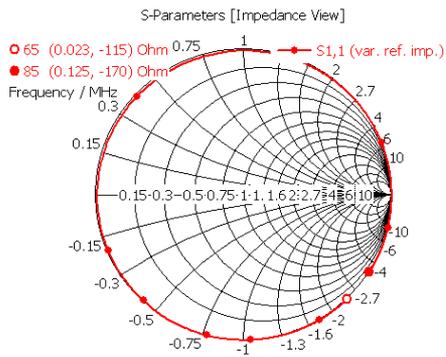
## Losses in copper and dielectric losses:

- Frequency domain solver with uniform garnet - 16.6 kW
- Eigenmode solver with uniform garnet - 16.7 kW
- Frequency domain with non-linear garnet at 106 MHz - 16.4 kW
- Transition model at 106 MHz - 20 kW

# Power coupler or blocking capacitor

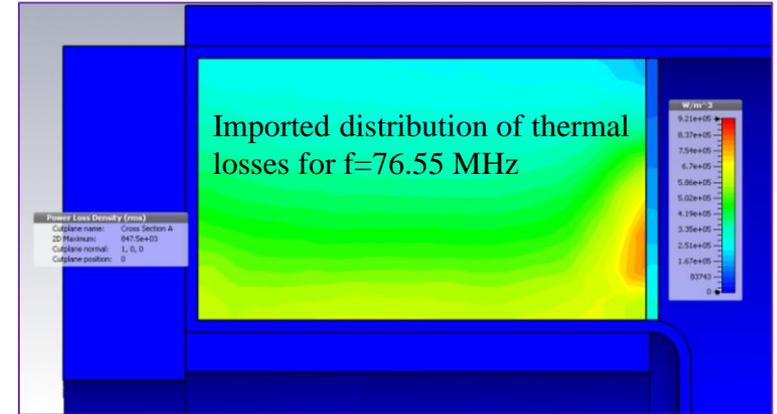
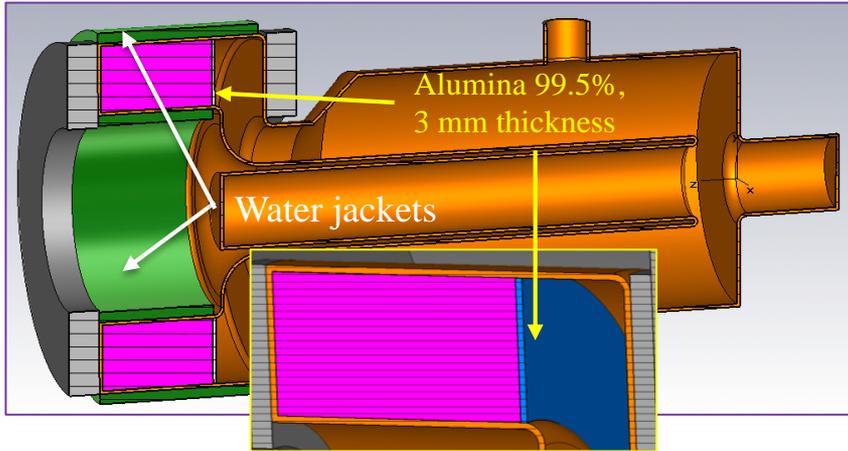


Capacitance (10pF from trans. model) is not convenient and sufficient requirement for designing. It is not even clear what is its definition in the 3D model.



Both are overcoupled. For higher frequency the reflection is increasing.

# Thermal analyses with alumina cooling disk

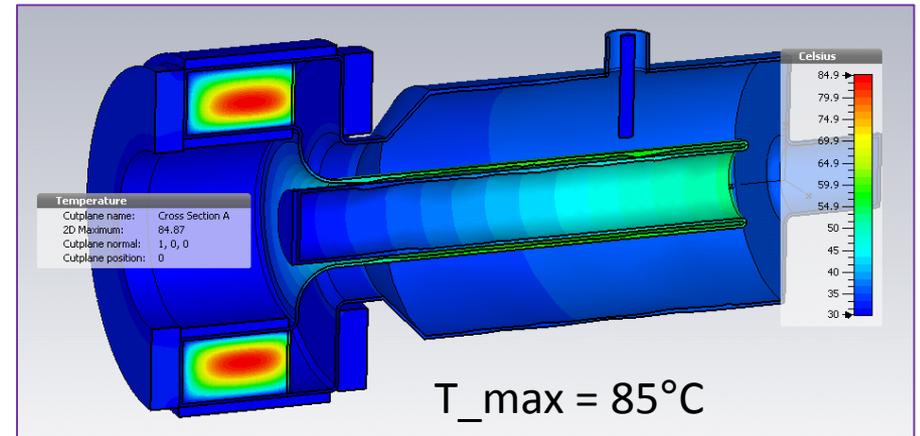


## Thermal conductivity

$\text{Al}_2\text{O}_3$  - 30 W/K/m

Al800 - 3.5 W/K/m

**Simulation** with thermal losses of  $P=3.2$  kW and cooling water temperature of  $30^\circ\text{C}$ , old ramp.



Temperature distribution

Additional alumina disks will reduce  $T_{\text{max}}$